Appendix E – Local Model Validation Report (LMVR)

REPORT N<sup>o</sup> 3

# LAKE LOTHING THIRD CROSSING

LOCAL MODEL VALIDATION REPORT

CONFIDENTIAL



# LAKE LOTHING THIRD CROSSING

#### LOCAL MODEL VALIDATION REPORT

**Suffolk County Council** 

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A P	Р	Ε	N	D	ΙX	D	POST ME SCREENLINE PERFORMANCE
A P	Р	Ε	N	D	ΙX	Ε	INDIVIDUAL LINK COUNT PERFORMANCE
A P	Р	Ε	N	D	ΙX	F	JOURNEY TIME GRAPHS
АР	Р	Е	N	D	ιx	G	FLOW AND V/C PLOTS

## 1 INTRODUCTION

#### 1.1 PROJECT BACKGROUND

- 1.1.1 WSP | Parsons Brinckerhoff has been commissioned by Suffolk County Council (SCC) to undertake traffic modelling in support of a Transport Business Case (TBC) for a third crossing of Lake Lothing in Suffolk.
- There is an existing Lowestoft SATURN highway assignment model representing a base year of 2001. It is therefore considerably outside the Department for Transport (DfT) Transport Analysis Guidance (TAG) requirement (TAG Unit M3.1, January 2014) that trips with both trip ends within the Fully Modelled Area are based on survey data that is less than six years old. The existing model has sub-optimal demand segmentation and assignment, with a single user class matrix representing all cars assigned on top of an HGV pre-load and there is no interpeak model.
- 1.1.3 There have also been improvements in software, techniques and best practice in the intervening period, which, combined with advice provided by SCC, make the existing model unsuitable for use as the basis for assessment.
- 1.1.4 The existing network and zone system will serve as the starting point for development of the updated Lowestoft model, with further refinement where necessary. Given their age, the existing matrices will not be used, but matrices will be rebuilt from new survey data.

#### 1.2 REPORT STRUCTURE

- 1.2.1 This Local Model Validation Report (LMVR) sets out information relating to the development, calibration and validation of the updated highway assignment model. It is structured as follows:
  - → Section 2 Proposed uses of the model and key design considerations
  - → Section 3 Model standards
  - → Section 4 Key features of the model
  - Section 5 Calibration and validation data
  - Section 6 Network development
  - → Section 7 Trip matrix development
  - Section 8 Network calibration and validation
  - → Section 9 Route choice calibration and validation
  - → Section 10 Trip matrix calibration and validation
  - → Section 11 Assignment calibration and validation
  - → Section 12 Summary of model development, standards achieved and fitness for purpose

#### 1.3 DISCLAIMER

- 1.3.1 This report, and information or advice which it contains, has been prepared for the purposes set out in the instructions commissioning it (June 2015) and has been prepared with reasonable skill, care and diligence. This report has been prepared by WSP | Parsons Brinckerhoff in their professional capacity as Consultants and in performance of WSP | Parsons Brinckerhoff's duties and liabilities under its contract with Suffolk County Council. Any advice, opinions, or recommendations within this report should be read and relied upon only in the context of the report as a whole. The advice and opinions in this report are based upon the information made available to WSP | Parsons Brinckerhoff at the date of this report and on current UK standards, codes, technology and construction practices as at the date of this report. The contents of the report do not, in any way, purport to include any manner of legal advice or opinion.
- 1.3.2 The transport modelling that has been carried out under the terms of our appointment (June 2015) and described in this report has been carried out using SATURN (version 11.3.12F). Transport modelling software of this type provides predictions of transport flows on the basis of a number of assumptions. The assumptions made in developing the transport model have been identified within this report.
- 1.3.3 The liability of WSP | Parsons Brinckerhoff in respect of the information contained in the report will not extend to any third party. WSP | Parsons Brinckerhoff accept no responsibility for any costs or losses howsoever incurred as a result of the use of the output from this report unless it is proved to have failed to exercise the degree of skill and care embodied in the terms and conditions of the governing appointment (June 2015) having regard to the use of the software and the assumptions made.

# PROPOSED USES OF THE MODEL AND KEY DESIGN CONSIDERATIONS

#### 2.1 SCENARIOS TO BE FORECAST AND INTERVENTIONS TO BE TESTED

2.1.1 The Lowestoft Traffic Model (LTM) has been developed and validated for the sole purpose of assessing a third crossing of Lake Lothing in Lowestoft. The town centre currently has two river crossings as shown in figure 2.1.

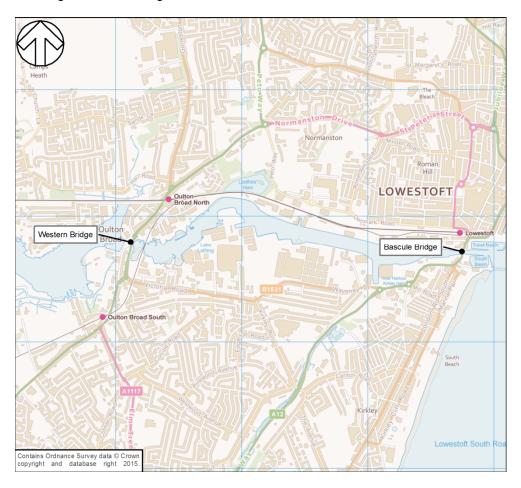


Figure 2.1 - Bridge locations

- 2.1.2 Various options regarding a third crossing are under consideration, and these will be discussed in the relevant reports relating to scheme design and the Transport Business Case (TBC).
- 2.1.3 In addition, the updated LTM may be used to for other assessment purposes subsequent to work relating to the third crossing, but this will require further review of validation to ensure it is fit for other purposes.

#### 2.2 KEY MODEL DESIGN CONSIDERATIONS

- 2.2.1 There are a number of key characteristics of Lowestoft town centre that require particular treatment, and these predominantly relate to the operation of the existing bridges.
- 2.2.2 The western bridge carries the A146 over Lake Lothing, and is significantly constrained by a level crossing to the north of the bridge. Barriers are frequently closed for long periods, leading to lengthy queues that block back across the bridge and other junctions.
- 2.2.3 The eastern Bascule bridge is a lifting bridge which, when raised, can lead to similarly long queues in the town centre. The majority of bridge openings occur in the interpeak period, but not exclusively so. The low height of this bridge and its proximity to the harbour mouth means that it is required to be opened for relatively small craft on a fairly frequent basis. Observations carried out between 14 and 16 April 2015, provided by AECOM, indicate the eastern bridge lifted once during the AM peak (0800-0900) and once during the PM peak (1700-1800) during the days surveyed. In the interpeak (1000-1600) the bridge lifted a maximum of three times during the observed period.
- 2.2.4 An additional design consideration for the traffic model is that there is a tidal flow lane running across the bridge along the A12 between Belvedere Road and Station Square. This was handled by changing the capacity and number of lanes in each direction according to the time of day.
- Observed data for the tidal flow section was provided to WSP | Parsons Brinckerhoff by AECOM, covering 14 to 16 April 2015, detailing the direction of the central lane between 07:00-10:00 and 16:00-19:00. For the AM peak (08:00-09:00) the central lane was modelled as allowing northbound traffic, in the PM peak (17:00-18:00) the central lane is southbound. No observed information was available for the interpeak, however journey time information covering the Bascule Bridge indicated delays similar to the PM peak, and therefore the central lane was modelled as allowing southbound traffic in the interpeak.
- A key issue that has arisen from previous work on this scheme is that it is important to understand the broad origins and destinations of the users of each bridge, and if there is any difference in the split between long-distance strategic users and local users at each bridge crossing that may inform the impacts of a third crossing.

## 3 MODEL STANDARDS

#### 3.1 VALIDATION CRITERIA AND ACCEPTABILITY GUIDELINES

3.1.1 The validation of specific aspects of the model is discussed in following sections of this report. In general, the following criteria will apply, drawn from WebTAG Unit M3.1, section 3.2 (January 2014):

#### SCREENLINE VALIDATION

3.1.2 Screenline validation is undertaken as a check on the trip matrix, and is assessed in terms of the percentage difference between observed and modelled flows as shown in table 3.1.

Table 3.1 - Screenline acceptability

CRITERIA	Description of Criteria	ACCEPTABILITY GUIDELINE
	Differences between modelled flows and counts should be less than 5% of counts	All or nearly all screenlines

- 3.1.3 Screenlines are presented for each time period, for cars and total vehicles. Although TAG requires information for all vehicle types to be presented, counts of LGV and HGV are not sufficiently high in this study area to allow useful comparisons to be made.
- 3.1.4 "Nearly all" is interpreted here as relating to 85% of cases, in keeping with link validation standards.

#### LINK FLOW AND TURNING MOVEMENT VALIDATION

- 3.1.5 Measures used for link validation are:
  - → Absolute and percentage differences between absolute and modelled flows
  - GEH statistic
- 3.1.6 The GEH statistic is a modified Chi-squared statistic incorporating both relative and absolute errors, defined as follows:

$$GEH = \sqrt{\frac{(M-C)^2}{(M+C)/2}}$$

3.1.7 The link flow and turning movement validation criteria are shown in table 3.2.

Table 3.2 - Link acceptability

CRITERIA	DESCRIPTION OF CRITERIA	ACCEPTABILITY GUIDELINE
1	Individual flows within 100 veh/hr of counts for flows less than 700 veh/hr	> 85% of cases
	Individual flows within 15% of counts for flows from 700 veh/hr to 2,700 veh/hr	> 85% of cases
	Individual flows within 400 veh/hr of counts for flows more than 2,700 veh/hr	> 85% of cases
2	GEH < 5 for individual flows	> 85% of cases

- 3.1.8 Both link flows and turning movements are presented using the above criteria, although turning movements are not generally expected to fully meet the criteria.
- 3.1.9 Information is presented for cars and total vehicles in all modelled time periods.

#### JOURNEY TIME VALIDATION

3.1.10 Criteria for journey time validation are presented in table 3.3.

Table 3.3 - Journey time acceptability

CRITERIA	DESCRIPTION OF CRITERIA	ACCEPTABILITY GUIDELINE	
1	Modelled times along routes should be within 15% of surveyed times (or minute, if higher than 15%)	> 85% of routes	

- 3.1.11 The model does not feature different speed/flow relationships or link speeds for different vehicle types, the comparisons are presented for all vehicles combined.
- 3.1.12 Comparisons are presented separately for all modelled time periods.

#### 3.2 CONVERGENCE CRITERIA AND STANDARDS

- 3.2.1 An element of calibrating the model is ensuring that a satisfactory convergence is achieved. Model convergence is needed to ensure traffic flows remain stable between successive iterations of the model. This is particularly important when model outputs are used to inform the economic benefits of scheme appraisal, as it is critical that calculated benefits arise from the impact of the scheme and not as a result of difference in convergence.
- In accordance with criteria set out in TAG Unit M3.1 (January 2014), the parameters %Flow, %GAP and Delta ( $\delta$ ) have been monitored to determine the level of convergence. %Flow measures the proportion of links in the network with flows changing by less than 1% from the previous iteration.  $\delta$  is the difference between costs on chosen routes and costs on minimum cost paths. %GAP is a generalisation of the  $\delta$  function to include the interaction effects within the simulation.

3.2.3 The convergence criteria used to assess when a model is considered to have converged is shown in table 3.4.

**Table 3.4 - Convergence criteria** 

Measure of Convergence	ACCEPTABLE VALUE
'Delta' and %GAP	Less than 0.1% or at least stable with convergence fully documented and all other criteria met
Percentage of links with flow change < 1%	Four consecutive iterations greater than 98%
Percentage of links with cost change < 1%	Four consecutive iterations greater than 98%
Percentage change in total user costs	Four consecutive iterations less than 0.1%

3.2.4 TAG Unit M3.1 indicates that delta  $(\delta)$  and %GAP values of less than 0.1% is the most fundamental indicator of model convergence and should be achieved as a minimum.

## 4 KEY FEATURES OF THE MODEL

#### 4.1 FULLY MODELLED AREA AND EXTERNAL AREA

4.1.1 The hierarchy of the model area is shown in figure 4.1

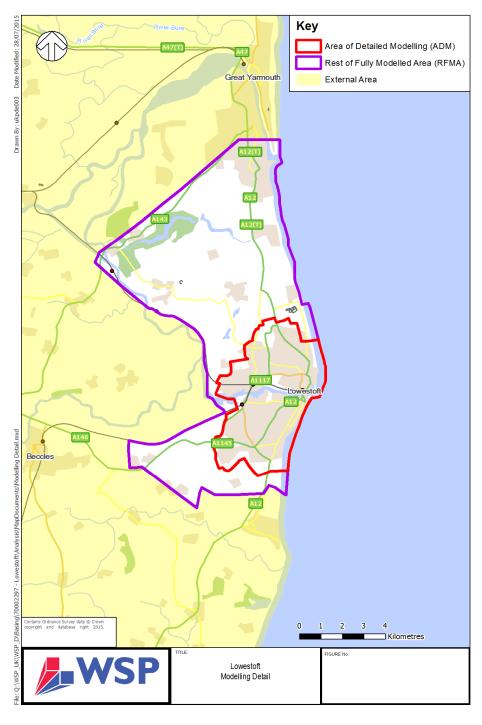


Figure 4.1 - Modelled area

#### 4.2 ZONING SYSTEM

4.2.1 The zoning system is based initially on census LSOA and MSOA boundaries, split to better fit realistic zoning points. The zones within the area of detailed modelling are shown in figure 4.2.

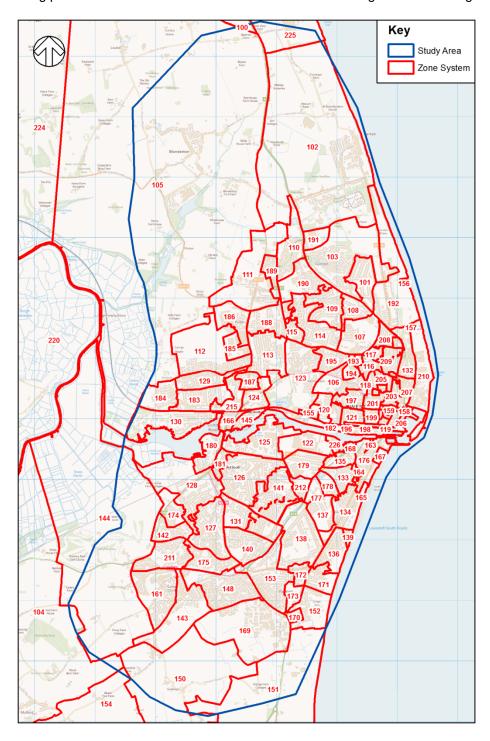


Figure 4.2 - Zoning in area of detailed modelling

#### 4.2.2 Figure 4.3 shows the zoning in the rest of the fully modelled area and the external area.

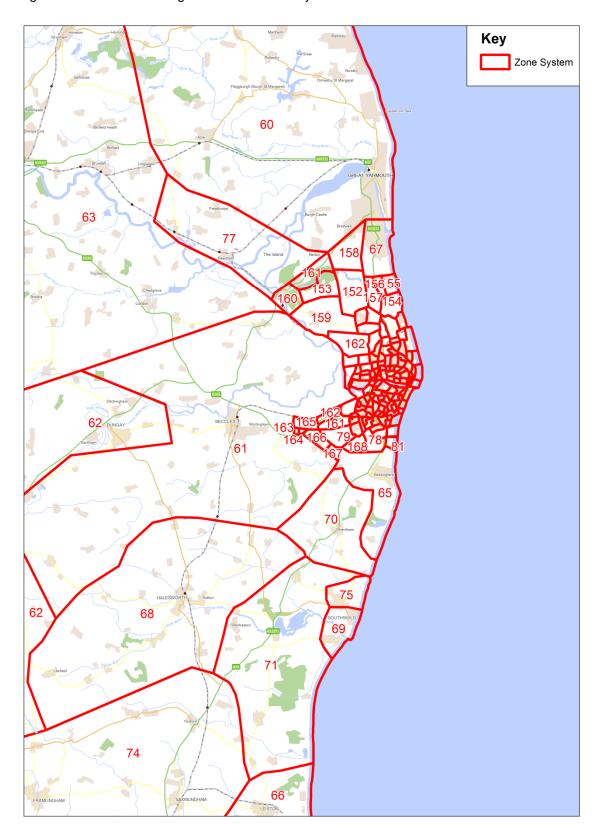


Figure 4.3 - Zoning in external area

4.2.3 The zones have been grouped to create five sectors. The locations of these can be seen in Figure 4.4.

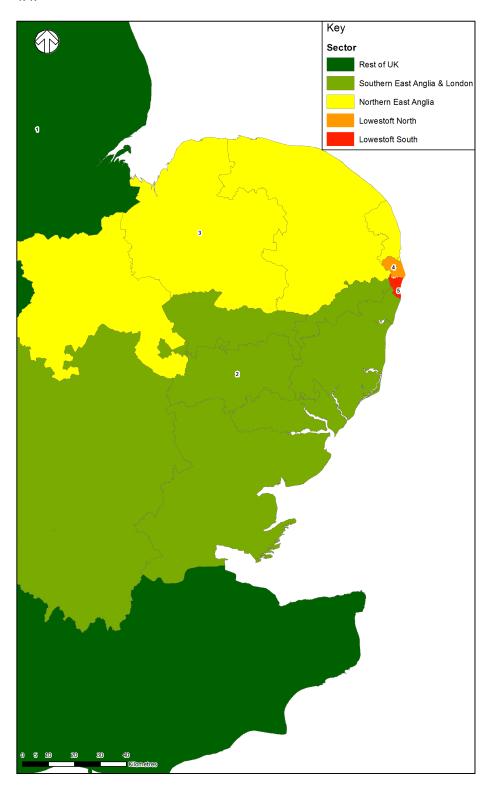


Figure 4.4 - Sector Plan

#### 4.3 NETWORK STRUCTURE

- 4.3.1 The area of detailed modelling covers the town of Lowestoft. In this area, the extent of the network is sufficient to cover all roads with significant traffic volumes and all realistic route choice available to drivers. All major junctions are modelled. In the Rest of the Fully Modelled Area, detail is reduced, with all principal strategic routes modelled and capacity restraint characterised through the use of speed/flow relationships as well as strategically important junctions.
- 4.3.2 In the External Area, the network is simplified to the extent that traffic is able to enter the Fully Modelled Area at the correct locations, without capacity restraint.
- 4.3.3 The network structure is shown in Figure 4.5.

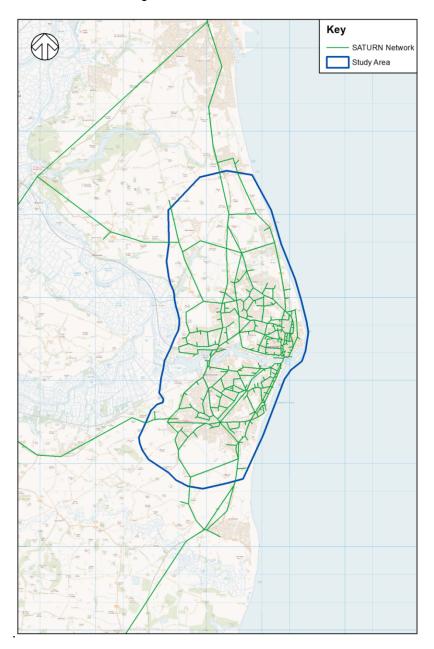


Figure 4.5 - Network structure

#### 4.4 CENTROID CONNECTORS

- 4.4.1 Centroid connectors connect the zoning system to the model network, allowing trips to load onto the network for assignment. It is critical that centroids connectors represent realistic loading points, particularly in the fully modelled area. Centroid connectors in the fully modelled area have been designed to represent actual loading points to specific residential and commercial areas, generally via a spur link to represent the actual access point. In this way, turns into and out of zones can be clearly understood.
- 4.4.2 The number of centroid connectors has been minimised, with most zones having a single centroid connector except in cases where a zone has clear multiple points of access, and sub-dividing the zone would not be realistic.
- 4.4.3 Centroid connectors have been designed so that they do not cross the network, further ensuring that loading is realistic. Connectors for different zones are loaded at different points, to ensure trips between adjacent zones are loaded on to the network. Centroid connectors are also loaded away from count locations, to avoid inconsistencies between the counted flow and loaded trips.
- 4.4.4 In the fully modelled area, zones are sufficiently small such that average costs to access the model are sufficiently represented by the spur access links, so centroids themselves do not have costs associated with them.
- In the external area, centroid connectors are linked to the network with appropriate parameters for distance and average speed to represent the average cost of accessing the network.

#### 4.5 TIME PERIODS

- 4.5.1 The following time periods are modelled:
  - → AM peak (08:00 09:00)
  - → Average interpeak (10:00 16:00)
  - → PM peak (17:00 18:00)

This is consistent with advice presented in Section 2.5 of TAG Unit M3.1 (January 2014). The choice of peak hour has been confirmed through analysis of the available long term ATC sites obtained through the Highways England TRADS database. Average counts are presented in Table 4.1 across each hour of the peak period, with the maximum peak identified in red.

Table 4.1 - Peak hour identification

N.4		AM PEAK			PM PEAK	
Month	0700-0800	0800-0900	0900-1000	1600-1700	1700-1800	1800-1900
January	1714	3020	2321	2495	2508	1624
February	1780	2679	2330	2462	2460	1724
March	1901	3078	2491	2620	2,594	1818
April	1818	2865	2470	2679	2772	1918
May	1837	2895	2438	2581	2677	1946
June	1858	3026	2466	2600	2735	1952
July	1766	2776	2424	2558	2700	1966
August	1629	2455	2351	2584	2746	2056
September	1850	2867	2387	2529	2591	1912
October	1817	2812	2350	2512	2565	1813
November	1797	2928	2399	2521	2476	1770
December	1548	2628	2380	2425	2275	1654

#### 4.6 USER CLASSES

- 4.6.1 The following user classes are modelled:
  - → UC1: Car Commuting
  - → UC2: Car Employer's Business
  - → UC3: Car Other
  - → UC4: LGV
  - → UC5: HGV
- 4.6.2 This is consistent with advice presented in Section 2.6 of TAG Unit M3.1 (January 2014).

#### 4.7 ASSIGNMENT METHODOLOGY

4.7.1 Model assignment of trips to the highway network was undertaken using a standard approach based on a 'Wardrop User Equilibrium', which seeks to minimise travel costs for all vehicles in the network. The Wardrop User Equilibrium is based on the following proposition:

"Traffic arranges itself on congested networks such that the cost of travel on all routes used between each origin-destination pair is equal to the minimum cost of travel and unused routes have equal or greater costs." 4.7.2 The Wardrop User Equilibrium as implemented in SATURN is based on the 'Frank-Wolfe Algorithm', which employs an iterative process. This process is based on successive 'All or Nothing' iterations, which are combined to minimise an 'Objective Function'. The travel costs are recalculated after each iteration and compared to those from the previous iteration. The process is terminated once successive iteration costs have not changed significantly. This process enables multi-routeing between any origin-destination pair.

#### 4.8 GENERALISED COST FORMULATIONS AND PARAMETER VALUES

4.8.1 Generalised cost is defined in keeping with the guidance in section 2.8 of TAG Unit M3.1 (January 2014), and is as follows:

$$Generalised\ cost = Time + \left(\frac{Vehicle\ operating\ cost}{Value\ of\ time}\right) Distance$$

- Value of time is calculated in pence per minute (PPM) and vehicle operating cost is calculated in pence per kilometre (PPK). The adopted parameters were calculated from the WebTAG databook (November 2014).
- 4.8.3 The parameters adopted for a 2015 base year are shown in Table 4.2. For the HGV class, local ATC data was used to determine the split of vehicles which could be classified as OGV1 and OGV2 by peak hour. This split was used to calculate average generalised cost parameters for HGV.

Table 4.2 – 2015 generalised cost parameters

USER CLASS	A	М	II	P	M	
	PPM	PPK	PPM	PPK	PPM	PPK
Car Commuting	13.74	6.70	13.63	6.70	13.44	6.70
Car Business	46.57	13.38	45.51	13.38	44.78	13.38
Car Other	17.49	6.70	18.18	6.70	18.72	6.70
LGV	20.98	13.66	20.98	13.66	20.98	13.66
HGV	21.25	37.35	21.25	37.35	21.25	37.35

## 4.9 CAPACITY RESTRAINT MECHANISMS: JUNCTION MODELLING AND SPEED/FLOW RELATIONSHIPS

#### JUNCTION MODELLING

- 4.9.1 The following key junctions were directly measured in terms of their geometric characteristics with accurate saturation flows included within the model:
  - → Normanston Drive / Peto Way
  - Normanston Drive / Bridge Road / B1375
  - → Bridge Road / A146
  - → A12 / A146

- → A12 / Mill Road
- → A12 / A1145

#### SPEED/FLOW RELATIONSHIPS

- 4.9.2 Speed flow curves consistent with COBA 10 values were allocated to specific links, detailed in section 6.3
- 4.10 RELATIONSHIPS WITH DEMAND MODELS AND PUBLIC TRANSPORT ASSIGNMENT MODELS
- 4.10.1 The highway assignment model will be used as a component of a DIADEM-based variable demand model. No public transport assignment model is included, as it is not required for this assessment. The Traffic Forecasting Report sets out the interactions between the highway assignment model and the demand model, as well as providing further consideration of the need for public transport assignment modelling.

## 5 CALIBRATION AND VALIDATION DATA

#### 5.1 INTRODUCTION

5.1.1 WSP | Parsons Brinckerhoff commissioned a range of surveys which are detailed in the data collection report (October 2015). This included the types of data shown in Table 5.2.

Table 5.1 - Commissioned survey data

Survey Type	Survey Period	Тіме
Automatic Number Plate Recognition (ANPR)	Tuesday 14 July 2015	07:00-19:00
Automatic Traffic Counts (ATC)	Monday 29 June 2015 to Monday 27 July 2015	All day
Manual Classified Counts (MCC)	Tuesday 14 <sup>h</sup> July 2015	07:00-19:00

5.1.2 Manual Classified Counts (MCC) were also obtained from AECOM which were carried out between Tuesday 14 April 2015 and Thursday 16 April 2015, count data was only available at these sites for 0700-1000 and 1600-1900.

#### 5.2 TRAFFIC COUNTS AT ANPR SITES

- 5.2.1 Traffic counts were collected via Automatic Number Plate Recognition (ANPR) cameras at 29 locations described in
- 5.2.2 Table 5.2. The ANPR were located:
  - → on links at key entry points into the study area and on links within the study area including the western Mutford Bridge and eastern Bascule Bridge
  - at car parks within the study area.
- 5.2.3 The purpose of this data was to observe the major origin-destination movements within the study area from which to build the prior matrix.
- 5.2.4 MCC were conducted at each ANPR location to capture the total volume of traffic with vehicles classified into the following types:
  - → Car
  - → LGV
  - → OGV1
  - → OGV2
  - → Bus / Coach
- 5.2.5 Overall the sample rates at each of the external ANPR locations in both inbound and outbound directions were consistently high at around 95%. The overall match rate compared the ANPR trips to the total number of inbound trips recorded by the associated MCC was 51%. Matched trips represented inbound trips into the study area which are then picked up by another ANPR within the cordon. The overall match rate achieved was considered acceptable from which to produce a prior matrix though entails inferring the distribution for 49% of the traffic from the matched trips.

- As detailed in the data collection report, there were a number of issues with the ANPR surveys. At Site 3, on the A12 Yarmouth Road to the north of the study area there was a low inbound sample rate of 36%. The survey company reported the camera at this location appears to have been moved by a member of the public during the survey report which caused the ANPR camera to be at an angle which affected the ability to capture vehicle number plates.
- As detailed in the data collection report, there were a number of issues with the ANPR surveys. At site 13 on Flixton Road, the survey company reported that the ANPR camera failed and no vehicle number plates were captured at this location during the survey period. However an MCC was still carried out at this location.
- 5.2.8 At site 17, Swimming Pool car park, the MCC camera failed and no classified data could be provided at this location.
- 5.2.9 At Site 18 (Battery Green Road Car Park), Intelligent Data reported a corruption of the MCC recording which lead to some data loss leading to the sample rate calculated being above 100%. The ANPR data was therefore scaled to match the MCC data.
- As detailed in the data collection report, the inbound sample rate and subsequent match rate were low at this site, 36% and 26% respectively. The survey company explained this occurred due to a member of the public moving the camera during the survey period.

Table 5.2 – ANPR count location descriptions

ID	Description	Түре
1	A12 London Road	Link
2	A146 Beccles Road	Link
3	A12 Yarmouth Road	Link
4	Coast Road	Link
5	A12 Pier Terrace (Eastern Bascule bridge)	Link
6	A146 Bridge Road (Western Mutford bridge)	Link
7	B1375 Gorleston Road	Link
8	A1117 Millennium Way	Link
9	A12 Yarmouth Road	Link
10	A12 Tom Crisp Way	Link
11	B1532 London Road South	Link
12	B1074 Blundeston Road	Link
13	Flixton Road	Link
14	B1531 Waveney Drive	Link
15	North Quay Retail Park	Car Park

ID	Description	Түре
16	Links Road Car Park	Car Park
17	Swimming Pool Road Car Park	Car Park
18	Shopping Centre Car Park (Battery Green Rd exit)	Car Park
19	Shopping Centre Car Park (Gordon Road entry)	Car Park
20	Surrey St Car Park entry	Car Park
21	Surrey St Car Park exit (onto Clapham Road)	Car Park
22	Clapham Road Car Park	Car Park
23	St Johns Rd Car Park	Car Park
24	Kirkley Rise Car Park (Northern access)	Car Park
25	Kirkley Rise Car Park (Southern access)	Car Park
26	Kirkley Cliff Road Car Park	Car Park
27	Claremont Road Car Park	Car Park
28	Marine Parade Car Park	Car Park
29	Asda Car Park	Car Park

5.2.11 Figure 5.1 shows the locations of the ANPR counts located on links within the study area.

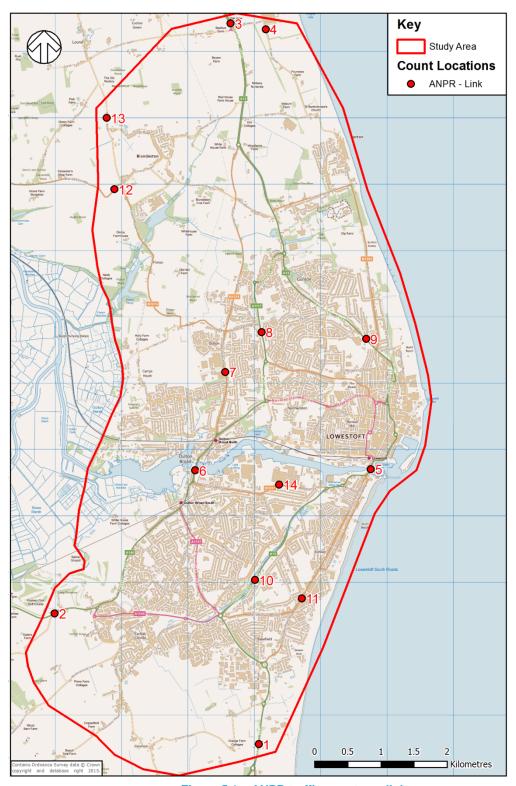


Figure 5.1 – ANPR traffic counts on links

#### 5.2.12 Figure 5.2 shows the locations of ANPR counts carried out at car parks.

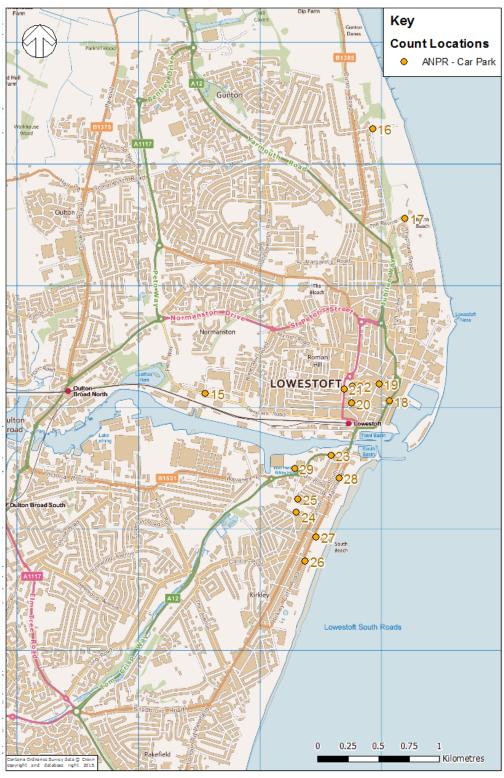


Figure 5.2 – ANPR traffic counts at car parks

#### 5.3 TRAFFIC COUNTS FOR MATRIX ESTIMATION

- 5.3.1 Table 5.3 describes the count locations which were used for matrix estimation.
- 5.3.2 The count locations used for matrix estimation were predominantly Automatic Traffic Counts (ATC). Monday to Thursday data was taken from the ATC data to provide an average flow at each location as per section 3.3 of TAG Unit M1.2. The majority of sites provided at least two continuous weeks of data, however data loss occurred at some sites as detailed in the data collection report, most notably at ATC Site 4 (A146 Beccles) Road for which only one observation was available.
- 5.3.3 The ANPR at site 3 (A12 Yarmouth Road) was used for matrix estimation; this site was located on a national speed limit dual carriageway. It was not possible for the survey company to safely lay an ATC at this location. The MCC count associated with ANPR site 3 (A12 Yarmouth Road) was used for matrix estimation at this location as it represents a key route for traffic entering and exiting the main study area.

Table 5.3 – Description of traffic counts used for matrix estimation

ID	Description	Түре
3	Gisleham Road	ATC
4	A146 Beccles Road	ATC
7	London Road South	ATC
8	A12 Tom Crisp Way	ATC
9	A1117 Elm Tree Road	ATC
11	Kirkley Run	ATC
12	A146 Waveney Drive	ATC
15	Katwijk Way	ATC
16	A12 Battery Green Road	ATC
19	Denmark Road	ATC
21	Peto Way	ATC
22	A1117 Normanston Drive	ATC
23	A1144 Normanston Drive	ATC
24	Oulton Road	ATC
25	B1375 Gorleston Road	ATC
26	A1117 Millennium Way	ATC
27	A12 Yarmouth Road	ATC

ID	Description	Түре
28	B1385 Corton Road	ATC
29	A12 Yarmouth Road	ATC
30	B1375 Parkhill	ATC
31	B1074 Blundeston Road	ATC
32	Flixton Road	ATC
3	A12 Yarmouth Road	ANPR - MCC

5.3.4 Figure 5.3 shows the locations of the counts used for matrix estimation and the calibration screenlines.

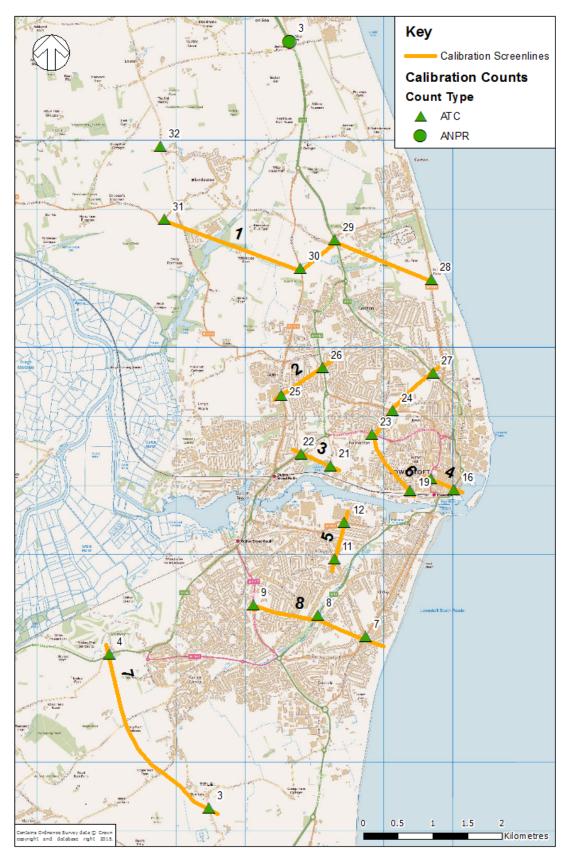


Figure 5.3 – Counts and screenlines used for calibration

#### 5.4 TRAFFIC COUNTS FOR VALIDATION

#### **LINK COUNTS**

5.4.1 Table 5.4 describes the count locations which were used for validation. As with the calibration counts the ATC data was processed to provide a Monday to Thursday average. For counts located at ANPR sites, the associated MCC link count / car park access count was used.

Table 5.4 – Description of traffic counts used for validation

ID	Description	TYPE
5	A1145 Castleton Avenue	ATC
6	A12 London Road	ATC
10	A146 Beccles Road	ATC
17	A12 Old Nelson Street	ATC
18	St Peter's Street	ATC
20	Rotterdam Road	ATC
33	Coast Road	ATC
6053	Katwijk Way	TRADS
5	A12 Pier Terrace (eastern Bascule Bridge)	ANPR - Link
6	A146 Saltwater Way (western Mutford Bridge)	ANPR - Link
15	North Quay Retail Park	ANPR – Car Park
16	Links Road Car Park	ANPR – Car Park
17	Swimming Pool Road Car Park	ANPR – Car Park
18	Shopping Centre Car Park (Battery Green Rd exit)	ANPR – Car Park
19	Shopping Centre Car Park (Gordon Road entry)	ANPR – Car Park
20	Surrey St Car Park entry	ANPR – Car Park
21	Surrey St Car Park exit (onto Clapham Road)	ANPR – Car Park
22	Clapham Road Car Park	ANPR – Car Park
23	St Johns Rd Car Park	ANPR – Car Park
24	Kirkley Rise Car Park (Northern access)	ANPR – Car Park
25	Kirkley Rise Car Park (Southern access)	ANPR – Car Park
26	Kirkley Cliff Road Car Park	ANPR – Car Park

ID	Description	Түре
28	Marine Parade Car Park	ANPR – Car Park
29	Asda Car Park	ANPR – Car Park

- 5.4.2 At ANPR site 5 (A12 Pier Terrace) on the eastern Bascule Bridge, only the MCC was available. The survey company were unable to find a suitable location at which to place an ATC.
- 5.4.3 At ANPR site 6 (A146 Saltwater Way) on the western Mutford Bridge, the MCC was used for validation. This was because the ATC laid at this location showed a notable difference in traffic flow southbound in the AM peak and PM peak, compared to the MCC (see Table 5.5). As discussed in section 7, regarding matrix development, the prior matrix was developed using the ANPR data, therefore the flow on the western Mutford Bridge would be more closely aligned to the MCC associated with the ANPR rather than the ATC data.

Table 5.5 – Comparison of ATC and MCC at western Mutford Bridge (A146 Saltwater Way)

ID	ATC COUNT TOTAL - NB	MCC COUNT TOTAL - NB	ATC COUNT TOTAL - SB	MCC COUNT TOTAL - SB
AM peak	942	944	777	904
Interpeak	920	983	861	931
PM peak	1064	1114	997	1133

The vehicle split for the western Mutford Bridge observed data was taken from the ATC data on the A146 Saltwater Way. This is because ATC was used for matrix estimation throughout the model. There was a notable difference in the vehicle splits between Car and LGV for the MCC and ATC at the western Mutford Bridge. This meant in terms of validation by vehicle type, the modelled flow was not ideally matched compared to the observed data if the MCC splits were used, which was out of keeping with adjacent counts based on ATC data. The comparison is shown in Table 5.6.

Table 5.6 – Comparison of ATC and MCC vehicle split for observed count total at western Mutford Bridge (A146 Saltwater Way)

ID	COUNT TOTAL	Car Total – MCC	LGV TOTAL – MCC	HGV Total - MCC	Car Total – ATC	LGV TOTAL – ATC	HGV TOTAL - ATC
AM - NB	944	780	139	25	656	242	46
AM - SB	904	716	152	36	506	367	31
IP - NB	983	819	130	35	718	228	38
IP - SB	931	780	120	31	575	329	27
PM - NB	1114	957	140	17	852	228	34
PM - SB	1133	1003	119	11	749	370	13

5.4.5 This issue was also prevalent for the MCC observed data on the eastern Bascule Bridge. As no ATC was available at this location, ATC 16 (A12 Battery Green Road) was used to provide the

vehicular split to the observed data, as shown in Table 5.7.

Table 5.7 – Comparison of ATC and MCC vehicle split for observed count total at eastern Bascule Bridge (A12 Pier Terrace)

ID	COUNT TOTAL	Car Total – MCC	LGV TOTAL – MCC	HGV TOTAL - MCC	Car Total – ATC	LGV TOTAL – ATC	HGV TOTAL - ATC
AM - NB	1531	1324	164	43	656	810	65
AM - SB	898	691	169	38	530	322	46
IP - NB	1041	870	127	44	453	532	56
IP - SB	1051	875	125	31	612	394	45
PM - NB	1104	966	110	28	582	499	24
PM - SB	1591	1419	147	25	1014	539	38

5.4.6 Figure 5.4 shows the locations of the counts used for validation and the validation screenlines.



Figure 5.4 – Counts and screenlines used for validation

#### MANUAL CLASSIFIED COUNTS

5.4.7 Manual classified counts were used for validation of turning movements at key junctions. Table 5.8 describes the locations of the turning counts.

Table 5.8 - Manual classified count locations

ID	Description
1	London Road/Arbor Lane/A12/Tower Road
2	Tom Crisp Way/Stadbroke Road/Elm Tree Road
3	Somerleyton Road/Oulton Street/Hall Lane/Gorleston Road
4	Yarmouth Road/Gorleston Road
5	Yarmouth Road/Leisure Way/Foxburrow Hill/Bentley Drive
6	Yarmouth Road/Corton Road
7	Millennium Way/Oulton Road/Peto Way
8	Horn Hill/Maconochie Way/A12/Waveney Drive
9	A12/Corton Long Lane/A12/Lowestoft Link Road
10	A12 Waveney Road/Station Square
11	Commercial Road/Station Square
12	A12 Pier Terrace/London Road South/Belvedere Road
13	A12 Belvedere Road/Kirkley Rise
14	Denmark Road/Katwijk Way
15	Katwijk Way/Raglan Street
16	A12 Waveney Road/Suffolk Road
17	A12 Tom Crisp Way/Blackheath Road
18	Saltwater Way/Victoria Road
19	Normanston Drive/Gorleston Road
20	Fir Lane/A117 Normanston Drive/Peto Way
21	A12/Gordon Road/Whapload Road
22	A12/St Peters Street
23	A1144/Katwijk Way
24	A146 Beccles Road/Cotmer Road

# 5.4.8 Figure 5.5 shows the location of the MCCs commissioned for this study.

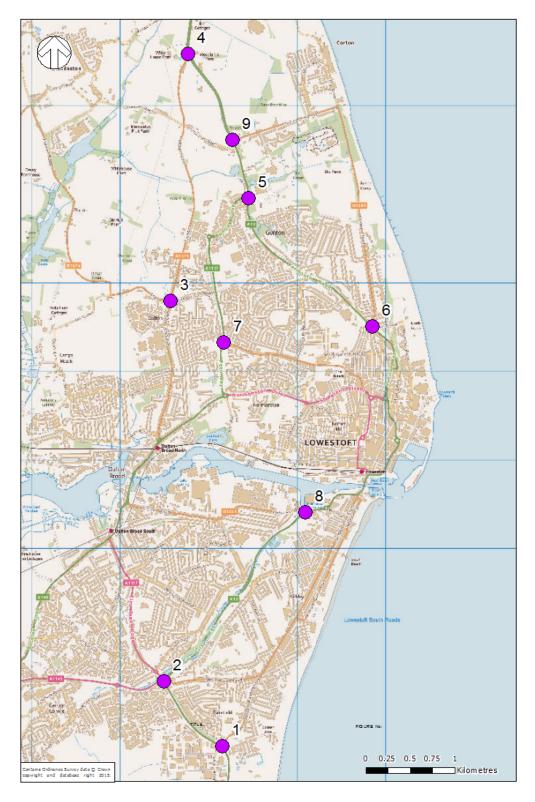


Figure 5.5 – Wider network MCC

# 5.4.9 Figure 5.6 shows the location of the MCCs carried out by AECOM.

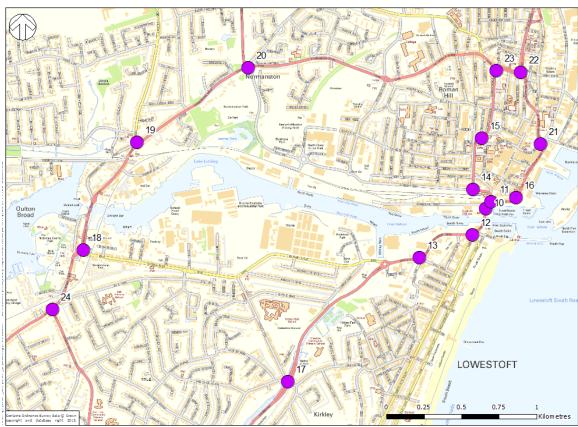


Figure 5.6 – AECOM town centre MCC

#### 5.5 JOURNEY TIME SURVEYS FOR CALIBRATION AND VALIDATION

5.5.1 Table 5.9 describes the journey time routes which were used for calibrating and validating the model. These represent the key routes through the model study area

Table 5.9 – Description of journey time routes

ID	DESCRIPTION	LENGTH
1	B1375 Gorleston Road	4.5km
2	A12 Yarmouth Road / Katwijk Way	6.2km
3	A1117 Normanston Drive / A1144 St Peter's Street	3.3km
4	A1117 Bentley Drive / Millennium Way / Peto Way	2.5km
5	A12 London Road / B1532 London Road South	6.7km
6	A1145 Castleton Avenue / A12 Tom Crisp Way / A12 Belvedere Road	6.7km
7	B1074 / A1117 Millennium Way / Oulton Road	3.9km
8	A146 Beccles Road / A146 Waveney Drive	9.5km
9	A12 Bloodmoor Road / A1117 Elm Tree Road	3.6km

- Trafficmaster journey time data covering key links within Suffolk was obtained from the DfT with the average journey time calculated from June 2015 data, for Monday to Thursdays only. The Trafficmaster data was related to an ITN road network, using ArcGIS this network was related to the SATURN network to allow the comparison of observed and modelled journey time.
- 5.5.3 Due to the variability of the data, the average and standard deviation of the data was analysed in order to determine the high and low confidence interval for the data. Observations outside these high and low intervals were deemed to be outliers and excluded. This ensured the average travel time was not unduly distorted by unusually high or low values.
- 5.5.4 Figure 5.7 shows the extent of the journey time routes.

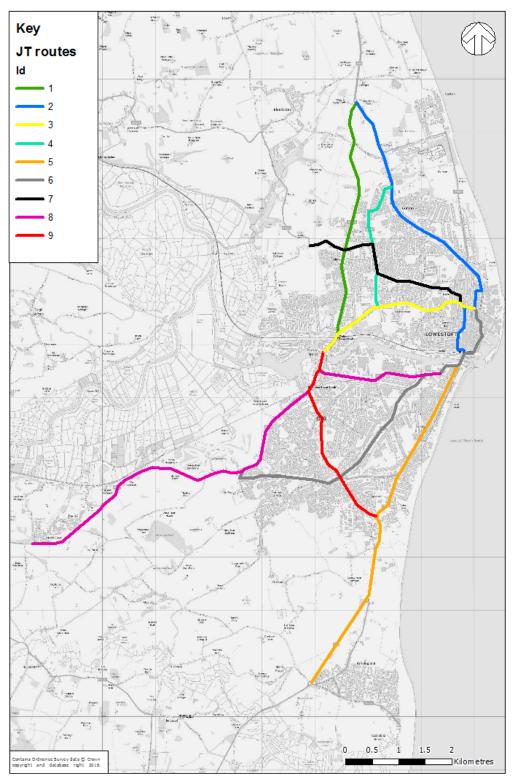


Figure 5.7 – Journey time routes

# 6 NETWORK DEVELOPMENT

### 6.1 NETWORK DATA, CODING AND CHECKING

- 6.1.1 The model network was based on the existing Lowestoft SATURN model network, updated to take account of any changes to the network that had occurred since the original Lowestoft model was built, or any significant coding errors.
- The network was verified through the use of ArcGIS, site visits and aerial photography. In particular, checks were carried out to verify:
  - Node co-ordinates
  - Link length check against measured GIS distance
  - Speed/flow relationship
  - → Link type
  - Link capacity
  - One way/two way operation
  - → Number of (effective) lanes
  - Length and position of flares
  - Any observed turn delays/penalties
  - → Location of public transport routes
  - Access points.
- 6.1.3 The network errors and warnings generated by SATURN were checked to ensure the model network is free of coding errors.
- 6.1.4 Traffic loads onto the model network from zones in the form of centroid connectors. The centroid zone connectors in the updated Lowestoft model have been reviewed and refined to realistically represent the way in which traffic joins the road network. In the Fully Modelled Area, where the zoning system is fine, specific access roads from residential and commercial areas have been used as a basis for connecting zones to the network via centroid connectors.
- Zones in the External Area, which have a large geographical coverage and significant demand associated with them, are generally connected to major routes to enter the network.

#### 6.2 JUNCTIONS

- 6.2.1 Each junction included in the ADM network required several parameters as detailed below:
  - > Lane allocations
  - Junction type
  - → Saturation flows at signal-controlled and priority-controlled junctions
  - Signal times, stages and phases
  - Circulation and saturation flows at roundabouts
  - Gap times.

#### FLOW/DELAY RELATIONSHIPS

Observations on when the eastern Bascule Bridge and western Mutford Bridge were lifted and not open to road traffic were obtained. This information was covered Tuesday 14 April 2015 to Thursday 16 April 2015. Table 6.1 details the observed data for the eastern bridge.

Table 6.1 -	Fastern	Rascula	Bridge	observed	lifting times
i able o. i –	Eastern	Dascule	Diluue	observed	munu umes

PEAK HOUR	AM OBS OPENING	OPENING TIME	IP OBS OPENING	OPENING TIME	PM OBS OPENING	OPENING TIME
Tues 14 April 2015	0	00:00:00	1	00:04:42	1	00:06:54
Weds 15 April 2015	0	00:00:00	3	00:12:22	0	00:00:00
Thurs 16 April 2015	1	00:04:17	0	00:00:00	0	00:00:00

- 6.2.3 The western Mutford Bridge was observed to only open once during the observation period, for 2 minutes 40 seconds on Wednesday 15 April 2015 at 09:51. As this occurred outside the modelled time periods, no swing bridge delay was included in the model for the western bridge.
- Table 6.2 shows the timings input into the model for the eastern Bascule Bridge. The delay was coded as a signalised node with a single stage, the red time representing when the swing bridge was lifted and with overall cycle time adding up to 3,600 seconds (1 hour). During the validation process, the AM peak bridge timings were initially coded as 257 seconds of red time to match the observed data, however during the validation process this was reduced to 227 seconds to ensure the flow validation improved on the bridge.

Table 6.2 - Eastern Bascule Bridge timings input into model

PEAK HOUR	GREEN TIME (SECONDS)	RED TIME (SECONDS)
AM peak	3,373	227
Inter peak	3,344	256
PM peak	3,186	414

Observations were also obtained for the two level crossings in the vicinity of the western Mutford Bridge – Bridge Road and Victoria Road. As with the swing bridge opening observations, the level crossings were observed between Tuesday 14 April 2015 and Thursday 16 April 2015. Table 6.3 shows the timings input for the Bridge Road level crossing. On average the barrier was down three times in the AM peak at this crossing, therefore the cycle time was set to 1,200 seconds (20 minutes), whereas in the interpeak and PM peak the barrier was down twice in an hour on average, the cycle time was therefore set to 1,800 seconds (30 minutes).

Table 6.3 - Bridge Road level crossing timings input into the model

PEAK HOUR	GREEN TIME (SECONDS)	RED TIME (SECONDS)
AM peak	1,017	183
Inter peak	1,485	315
PM peak	1,653	147

6.2.6 Table 6.4 outlines the timings input for the Victoria Road level crossing. On average the barrier was down twice in an hour at this location, therefore the cycle time was set to 1,800 seconds (30 minutes).

Table 6.4 – Victoria Road level crossing timings input into the model

PEAK HOUR	GREEN TIME (SECONDS)	RED TIME (SECONDS)
AM peak	1,693	107
Inter peak	1,553	247
PM peak	1,676	124

#### SIGNAL TIMINGS

- 6.2.7 Signal timings were extracted from controlled specs which were provided for eight key junctions within the study area, the junctions comprising of:
  - > Station Square / Denmark Road / Waveney Road
  - London Road South / Belvedere Road
  - Katwijk Way / Denmark Road
  - → Waveney Road / Suffolk Road / Battery Green Road
  - → Tom Crisp Way / Blackheath Road
  - Beccles Road / Cotmer Road
  - → St Peters Street / Boston Road
  - London Road / Mill Road.
- 6.2.8 The data from the controller specs were put into basic LinSig models to obtain realistic signal timings, stages and phases. The output results were inputted into the SATURN model for each time period.

#### SATURATION FLOWS

- 6.2.9 Default saturation flows were used for all junctions within the model. The default saturation flows per lane for priority junctions are:
  - Major straight ahead movement (unopposed) 1,980 pcu/hr
  - → Major left turn movement (unopposed) 1,500 pcu/hr
  - Major right turn movement (opposed) 745 pcu/hr
  - → Minor left turn movement (opposed) 700 pcu/hr
  - Minor right turn movement (opposed) 800 pcu/hr
  - → Minor straight ahead movement (opposed) 600 pcu/hr
- 6.2.10 Default saturation flows at signalised junctions are set to:
  - → Straight ahead movement 1,980 pcu/hr
  - → Left or right turn movement 1,740 pcu/hr

- 6.2.11 By default, SATURN assumes that opposing right turns at signalised junctions are "hooked" i.e. they interfere with each other. At larger junctions where there is sufficient space for traffic to turn right without being affected by the opposing right turn, it is possible to code these turns in the model so they do not interfere with each other. This was implemented at relevant junctions.
- Roundabouts require special consideration. Unlike with other junction types, each turn needs to be given the total saturation flow for the approach e.g. if a roundabout has a two-lane approach, with one lane to turn left and one to turn right, each turn should be coded with a saturation flow of 2,200. Default saturation flows (pcu/hr) adopted for roundabouts are given in Table 6.5. These values have been adopted to replicate typical ARCADY capacity estimates and have previously been utilised.

Table 6.5 - Roundabout entry capacity saturation flows

APPROACH LANES	NUMBER OF ENTRY LANES						
APPROACH LAINES	1	2	3	4			
Single (3.5m)	1,130	1,670	2,030				
Single (5.0m)	1,510	1,940	2,250	2,450			
Dual 2 lane		2,200	2,780	3,190			
Dual 3 lane			3,330	3,940			

6.2.13 Equivalent gap acceptance parameters are provided in Table 6.6.

Table 6.6- Roundabout gap acceptance parameters (seconds)

APPROACH LANES	Number of entry lanes						
APPROACH LAINES	1	2	3	4			
Single (3.5m)	1.8	1.3	1.2				
Single (5.0m)	1.4	1.2	1.1	1.1			
Dual 2 lane		1.1	1.0	0.9			
Dual 3 lane			0.9	0.8			

6.2.14 The overall circulatory saturation flow was set to be the same as the highest saturation flow on the approach arms of the roundabout. Large gyratory systems were coded as a series of priority junctions for a better representation of journey times through the junction

#### 6.3 LINKS

- 6.3.1 Each link included in the ADM network required several parameters as detailed below:
  - Distance
  - Speed

- Speed flow curve
- → Number of lanes
- → Penalties/bans.

#### SPEED/FLOW RELATIONSHIPS

- 6.3.2 Highway capacity is restrained by junctions and by the speed-flow curves allocated to links in the study area. Speed flow curves are based on standard COBA 10 values and allocated to specific links based on assessment of the road speed, width and capacity. Speed-flow curves have generally only been used on rural or inter-urban links where the characteristics of the link itself, rather than junction capacity, have an impact on traffic speed. It has been necessary in some circumstances to use speed-flow curves in suburban areas to replicate the impacts of unmodelled minor junctions.
- 6.3.3 The speed flow curves that were used are shown in Table 6.7.

Table 6.7 - Model speed flow curves

DESCRIPTION	ID	FREE FLOW SPEED	SPEED AT CAPACITY	CAPACITY	Power value
Rural - D4M Motorway - 4 lanes	1	116	45	9,999	3.8
Rural - D3M Motorway - 3 lanes	2	116	45	7,560	3.8
Rural - D2M Motorway - 2 lanes	3	112	45	4,860	3.9
Rural - D3AP All-purpose - 3 lanes	4	109	45	6,780	3.7
Rural – D2AP All-purpose - 2 lanes	5	105	45	4,360	3.7
Rural - S10(Good) - 2 lanes	6	91	45	3,720	2.2
Rural - S10(Good) - 1 lane	7	91	45	1,860	2.2
Rural - S10(Typical) - 2 lanes	8	84	45	3,320	2.2
Rural - S10(Typical) - 1 lane	9	84	45	1,660	3.1
Rural - S7.3(Good) - 2 lanes	10	87	45	3,280	2.2
Rural - S7.3(Good) - 1 lane	11	87	45	1,640	2.2
Rural - S7.0(Typical) - 2 lanes	12	78	45	2,760	2.1
Rural - S7.0(Typical) - 1 lane	13	78	45	1,380	2.1
Rural - S6.5(Bad) - 2 lanes	14	67	45	2,020	1.8
Rural - S6.5(Bad) - 1 lane	15	67	45	1,010	1.8
Suburban - Dual(Slight devel)	16	78	35	3,460	3.3
Suburban - Single(Slight devel)	19	68	25	3,460	3.7

Description	ID	FREE FLOW SPEED	SPEED AT CAPACITY	Capacity	Power value
Suburban - Single(Slight devel)	20	68	25	1,730	3.7
Suburban - Dual(Typical devel)	21	61	25	2,540	2.3
Suburban - Dual(Typical devel)	22	61	25	1,570	2.3
Suburban - Dual(Heavy devel)	23	48	25	1,000	1.6
Suburban - Dual(Heavy devel)	24	48	25	500	1.6
Urban - Non-central(Good) - 2 lanes	25	54	25	1,960	1.7
Urban - Non-central(Good) - 1 lane	26	54	25	980	1.7
Urban - Non-central(Typical) - 2 lanes	27	49	25	1,560	1.6
Urban - Non-central(Typical) - 1 lane	28	49	25	780	1.6
Urban - Non-central(Poor) - 2 lanes	29	45	25	1,300	1.5
Urban - Non-central(Poor) - 1 lane	30	45	25	650	1.5
Urban - Central(Good) - 2 lanes	31	37	15	1,480	1.8
Urban - Central(Good) - 1 lane	32	37	15	740	1.8
Urban - Central(Typical) - 2 lanes	33	34	15	1,260	1.7
Urban - Central(Typical) - 1 lane	34	34	15	630	1.7
Urban - Central(Poor) - 2 lanes	35	29	15	900	1.6
Urban - Central(Poor) - 1 lane	36	29	15	450	1.6
Small Town - Light devel - 2 lanes	37	66	30	2,600	3.0
Small Town - Light devel - 1 lane	38	66	30	1,300	3.0
Small Town - Typical devel - 2 lanes	39	57	30	2,000	3.4
Small Town - Typical devel - 1 lane	40	57	30	1,000	3.4
Small Town - Heavy devel - 2 lanes	41	47	30	1,760	2.5
Small Town - Heavy devel - 1 lane	42	47	30	880	2.5
Suburban - Single(Slight devel)	43	78	35	1,730	3.7
Centroid Connector - Internal	50	87	87	9,999	3.3

#### **FIXED SPEEDS**

- 6.3.4 Within the urban area of the model speed flow curves were not necessary due to capacity restraints from the junctions at either end of the link.
- 6.3.5 These links were given fixed speeds based on their individual speed limit as obtained from imagery and site visits.
- 6.3.6 These speeds will reflect the free flow speed whilst the delay at junctions will reflect the conditions in busier periods.

# 7 TRIP MATRIX DEVELOPMENT

#### 7.1 TRAVEL DEMAND DATA

7.1.1 The matrix was initially built from observed data based on the ANPR surveys detailed in section 5. ANPR data was filtered and factored to match the associated MCC. Following assignment of the observed matrix using select link analysis, a gravity model was devised utilising synthetic trip ends based on NTEM version 6.2 and the 2011 census. The gravity model produced a synthetic matrix which was then combined with the observed matrix to produce the initial prior matrix.

#### 7.2 PARTIAL TRIP MATRICES FROM SURVEYS

- 7.2.1 For each site, trip chains were split into the following peak periods:
  - → AM peak period (07:00-10:00)
  - → Inter peak period (10:00-16:00)
  - → PM peak period (16:00-19:00)
- 7.2.2 Peak periods were used for the AM peak and PM peak rather than peak hours to increase the size of the sample which would be used to infer O-D movements within the study area.
- 7.2.3 Timestamps were available which detailed the exact time a vehicle was detected by an ANPR camera. Each unique matched vehicle was given an anonymised Vehicle Registration Number (VRN) and its data split into the different ANPR locations based on the first site at which the vehicle was detected. The site at which the vehicle was first detected was taken to be its origin for the purposes of matrix building.
- 7.2.4 The peak period for a vehicle was based on the timestamp for when it was first detected.
- 7.2.5 The total travel time for a trip chain was provided within the ANPR data, journeys taking longer than 60 minutes were excluded from the matrix building process. This was done because examination of the data highlighted many instances when vehicles were initially tracked at one location during a specific peak. However the next detection of the vehicle occurred over an hour later, often falling within a later peak period making such examples problematic to infer the origin-destination movement within the prescribed peak periods.
- 7.2.6 Table 7.1 shows the total number of observed trips with a duration of 60 minutes or less by peak period by the ANPR location at which they were first detected (for matrix purposes taken to be their origin).

Table 7.1 – Total observed ANPR trips (Less than 60 minutes in duration)

SITE	SITE DESCRIPTION	AM PEAK PERIOD (07:00-10:00)		INTER PEAK PERIOD (10:00-16:00)			PM PEAK PERIOD (16:00-19:00)			
		Car	LGV	HGV	Car	LGV	HGV	Car	LGV	HGV
1	A12 London Road	907	156	80	1,569	220	152	927	150	63
2	A146 Beccles Road	788	100	95	1,173	196	175	975	127	69
3	A12 Yarmouth Road	375	42	13	745	97	24	902	75	9
4	Coast Road	36	0	7	79	7	17	48	2	8
5	A12 Pier Terrace (Eastern Bascule bridge)	494	51	27	1,089	102	53	1,044	100	13
6	A146 Bridge Road (Western Mutford bridge)	1,293	175	68	1,488	155	87	806	80	31
7	B1375 Gorleston Road	680	124	40	926	100	60	640	67	23
8	A1117 Millennium Way	449	41	31	695	81	44	412	33	9
9	A12 Yarmouth Road	628	100	70	1,271	133	116	835	84	32
10	A12 Tom Crisp Way	787	96	32	711	70	46	508	37	16
11	B1532 London Road South	379	60	26	499	51	30	326	28	14
12	B1074 Blundeston Road	159	20	9	211	35	20	142	42	6
13	Flixton Road	0	0	0	0	0	0	0	0	0
14	B1531 Waveney Drive	341	34	12	375	22	10	240	18	3
15	North Quay Retail Park	60	6	2	280	12	4	122	12	0
16	Links Road Car Park	4	1	0	13	1	0	3	0	0
17	Swimming Pool Road Car Park	1	0	0	12	0	0	20	0	0
18	Shopping Centre Car Park (Battery Green Rd exit)	0	1	0	48	1	0	25	1	0
19	Shopping Centre Car Park (Gordon Road entry)	0	0	0	5	0	0	0	0	0
20	Surrey St Car Park entry	7	0	0	43	2	0	4	0	0

SITE	SITE DESCRIPTION	AM PEAK PERIOD (07:00-10:00)		INTER PEAK PERIOD (10:00-16:00)			PM PEAK PERIOD (16:00-19:00)			
		Car	LGV	HGV	Car	LGV	HGV	Car	LGV	HGV
21	Surrey St Car Park exit (onto Clapham Road)	0	0	0	38	1	0	9	2	0
22	Clapham Road Car Park	3	0	1	56	0	0	10	0	0
23	St Johns Rd Car Park	1	0	0	4	1	0	4	0	0
24	Kirkley Rise Car Park (Northern access)	3	0	0	12	0	0	10	0	1
25	Kirkley Rise Car Park (Southern access)	1	0	0	2	0	0	2	0	0
26	Kirkley Cliff Road Car Park	0	0	0	0	0	0	1	0	0
27	Claremont Road Car Park	0	0	0	8	1	0	11	0	0
28	Marine Parade Car Park	0	1	0	44	0	0	17	1	0
29	Asda Car Park	135	11	1	282	14	3	161	8	3
	Total		1,019	514	11,678	1,302	841	8,204	867	300

- 7.2.7 The observed ANPR trips were then factored using MCC totals for the peak hour carried out at each of the ANPR sites. The relevant direction for the MCC was used for factor the ANPR trips depending on whether it was an origin or a destination. For ANPR trips internal to the study area, the MCC directions had to be split proportionally based on the origin and destination totals at each site. Appendix A details the MCC totals used at each site
- 7.2.8 The MCC totals were used by site for doubly constrained furnessing of the observed ANPR trips taking an average of the origin and destination factor. This produced the observed peak hour matrix totals shown in Table 7.2.

Table 7.2 – Observed ANPR matrix totals following furnessing to MCC totals

USER CLASS	AM PEAK HOUR (08:00-09:00)			Inter Peak Avg. Hour (10:00-16:00)			PM PEAK HOUR (17:00-18:00)		
	TOTAL	INTER- ZONALS	Intra- Zonals	Car	LGV	HGV	Car	LGV	HGV
UC1 – Car	7,175	7,100	75	7,602	7,489	112	9,286	9,239	48
UC2 – LGV	1,115	1,110	5	980	973	7	1,039	1,031	7
UC3 – HGV	298	298	0.00	301	297	4.	148	147	2
Total	8,587	8,508	80	8,882	8,759	123	10,473	10,417	57

- 7.2.9 In order to distribute the ANPR matrices within the model, select link analysis at each ANPR site location was carried out using the 2001 Lowestoft SATURN model. This meant the observed data was distributed within the old zone system used for the 2001 Lowestoft SATURN model.
- 7.2.10 Analysis of the demand for each zone in this matrix showed that two zones adjacent to the eastern Bascule bridge had high numbers of trips associated with them relative to observed data available at these locations:
  - → Zone 2: covering the docks east of the A12 Battery Green Road / Waveney Road, linking to a single access at the A12 / Suffolk Road signals
  - → Zone 9: covering the commercial developments linking onto Commercial Road, linking on to a single access at the A12 Pier Terrace / Commercial Road.
- 7.2.11 Origin and destination totals for these zones were factored to match the arm in the respective MCC site 10 and site 11. The excess traffic was then distributed using select link analysis of the A12 Pier Terrace to ensure the overall matrix total was retained.
- The observed trip matrix was then converting into the new zone system used for the 2015 Lowestoft SATURN model. Correspondence between the old 2001 zone system and new 2015 zone system was done based on area, but took into account an urban outline boundary covering all built-up areas within the study area. This ensured that for instances in which zones contained large amounts of open space, the trip totals were concentrated only in the built-up area. This ensured land-use density was taken into account when the correspondence between the old and new zone system was carried out.
- 7.2.13 Following this process there was a small loss in the overall number of trips due to rounding issues as shown in Table 7.3

Table 7.3 – Observed ANPR matrix totals following correspondence between 2001 zone system and 2015 zone system

User Class	AM PEAK HOUR (08:00-09:00)		INTER PEAK AVG. HOUR (10:00-16:00)			PM PEAK HOUR (17:00-18:00)			
	TOTAL	INTER- ZONALS	INTRA- ZONALS	Car	LGV	HGV	Car	LGV	HGV
UC1 – Car	7,173	6,952	221	7,609	7,322	286	9,286	9,024	262
UC2 – LGV	1,114	1,083	31	981	948	33	1038	1,011	28
UC3 – HGV	298	287	11	301	292	9	149	145	4
Total	8,585	8,322	263	8,891	8,563	323	10,473	10,179	293

- 7.2.14 Intra-zonal trips were removed from the matrix, prior to splitting the car user class into the following three user classes:
  - Car commuting
  - Car employers business
  - Car other

7.2.15 This was carried out based on trip synthesis factors derived on a zone by zone basis as detailed in section 7.3. As factors were applied to both row and column values on a zone by zone basis this lead to a change in the overall size of the matrix.

Table 7.4 - Summary ANPR matrix totals

USER CLASS	AM PEAK HOUR (08:00-09:00)	INTER PEAK AVG. HOUR (10:00-16:00)	PM PEAK HOUR (17:00-18:00)
UC1 – Car Commuting	4,079	1,417	3,259
UC2 – Car EmpBus	485	499	524
UC3 – Car Other	2,373	5,391	5,232
UC4 – LGV	1,083	948	1,011
UC5 – HGV	287	292	145
Total	8,307	8,548	10,171

#### 7.3 TRIP SYNTHESIS

- 7.3.1 To account for trips that were otherwise unobserved by the ANPR surveys, a synthetic gravity model was created.
- 7.3.2 Peak period trip end totals were calculated for each model zone using trip end information from NTEM version 6.2 accessed via TEMPRO. Intersecting the model zoning system with the NTEM zones, NTEM trip ends were split proportionally to create synthetic trip ends totals for each model zone. 2011 work place zones and census output areas were used to determine the employment and housing numbers in the model zone system, these totals were used to help proportion the NTEM synthetic trip end totals.
- 7.3.3 NTEM trips were output by trip purpose. Three car user classes were made up of the following NTEM trip purposes:
  - → Car commuting:
    - Home-Based Work
    - Home-Based Education
  - Car employers business:
    - Home-Based Employers Business
    - Non-Home-Based Employers Business
  - Car other:
    - Home-Based Shopping
    - Home-Based Recreation / Social
    - Home-Based Personal Business
    - Home-Based Visiting Friends & Relatives
    - Home-Based Holiday / Day Trip
    - Non-Home-Based Work

- Non-Home-Based Education
- Non-Home-Based Shopping
- Non-Home-Based Recreation / Social
- Non-Home-Based Personal Business
- Non-Home-Based Holiday / Day Trip
- 7.3.4 The trips were factored from the peak periods available within NTEM to represent a peak hour using factors from local ATC as shown in Table 7.5.:

Table 7.5 – Peak period to peak hour factors

USER CLASS	Factor
AM peak period (07:00-10:00) to AM peak hour factor (08:00-09:00)	2.63
Inter peak period (10:00-16:00) to average hour factor	6.00
PM peak period (16:00-18:00) to PM peak hour factor (17:00-18:00)	1.84

#### 7.4 MERGING DATA FROM SURVEYS AND TRIP SYNTHESIS

- 7.4.1 The observed trip matrix was combined with the synthetic matrix using the gravity model.
- 7.4.2 The SATURN model was skimmed to produce generalised cost matrices, which were then used to distribute the synthetic trip end totals according to the following formula:

$$T_{ij} = O_i * D_j * \exp(-\beta * C_{ij})$$

- 7.4.3 Thus a trip (T) between any given origin-destination pair is defined as a function of total origin trips (O), total destination trips (D), generalised cost (C), and a deterrence parameter (β). The resultant trip matrices were assigned, and the costs re-skimmed. This process was repeated until the relative gap between the matrices was less than 1% on three successive iterations.
- 7.4.4 Due to there being few zero values in the observed matrix, a threshold was set at which trip ends within the gravity model would replace the values in the observed matrix. The thresholds for each peak were set as shown in Table 7.6.

Table 7.6 - Gravity model infill thresholds

Реак	THRESHOLD
AM peak (08:00-09:00)	5
Inter peak (10:00-16:00)	0.1
PM peak (17:00-18:00)	0.05

- 7.4.5 Trip length distributions were calculated and compared for known movements in the observed ANPR matrix. The results were analysed and the beta value adjusted with the gravity model rerun to produce an optimal fit between synthetic and observed trips. Attention was also paid to the distribution of the full matrix of synthetic trips to ensure close approximation to likely trip lengths.
- 7.4.6 The  $\beta$  values used within the gravity model are shown in Table 7.7.

Table 7.7 – Beta (β) values used within gravity model

USER CLASS	AM PEAK HOUR (0800-0900)	Inter Peak Avg. Hour (1000-1600)	PM PEAK HOUR (1700-1800)
Car commuting	0.91	0.39	0.9
Car emp business	0.96	0.33	0.9
Car other	0.71	0.3	0.9

7.4.7 The r-squared values that were achieved for each car user class across the three peaks are shown in Table 7.8.

Table 7.8 - R-square results from gravity model

USER CLASS	AM PEAK HOUR (0800-0900)	Inter Peak Avg. Hour (1000-1600)	PM PEAK HOUR (1700-1800)
Car commuting	0.729	0.887	0.592
Car emp business	0.697	0.872	0.629
Car other	0.911	0.881	0.838
Car overall	0.816	0.892	0.761

7.4.8 Appendix B contains details of the trip length distribution and changes applied to the matrix by the gravity model.

# 7.4.9 Following the gravity model infill, the prior matrix totals are shown in Table 7.9.

Table 7.9 – Prior matrix totals

USER CLASS	AM PEAK HOUR (0800-0900)	Inter Peak Avg. Hour (1000-1600)	PM PEAK HOUR (1700-1800)
UC1 – Car Commuting	6716	1970	4631
UC2 – Car EmpBus	7401	723	1034
UC3 – Car Other	3529	6513	6850
UC4 – LGV	1083	948	1011
UC5 – HGV	287	292	145
Total	12355	10447	13672

# 8 NETWORK CALIBRATION AND VALIDATION

#### 8.1 NETWORK CALIBRATION

- 8.1.1 Network calibration was carried out using the initial prior matrix to assist with checks of the network. The initial checks included:
  - Link speeds
  - Link flows
  - Junction delays
  - Volume over Capacity (V/C) ratios.
- 8.1.2 The junctions were also checked to ensure that the capacity of the junction was not less than the counts at any arms.
- 8.1.3 The modelled delay was not analysed due to no observed data being collected.
- 8.1.4 Following on from these adjustments the initial matrix was re-run and in addition the observed flows were checked against the modelled flow to ensure they were not significantly higher or lower.
- 8.1.5 The delays were rechecked to isolate any that were unacceptably lower than the observed delays.
- 8.1.6 The routes through the network were checked which focussed on ensuring that the routing over the two existing bridges are correct as well as the other main strategic routes through Lowestoft.
- 8.1.7 The routes taken by HGV were also checked to confirm that certain links with weight or height restrictions had the appropriate ban on them.
- 8.1.8 The route choice will be discussed in greater detail in Section 9 of this report.

#### 8.2 NETWORK VALIDATION

- 8.2.1 The journey time routes were assessed with the initial prior matrix to sense check the time it takes to travel on certain links. This indicated any junctions that had unexpected delays or link speeds that were consistently less than the speed limit.
- 8.2.2 Journey times that had a difference of greater than 25% versus the observed time were checked to confirm that all the characteristics as set out in Section 6 for both links and junctions were consistent with the actual road network.
- 8.2.3 The link characteristics were also checked on any links where the observed count and modelled flow had a difference of 25% or more.
- 8.2.4 These checks allowed full confidence that the model reflected the real situation as close as possible.

# 9 ROUTE CHOICE CALIBRATION AND VALIDATION

#### 9.1 ROUTE CHOICE CALIBRATION

- 9.1.1 The generalised costs have an effect on the route choice made by different user class and trip purposes.
- 9.1.2 Generalised costs were calculated using values of time, GDP growth rates, purpose splits, and vehicle operating costs recommended by the DfT for use in economic appraisals of transport projects in England. These values are presented in the November 2014 TAG data book and follow the guidance within the latest version of WebTAG Unit A1.3. The values calculated for use in the base year models are shown in Table 9.1 and Table 9.2. Table 9.1 outlines the Pence per Minute (PPM) values by peak period and vehicle class, whilst Table 9.2 shows this in terms of Price per Kilometre (PPK).

Table 9.1 - Generalised cost parameters - pence per minute (PPM)

PEAK	CAR – COMMUTING	Car – Employers Business	Car – Other	LGV	HGV
AM	13.74	46.57	17.49	20.98	21.25
IP	13.63	45.51	18.18	20.98	21.25
PM	13.44	44.78	18.72	20.98	21.25

Table 9.2 - Generalised cost parameters - pence per kilometre (PPK)

PEAK	CAR – COMMUTING	Car – Employers Business	Car – Other	LGV	HGV
AM	6.70	13.38	6.70	13.66	37.35
IP	6.70	13.38	6.70	13.66	37.35
PM	6.70	13.38	6.70	13.66	37.35

- 9.1.3 Due to heavy goods vehicles favouring shorter slower routes over the longer faster routes such as trunk roads the HGV routes were looked at in greater detail.
- 9.1.4 The HGV route check looked at any roads that were unsuitable for HGV such as London Road and the appropriate ban was added to these.

## 9.2 ROUTE CHOICE VALIDATION

- 9.2.1 The routes that were chosen to validate the route choice were based on the criteria set out in TAG Unit M3.1 (January 2014):
  - Relate to significant number of trips
  - → Are of significant length or cost

- → Pass through areas of interest
- → Include both directions of travel
- → Link different compass areas
- → Coincide with journey time routes as appropriate.
- 9.2.2 Routes were plotted for all user classes. Guidance presented in section 7.3 of TAG Unit M3.1 (January 2014), with the number of OD pairs determined as follows:

Number of OD pairs =  $(number of zones)^{0.25} x number of user classes$ 

Based on the initial proposed zoning system, this equates to 14 routes. The routes that were chosen in the appraisal specification report (Sept 2015) and can be seen in Table 9.3 were used to validate the route choice.

Table 9.3 - OD route checks

Route	ORIGIN	ORIGIN NAME	DESTINATION	DESTINATION NAME
1			119	Katwijk Way, Lowestoft
2			122	Waveney Drive (between A12 & Kirkley Run)
3			130	Borrow Road, Oulton
4	102	Corton	131	Windward Way, Lowestoft
5			136	Pakefield Street, Pakefield
6			143	The Street, Carlton Colville
7			149	Kessingland
8			101	Corton Road, Gunton
9			104	Blundeston
10			113	Higher Drive, Normanston
11	149	Kessingland	114	Spashett Road, Lowestoft
12		j	120	Rotterdam Road, Lowestoft
13			122	Waveney Drive (between A12 & Kirkley Run)
14			128	A146 Beccles Road (near Burnt Hill Lane), Oulton Broad

- 9.2.3 The results of these routes can be seen in Appendix C.
- 9.2.4 The routes were assessed based on the best fit route taking particular interest in which bridge was used and if the key strategic routes were being utilised for the longer journeys.
- 9.2.5 The O-D trees in Appendix C look at user class 1 (Car Commuting) for the three time periods.
- 9.2.6 In the AM peak all the routes starting from zone 102 use a logical route. The choice of bridges is accurate especially between Corton to Pakefield (zone 102 and zone 136) and Corton to Oulton (zone 102 and zone 130) while longer trips are using the strategic links for example between Corton to Kessingland (zone 102 and zone 149) and Corton to Carlton Colville (zone 102 and zone 143). The trips between Corton and Waveney Drive (zone 102 and zone 122) use the eastern bascule bridge when either bridge would be appropriate for these trips.
- 9.2.7 The routes starting from Kessingland (zone 149) use the most strategic routes especially for longer journeys such as Kessingland to Gunton (zone 149 and zone 101) and Kessingland to Blundeston (zone 149 and zone 104). The split between the bridges is also acceptable with trips included between Kessingland to Normanston (zone 149 and zone 113) and Kessingland to Rotterdam Road (zone 149 and zone 120) uses the bridge which provides the best fit route.
- 9.2.8 The inter peak shows that some routes have multiple options with traffic using more than one route in some of the OD pairs for example between Corton to Oulton (zone 102 and zone 130) and Kessingland to Gunton (zone 149 and zone 101). The route between Kessingland to Normanston (zone 149 and zone 113) shows a split between both the eastern and western bridges.
- 9.2.9 The PM peak routes also show some route choice between certain OD pairs. All of the routes in the PM peak match the routes in either the AM peak or the interpeak if not both.
- 9.2.10 All of the routes generally remain consistent between the three peaks.
- 9.2.11 User class 2 and user class 3 (Car Employer's Business & Car Other) show the same route choices as user class 1 for all routes in the AM peak and PM peak.
- 9.2.12 The interpeak shows an increase amount of route choice for user class 2 and user class 3. These are all minor route choices and the main strategic routes remain consistent.
- 9.2.13 User class 4 (LGV) has only one small difference compared to the car user classes within the AM peak and PM peak. In the interpeak two routes show a change in local route whilst retaining the same strategic routes.
- 9.2.14 HGV (user class 5) show increased variance in their route choice which is expected. The HGV user class will prioritise distance over time as well as having to avoid banned turns and therefore show some alternative route choice.

# 10 TRIP MATRIX CALIBRATION AND VALIDATION

#### 10.1 TRIP MATRIX VALIDATION

- The initial prior matrix was created as explained in Section 7 of this report. The initial prior matrix was assigned within the model and the screenline performance analysed.
- The observed data was split into calibration and validation counts, the validation counts were not used in any matrix adjustment or matrix estimation.
- 10.1.3 Section 3.2 of TAG Unit M3.1 (January 2014) stipulates modelled flows across screenlines for each vehicle type should be within 5% of observed flows. WebTAG recommends that this should apply to "all, or nearly all" screenlines. However, due to the relatively low overall flows through the screenlines a difference between the modelled and observed flow of within 5% was considered difficult to. Therefore in this instance a GEH across the screenline of 4.0 or below has been considered in this report when looking at screenline performance. This approach is compliant with previous versions of WebTAG. We have applied a threshold of 85% of screenline totals to meet this criterion.

10.1.4 There are six screenlines which are used as part of the validation process and five which is part of the calibration process as set out in section 5 of this report. The results of the screenlines for the AM peak can be seen in Table 10.1.

Table 10.1 - Initial prior matrix screenline validation and calibration results - AM Peak

SCREENLINE		020501/52	Monsusa	Distribution	OF.II	
ID	Name	Туре	Observed	Modelled	DIFFERENCE	GEH
1	Screenline 1 - NB	Calibration	1,304	761	-42%	16.893
2	Screenline 1 - SB	Calibration	1,032	1,019	-1%	0.419
3	Screenline 2 - NB	Calibration	959	1,007	5%	1.525
4	Screenline 2 - SB	Calibration	933	781	-16%	5.202
5	Screenline 3 - NB	Calibration	1,082	1,233	14%	4.434
6	Screenline 3 - SB	Calibration	824	833	1%	0.330
7	Screenline 4 - NB	Calibration	1,086	965	-11%	3.778
8	Screenline 4 - SB	Calibration	705	761	8%	2.078
9	Screenline 5 - EB	Calibration	440	380	-14%	2.982
10	Screenline 5 - WB	Calibration	313	224	-28%	5.438
11	Screenline 6 - EB	Calibration	1,749	1,703	-3%	1.109
12	Screenline 6 - WB	Calibration	1,200	917	-24%	8.691
13	Screenline 7 - EB	Calibration	660	1,199	82%	17.694
14	Screenline 7 - WB	Calibration	687	1,075	56%	13.055
15	Screenline 8 - NB	Calibration	1,585	1,702	7%	2.883
16	Screenline 8 - SB	Calibration	1,096	1,364	24%	7.644
19	Screenline 9 - NB	Validation	2,475	2,682	8%	4.076
20	Screenline 9 - SB	Validation	1,802	1,959	9%	3.620
21	Screenline 10 - NB	Validation	1,639	1,895	16%	6.096
22	Screenline 10 - SB	Validation	1,373	1,586	16%	5.543

## 10.1.5 The results for the Interpeak can be seen in Table 10.2.

Table 10.2: Initial prior matrix screenline validation and calibration results - Inter Peak

SCREENLINE		Opernyen	Modelled	Difference	GEH		
ID	Name	Туре	Observed	IVIODELLED	DIFFERENCE	GLII	
1	Screenline 1 - NB	Calibration	963	470	-51%	18.406	
2	Screenline 1 - SB	Calibration	935	695	-26%	8.411	
3	Screenline 2 - NB	Calibration	884	718	-19%	5.852	
4	Screenline 2 - SB	Calibration	864	667	-23%	7.136	
5	Screenline 3 - NB	Calibration	1,086	1,247	15%	4.720	
6	Screenline 3 - SB	Calibration	1,200	981	-18%	6.621	
7	Screenline 4 - NB	Calibration	788	587	-25%	7.659	
8	Screenline 4 - SB	Calibration	814	782	-4%	1.142	
9	Screenline 5 - EB	Calibration	367	193	-47%	10.407	
10	Screenline 5 - WB	Calibration	398	300	-25%	5.254	
11	Screenline 6 - EB	Calibration	1,353	1,190	-12%	4.578	
12	Screenline 6 - WB	Calibration	1,391	752	-46%	19.530	
13	Screenline 7 - EB	Calibration	609	1,089	79%	16.491	
14	Screenline 7 - WB	Calibration	610	955	57%	12.328	
15	Screenline 8 - NB	Calibration	1,257	1,239	-1%	0.511	
16	Screenline 8 - SB	Calibration	1,304	1,456	12%	4.085	
19	Screenline 9 - NB	Validation	2,024	1,944	-4%	1.803	
20	Screenline 9 - SB	Validation	1,982	2,126	7%	3.181	
21	Screenline 10 - NB	Validation	1,365	1,512	11%	3.864	
22	Screenline 10 - SB	Validation	1,385	1,615	17%	5.942	

## 10.1.6 The screenline results for the PM peak can be seen in Table 10.3.

Table 10.3 - Initial prior matrix screenline validation and calibration results - PM Peak

SCREENLINE		Observed	Modelled	Difference	GEH	
ID	Name	Туре	OBSERVED	IVIODELLED	DIFFERENCE	GER
1	Screenline 1 - NB	Calibration	1,294	751	-42%	16.969
2	Screenline 1 - SB	Calibration	1,450	1,005	-31%	12.704
3	Screenline 2 - NB	Calibration	1,088	985	-9%	3.199
4	Screenline 2 - SB	Calibration	1,212	1,003	-17%	6.287
5	Screenline 3 - NB	Calibration	1,031	1,586	54%	15.353
6	Screenline 3 - SB	Calibration	1,257	1,413	12%	4.265
7	Screenline 4 - NB	Calibration	764	615	-20%	5.676
8	Screenline 4 - SB	Calibration	1,136	1,013	-11%	3.756
9	Screenline 5 - EB	Calibration	404	278	-31%	6.823
10	Screenline 5 - WB	Calibration	650	472	-27%	7.502
11	Screenline 6 - EB	Calibration	1,470	1,618	10%	3.757
12	Screenline 6 - WB	Calibration	1,783	1,340	-25%	11.214
13	Screenline 7 - EB	Calibration	938	1,294	38%	10.648
14	Screenline 7 - WB	Calibration	690	1,086	57%	13.271
15	Screenline 8 - NB	Calibration	1,443	1,434	-1%	0.234
16	Screenline 8 - SB	Calibration	1,624	1,999	23%	8.817
19	Screenline 9 - NB	Validation	2,218	2,354	6%	2.844
20	Screenline 9 - SB	Validation	2,724	2,988	10%	4.940
21	Screenline 10 - NB	Validation	1,753	1,854	6%	2.367
22	Screenline 10 - SB	Validation	1,713	2,049	20%	7.748

#### 10.2 TRIP MATRIX CALIBRATION

#### ADJUSTED PRIOR MATRIX

- To improve on these results scaling was used on a selection of the calibration counts to produce an adjusted prior matrix. This looked at the difference between the modelled and observed data and adjusted the matrix to either add or remove trips between OD pairs which used those routes.
- The counts on the eastern and western bridge were not scaled as these already had acceptable GEH values and could act as a check that the matrix was not being distorted by the scaling process.
- Table 10.4 shows the number of trips in each user class for the initial and adjusted prior matrix.

Table 10.4 - Pre and post prior matrix adjustment trip totals

USER CLASS	AM PEAK HOUR (08:00-09:00)		INTER PEAK (10:00-	Avg. Hour -16:00)	PM PEAK HOUR (17:00-18:00)	
	INITIAL PRIOR	ADJ PRIOR	INITIAL PRIOR	ADJ PRIOR	INITIAL PRIOR	ADJ PRIOR
UC1 – Car Commuting	6,716	5,735	1,970	1,724	4,631	4,019
UC2 – Car EmpBus	741	646	723	693	1,034	932
UC3 – Car Other	3,529	3,491	6,513	6,183	6,850	6,166
UC4 – LGV	1,083	2,454	948	2,760	1,011	3,019
UC5 – HGV	287	842	292	814	145	416
Total	12,355	13,167	10,447	12,174	13,672	14,553

Table 10.5 to Table 10.7 show the screenline performance of the adjusted prior matrix. These results show a major improvement in how the modelled flows match the observed screenlines, with the majority of screenlines showing a GEH of 4.0 or below.

Table 10.5 - Adjusted prior matrix screenline validation and calibration results - AM Peak

SCREENLINE		Opospysp	Modelled	Difference	CEH	
ID	Name	Туре	Observed Modelled I		DIFFERENCE	GEH
1	Screenline 1 - NB	Calibration	1,304	1,157	-11%	4.185
2	Screenline 1 - SB	Calibration	1,032	1,352	31%	9.256
3	Screenline 2 - NB	Calibration	959	897	-6%	2.041
4	Screenline 2 - SB	Calibration	933	951	2%	0.576
5	Screenline 3 - NB	Calibration	1,082	960	-11%	3.823
6	Screenline 3 - SB	Calibration	824	840	2%	0.572
7	Screenline 4 - NB	Calibration	1,086	1,003	-8%	2.568
8	Screenline 4 - SB	Calibration	705	723	3%	0.683
9	Screenline 5 - EB	Calibration	440	422	-4%	0.886
10	Screenline 5 - WB	Calibration	313	263	-16%	2.953
11	Screenline 6 - EB	Calibration	1,749	1,701	-3%	1.157
12	Screenline 6 - WB	Calibration	1,200	1,232	3%	0.925
13	Screenline 7 - EB	Calibration	660	747	13%	3.296
14	Screenline 7 - WB	Calibration	687	695	1%	0.287
15	Screenline 8 - NB	Calibration	1,585	1,503	-5%	2.090
16	Screenline 8 - SB	Calibration	1,096	1,075	-2%	0.634
19	Screenline 9 - NB	Validation	2,475	2,370	-4%	2.133
20	Screenline 9 - SB	Validation	1,802	1,812	1%	0.235
21	Screenline 10 - NB	Validation	1,639	1,540	-6%	2.477
22	Screenline 10 - SB	Validation	1,373	1,289	-6%	2.297

Table 10.6 - Adjusted prior matrix screenline validation and calibration results - Inter Peak

SCREENLINE		0	NA	<b>D</b>	OFIL	
ID	Name	Туре	Observed	Modelled	DIFFERENCE	GEH
1	Screenline 1 - NB	Calibration	963	1,076	12%	3.551
2	Screenline 1 - SB	Calibration	935	918	-2%	0.562
3	Screenline 2 - NB	Calibration	884	996	13%	3.666
4	Screenline 2 - SB	Calibration	864	943	9%	2.613
5	Screenline 3 - NB	Calibration	1,086	1,117	3%	0.940
6	Screenline 3 - SB	Calibration	1,200	1,163	-3%	1.066
7	Screenline 4 - NB	Calibration	788	697	-12%	3.332
8	Screenline 4 - SB	Calibration	814	828	2%	0.480
9	Screenline 5 - EB	Calibration	367	281	-23%	4.786
10	Screenline 5 - WB	Calibration	398	422	6%	1.177
11	Screenline 6 - EB	Calibration	1,353	1,162	-14%	5.393
12	Screenline 6 - WB	Calibration	1,391	1,386	0%	0.144
13	Screenline 7 - EB	Calibration	609	697	15%	3.462
14	Screenline 7 - WB	Calibration	610	642	5%	1.273
15	Screenline 8 - NB	Calibration	1,257	1,360	8%	2.846
16	Screenline 8 - SB	Calibration	1,304	1,419	9%	3.110
19	Screenline 9 - NB	Validation	2,024	1,899	-6%	2.830
20	Screenline 9 - SB	Validation	1,982	2,181	10%	4.366
21	Screenline 10 - NB	Validation	1,365	1,350	-1%	0.418
22	Screenline 10 - SB	Validation	1,385	1,281	-8%	2.845

Table 10.7 - Adjusted prior matrix screenline validation and calibration results - PM Peak

Screenline		020501/52	<b>N</b> 4	D:====	OF.II	
ID	Name	Туре	Observed	Modelled	DIFFERENCE	GEH
1	Screenline 1 - NB	Calibration	1,294	1,385	7%	2.499
2	Screenline 1 - SB	Calibration	1,450	1,180	-19%	7.448
3	Screenline 2 - NB	Calibration	1,088	1,142	5%	1.618
4	Screenline 2 - SB	Calibration	1,212	1,235	2%	0.650
5	Screenline 3 - NB	Calibration	1,031	1,071	4%	1.244
6	Screenline 3 - SB	Calibration	1,257	1,268	1%	0.305
7	Screenline 4 - NB	Calibration	764	719	-6%	1.654
8	Screenline 4 - SB	Calibration	1,136	1,126	-1%	0.301
9	Screenline 5 - EB	Calibration	404	404	0%	0.000
10	Screenline 5 - WB	Calibration	650	596	-8%	2.150
11	Screenline 6 - EB	Calibration	1,470	1,357	-8%	3.015
12	Screenline 6 - WB	Calibration	1,783	1,692	-5%	2.186
13	Screenline 7 - EB	Calibration	938	1,006	7%	2.172
14	Screenline 7 - WB	Calibration	690	640	-7%	1.957
15	Screenline 8 - NB	Calibration	1,443	1,483	3%	1.049
16	Screenline 8 - SB	Calibration	1,624	1,682	4%	1.433
19	Screenline 9 - NB	Validation	2,218	2,203	-1%	0.319
20	Screenline 9 - SB	Validation	2,724	2,765	2%	0.783
21	Screenline 10 - NB	Validation	1,753	1,608	-8%	3.548
22	Screenline 10 - SB	Validation	1,713	1,529	-11%	4.570

#### 10.3 TRIP MATRIX ESTIMATION

- The matrix estimation process employed as part of the calibration process is designed to modify the travel patterns using the observed traffic counts. Trips are adjusted in the matrix to produce the estimated matrix, which is most likely to be consistent with the traffic counts. The matrix of trips input to matrix estimation is known as the prior matrix, while the output matrix from matrix estimation is known as the post matrix. The calibration process has used matrix estimation procedures as contained in the SATME2 program in the SATURN suite of software.
- SATME2 requires a PIJA file which represents the proportion (P) of trips between a particular origin-destination pair (IJ) which uses the counted link (A). The PIJA data is obtained through the program SATPIJA following a SATURN assignment using the SAVEIT option.
- This produces PIJA output files for each user class which are used by SATME2 along with the prior matrix to produce an updated 2015 estimated highway demand matrices which were then combined into a 'stacked' estimated matrix for assignment. No cells were frozen and there were no zonal constraints applied.
- Matrix estimation often involves an iterative process, where the first post matrix is assigned to the network and is used to update assignment costs, creating a new set of PIJA factors to create a second post matrix. This process can continue to be repeated, updating assignment costs but retaining the original prior matrix each time to prevent undue distortion of observed trip patterns. The benefit of this approach is that the post matrix will contain a better representation of the PIJA factors on counted links than the prior matrix assignment, which should result in an improved post matrix the second time around.
- 10.3.5 Further iterations can be undertaken, but typically after 3 or 4 iterations the additional benefits in terms of improved goodness of fit are small. There are no specific convergence criteria for matrix estimation, but the aim of the procedure is to improve the goodness of fit between modelled flows and counts.
- 10.3.6 The matrix estimation was carried out using the calibration counts only based on the scaled matrices for each time period.

Table 10.8 compares the matrix totals for the adjusted prior and post matrix estimation matrices for each modelled peak hour by user class. Overall, following matrix estimation, the matrix increased by 0.76% in the AM peak, there was a decrease of 1% in the inter peak and an increase of 0.87% in the PM peak.

**Table 10.8: Prior and Post Matrix Totals** 

User Class	AM PEAK HOUR (0800-0900)		INTER PEAK (1000-		PM PEAK HOUR (1700-1800)	
	ADJ PRIOR	Post ME	Adj Prior	Роѕт МЕ	Adj Prior	Post ME
UC1 – Car Commuting	5,735	5,447	1,724	1,696	4,019	3,964
UC2 – Car EmpBus	646	622	693	658	932	904
UC3 – Car Other	3,491	3,474	6,183	5,954	6,166	6,141
UC4 – LGV	2,454	2,855	2,760	2,919	3,019	3,215
UC5 – HGV	842	868	814	825	416	456
Total	13,167	13,267	12,174	12,052	14,553	14,680

10.3.8 Appendix D contains a breakdown of the individual count performance within the screenlines for the final post-ME assignment.

10.3.9 Table 10.9 to Table 10.11 detail the screenline performance of the post ME assignment.

Table 10.9: Post ME screenline validation and calibration results - AM Peak

	SCREENLINE		OBSERVED	Modelled	DIFFERENCE	GEH
ID	Name	Type				
1	Screenline 1 - NB	Calibration	1,304	1,277	-2%	0.746
2	Screenline 1 - SB	Calibration	1,032	1,139	10%	3.235
3	Screenline 2 - NB	Calibration	959	960	0%	0.027
4	Screenline 2 - SB	Calibration	933	937	0%	0.121
5	Screenline 3 - NB	Calibration	1,082	1,085	0%	0.086
6	Screenline 3 - SB	Calibration	824	795	-3%	1.002
7	Screenline 4 - NB	Calibration	1,086	1,041	-4%	1.380
8	Screenline 4 - SB	Calibration	705	693	-2%	0.444
9	Screenline 5 - EB	Calibration	440	438	-1%	0.114
10	Screenline 5 - WB		313	298	-5%	0.864
11	Screenline 6 - EB	Calibration	1,749	1,599	-9%	3.668
12	Screenline 6 - WB	Calibration	1,200	1,238	3%	1.096
13	Screenline 7 - EB	Calibration	660	644	-2%	0.611
14	Screenline 7 - WB		687	688	0%	0.020
15	Screenline 8 - NB	Calibration	1,585	1,581	0%	0.103
16	Screenline 8 - SB	Calibration	1,096	1,097	0%	0.033
19	Screenline 9 - NB	Validation	2,475	2,368	-4%	2.174
20	Screenline 9 - SB	Validation	1,802	1,670	-7%	3.168
21	Screenline 10 - NB	Validation	1,639	1,518	-7%	3.040
22	Screenline 10 - SB	Validation	1,373	1,293	-6%	2.186

Table 10.10: Post ME screenline validation and calibration results - Inter Peak

	SCREENLINE		OBSERVED	Modelled	DIFFERENCE	GEH
ID	Name	Type				
1	Screenline 1 - NB	Calibration	963	926	-4%	1.192
2	Screenline 1 - SB	Calibration	935	894	-4%	1.360
3	Screenline 2 - NB	Calibration	884	887	0%	0.114
4	Screenline 2 - SB	Calibration	864	907	5%	1.430
5	Screenline 3 - NB	Calibration	1,086	1,127	4%	1.238
6	Screenline 3 - SB	Calibration	1,200	1,198	0%	0.047
7	Screenline 4 - NB	Calibration	788	764	-3%	0.854
8	Screenline 4 - SB	Calibration	814	781	-4%	1.177
9	Screenline 5 - EB	Calibration	367	368	0%	0.044
10	Screenline 5 - WB	Calibration	398	400	0%	0.092
11	Screenline 6 - EB	Calibration	1,353	1,289	-5%	1.768
12	Screenline 6 - WB	Calibration	1,391	1,381	-1%	0.278
13	Screenline 7 - EB	Calibration	609	627	3%	0.742
14	Screenline 7 - WB	Calibration	610	612	0%	0.075
15	Screenline 8 - NB	Calibration	1,257	1,291	3%	0.951
16	Screenline 8 - SB	Calibration	1,304	1,305	0%	0.021
19	Screenline 9 - NB	Validation	2,024	1,912	-6%	2.532
20	Screenline 9 - SB	Validation	1,982	2,064	4%	1.827
21	Screenline 10 - NB	Validation	1,365	1,285	-6%	2.209
22	Screenline 10 - SB	Validation	1,385	1,228	-11%	4.340

Table 10.11: Post ME screenline validation and calibration results - PM Peak

	SCREENLINE		OBSERVED	Modelled	DIFFERENCE	GEH
ID	Name	Type				
1	Screenline 1 - NB	Calibration	1,294	1,324	2%	0.842
2	Screenline 1 - SB	Calibration	1,450	1,368	-6%	2.187
3	Screenline 2 - NB	Calibration	1,088	1,092	0%	0.122
4	Screenline 2 - SB	Calibration	1,212	1,256	4%	1.245
5	Screenline 3 - NB	Calibration	1,031	999	-3%	0.994
6	Screenline 3 - SB	Calibration	1,257	1,229	-2%	0.798
7	Screenline 4 - NB	Calibration	764	749	-2%	0.547
8	Screenline 4 - SB	Calibration	1,136	1,102	-3%	1.020
9	Screenline 5 - EB	Calibration	404	399	-1%	0.250
10	Screenline 5 - WB	Calibration	650	623	-4%	1.057
11	Screenline 6 - EB	Calibration	1,470	1,332	-9%	3.697
12	Screenline 6 - WB	Calibration	1,783	1,755	-2%	0.669
13	Screenline 7 - EB	Calibration	938	951	1%	0.414
14	Screenline 7 - WB	Calibration	690	673	-3%	0.669
15	Screenline 8 - NB	Calibration	1,443	1,480	3%	0.971
16	Screenline 8 - SB	Calibration	1,624	1,699	5%	1.846
19	Screenline 9 - NB	Validation	2,218	2,185	-1%	0.703
20	Screenline 9 - SB	Validation	2,724	2,600	-5%	2.403
21	Screenline 10 - NB	Validation	1,753	1,570	-10%	4.501
22	Screenline 10 - SB	Validation	1,713	1,477	-14%	5.909

- 10.3.10 In the AM peak, all screenlines are shown to perform well with a GEH below 4.
- The interpeak performs similarly with all the calibration screenlines achieving a GEH of less than 4. Screenline 10 southbound does not meet these criteria is close with a GEH value of 4.340.
- The PM peak again has all the calibration screenlines meeting the criteria whilst validation screenline 10 is slightly over with a GEH of 4.501 in the northbound direction. In the southbound direction, screenline 10 has a higher GEH of 5.909. This is due to ATC 10 (A146 Beccles Road) showing a high GEH in the south-west bound direction. The other two ATCs (ATC 5 on A1145 Castleton and A12 London Road) show the modelled flow closely matches the observed flow with GEH of 0.3 and 2.2 respectively.
- 10.3.13 Overall the screenline results echo the results of the link flows in indicating that the model represents and accurately reflects the observed data and indicates that the key movements around the model are accurate.

### IMPACT OF MATRIX ESTIMATION

- 10.3.14 It is important to look at the different in the trip length distribution between the adjusted prior matrix assignment and post ME matrix assignment.
- Figure 10.1, Figure 10.2 and Figure 10.3 show the trip length distributions for each peak hour model graphically comparing the adjusted prior assignment to the post matrix estimation assignment. The graphs show matrix estimation does not fundamentally alter the trip length distribution between the two assignments.

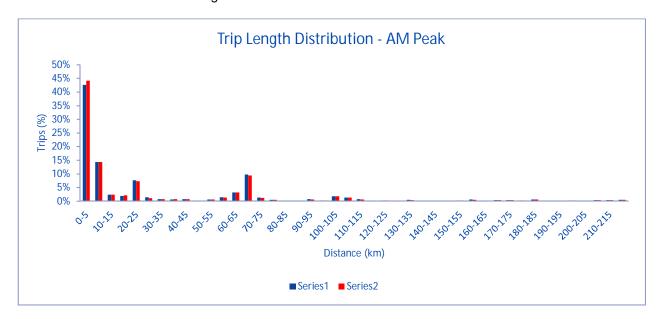


Figure 10.1: AM peak trip length distribution

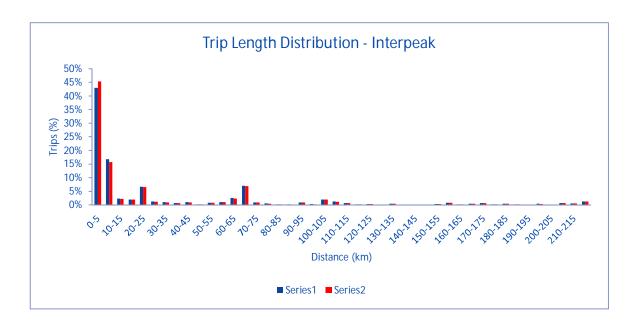


Figure 10.2: Inter peak trip length distribution

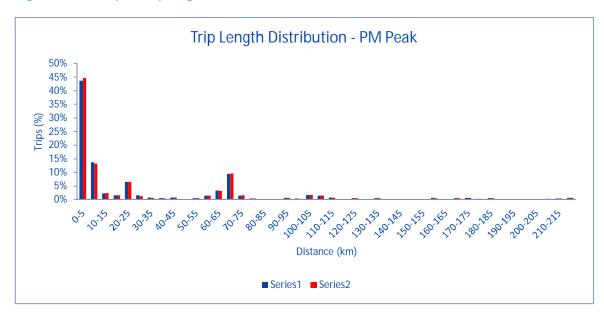


Figure 10.3: PM peak trip length distribution

**Table 10.12: Regression statistics AM Peak** 

MEASUI	REMENT	REQUIREMENT	Value	Pass?
Slope		Within 0.98 and 1.02	0.965	No
Cells	Intercept	Near 0	0.035	Yes
	R-Sq	> 0.95	0.8341	No
	Slope	Within 0.99 and 1.01	1.007	Yes
Rows	Intercept	Near 0	0.019	Yes
	R-Sq	> 0.98	0.9752	No
	Slope	Within 0.99 and 1.01	0.938	No
Columns	Intercept	Near 0	7.221	No
	R-Sq	> 0.98	0.9569	No
	Prior		32.033	
Mean	Post	Within 5%	Within 5% 30.914	
	Diff		3.5%	
0.0	Prior	W	54.763	V
SD	Post	Within 5%	54.353	Yes
	Diff		0.7%	

**Table 10.13: Regression statistics Inter Peak** 

MEASUF	REMENT	REQUIREMENT	VALUE	Pass?
	Slope Within 0.98 and 1.02		0.944	No
Cells	Intercept	Near 0	0.034	Yes
	R-Sq	> 0.95	Near 0 0.944  Near 0 0.934  > 0.95 0.9304  ithin 0.99 and 1.01 0.96  Near 0 2.876  > 0.98 0.99	No
	Slope	Within 0.99 and 1.01	0.96	No
Rows	Intercept	Near 0	2.876	No
	R-Sq	> 0.98	0.99	Yes
	Slope	Within 0.99 and 1.01	0.959	No
Columns	Intercept	Near 0	2.942	No
	R-Sq	> 0.98	0.9854	Yes
	Prior		33.083	
Mean	Post	Within 5%	31.943	Yes
	Diff		3.4%	
	Prior		57.523	
SD	Post	Within 5%	54.353	Yes
	Diff		0.7%	

Table 10.14: Regression statistics PM Peak

Measur	REMENT	REQUIREMENT	VALUE	Pass?
	Slope Within 0.98 and 1.02		0.989	Yes
Cells	Intercept	Near 0	0.02	Yes
	R-Sq	> 0.95	0.8325	No
	Slope	Within 0.99 and 1.01	0.959	No
Rows	Intercept	Near 0	5.983	No
	R-Sq	> 0.98	0.9782	No
	Slope	Within 0.99 and 1.01	1.036	No
Columns	Intercept	Near 0	-2.913	No
	R-Sq	> 0.98	0.975	No
	Prior		32.999	
Mean	Post	Within 5%	32.688	Yes
	Diff		0.9%	
	Prior		52.491	
SD	Post	Within 5%	Within 5% 52.143	
	Diff		0.7%	

10.3.16 The regression statistics show that for all three time periods both the mean and standard deviation are both within the criteria of 5%.

- 10.3.17 The sector to sector movements were analysed to ensure the matrix estimation process did not distort the matrix.
- 10.3.18 Table 10.15 shows the percentage difference in sector to sector movements for the AM peak.

Table 10.15: Sector to sector movement results - AM Peak

	1	2	3	4	5	TOTAL	
1	0%	-13%	0%	0%	-4%	-2%	
2	0%	-10%	-8%	-9%	11%	-3%	
3	0%	-6%	0%	9%	-7%	2%	
4	-6%	-4%	-7%	4%	-11%	-2%	
5	2%	2%	-18%	8%	8%	5%	
Total	-2%	-3%	-9%	4%	1%	1%	

10.3.19 The interpeak results can be seen in Table 10.16.

Table 10.16: Sector to sector movement results - Inter Peak

	1	2	3	4	5	TOTAL
1	0%	-6%	0%	2%	-13%	-3%
2	0%	-5%	-5%	-6%	-3%	-5%
3	-3%	-7%	0%	3%	-10%	-2%
4	-6%	-9%	-2%	1%	-5%	-2%
5	-6%	-3%	-12%	5%	3%	2%
Total	-5%	-6%	-4%	2%	-2%	-1%

10.3.20 The results for the PM peak can be seen in Table 10.17.

Table 10.17: Sector to sector movement results - PM Peak

	1	2	3	4	5	TOTAL
1	0%	-8%	0%	-1%	-15%	-5%
2	10%	2%	4%	-12%	-2%	-5%
3	0%	-9%	0%	9%	-18%	-3%
4	7%	-2%	6%	5%	-2%	2%
5	7%	7%	6%	0%	3%	3%
Total	6%	-1%	5%	3%	-2%	1%

### 11 ASSIGNMENT CALIBRATION AND VALIDATION

### 11.1 MODEL CONVERGENCE

- 11.1.1 The model convergence criterion has been set out in Section 3.2.
- 11.1.2 Table 11.1, table 11.2 and table 11.3 show the convergence statistics for the AM peak, interpeak and PM peak respectively. The results show that all the models converge within the guidance that was set out in Table 3.4.

Table 11.1 - AM peak convergence results

ITERATION	DELTA	%FLOW	%Сар
11	0.0006	95.4	0.00045
12	0.0002	96.8	0.00026
13	0.0001	98.4	0.00023
14	0.0001	99	0.00013
15	0.0002	99.6	0.00009
16	0.0001	99.5	0.00006

Table 11.2 - Inter peak convergence results

ITERATION	DELTA	%FLOW	%Сар
9	0.0136	95.3	0.01
10	0.0071	97.3	0.012
11	0.0083	98.4	0.0064
12	0.0046	99.2	0.008
13	0.0062	99.1	0.0043
14	0.0033	99.4	0.0058

Table 11.3 - PM peak convergence results

İTERATION	DELTA	%FLOW	%САР
26	0.0016	99.5	0.0042
27	0.0044	97.2	0.0017
28	0.0011	98.3	0.0018
29	0.0015	99.1	0.0027
30	0.0017	99.8	0.00089
31	0.0009	98.5	0.0013

### 11.2 ASSIGNMENT CALIBRATION

- 11.2.1 Assignment calibration involved steps to identify any issues that prevented an acceptable level of calibration of the network, route choice and trip matrix. This will included:
  - → Checking appropriateness of centroid connectors
  - → Production of forests to understand nature of competing routes between OD pairs
  - → Checking representation of queues on surveyed journey time routes

### 11.3 ASSIGNMENT VALIDATION

Link flow validation and calibration results for the final post-matrix estimation show an improved situation compared to the scaled matrix.

### **OVERALL MODEL PERFORMANCE**

11.3.2 The calibration and validation results for all user classes in the AM peak are shown in table 11.4. The results for the car as an individual user class are shown in table 11.5.

Table 11.4 - AM Peak hour all user classes calibration and validation results

Criteria and Measure		ACCEPTABILITY	(	Calibration			Validation		
		Guideline	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%	
			Flow C	riteria					
< 700 vph	±100 vph	> 85 % of links	43	43	100%	38	32	84%	
700 - 2,700 vph	±15%	> 85 % of links	3	3	100%	5	5	100%	
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%	
GEH Criteria									
GEH Statistic f		> 85 % of links	46	46	100%	43	36	84%	

11.3.3 The AM peak results show that 100% of the calibration links and 84% of the validation links pass the criteria set out in WebTAG to achieve GEH values with a value of less than 5. The car only results show a very similar pattern.

Table 11.5 - AM Peak hour car only calibration and validation results

Criteria and Measure		Acceptability		Calibration			Validation		
		GUIDELINE	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%	
			Flow C	riteria					
< 700 vph	±100 vph	> 85 % of links	44	44	100%	43	38	88%	
700 - 2,700 vph	±15%	> 85 % of links	2	2	100%	0	0	0%	
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%	
GEH Criteria									
GEH Statistic for individual links < 5 > 85 % of links			46	46	100%	43	36	84%	

11.3.4 The interpeak results for all user classes can be seen in Table 11.6 whilst car only is seen in Table 11.7.

Table 11.6 - Inter Peak hour all user classes calibration and validation results

		Acceptability	ı	Calibration	I	Validation			
CRITERIA AND MEASURE		Guideline	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%	
			Flow C	riteria					
< 700 vph	±100 vph	> 85 % of links	44	44	100%	39	34	87%	
700 - 2,700 vph	±15%	> 85 % of links	2	2	100%	4	4	100%	
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%	
	GEH Criteria								
GEH Statistic for individual links < 5		> 85 % of links	46	46	100%	43	38	88%	

The Interpeak results show that both the calibration and validation counts have at least 85% of links with a GEH value of less than 5. However, for cars the validation percentage is at 79% of links with a GEH below 5. This is not considered an issue as in terms of flow validation the car user class is at 88% of links within 100 pcus of the observed count.

Table 11.7 - Inter Peak hour car only calibration and validation results

		Acceptability		CALIBRATION	I	VALIDATION			
Criteria and Measure		Guideline	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%	
			Flow C	riteria					
< 700 vph	±100 vph	> 85 % of links	44	44	100%	42	37	88%	
700 - 2,700 vph	±15%	> 85 % of links	2	2	100%	1	0	0%	
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%	
	GEH Criteria								
GEH Statistic for individual links < 5		> 85 % of links	46	46	100%	43	34	79%	

11.3.6 The PM results below show that all of the calibration links have a GEH of less than 5. The car only also shows a good level of calibration and can be seen in Table 11.9. In terms of validation, 77% of links have a GEH below 5 which is marginally outside of WebTAG criteria.

Table 11.8 - PM Peak hour all user classes calibration and validation results

		ACCEPTABILITY		Calibration			Validation		
Criteria and Measure		GUIDELINE	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%	
			Flow C	riteria					
< 700 vph	±100 vph	> 85 % of links	38	38	100%	37	28	76%	
700 - 2,700 vph	±15%	> 85 % of links	8	8	100%	6	5	83%	
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%	
GEH Criteria									
GEH Statistic for individual links < 5		> 85 % of links	46	46	100%	43	33	77%	

Table 11.9 - PM peak hour car only calibration and validation results

		ACCEPTABILITY		Calibration			VALIDATION			
Criteria and Measure		GUIDELINE	Total Counts	Meet Criteria	%	Total Counts	Meet Criteria	%		
			Flow C	riteria						
< 700 vph	±100 vph	> 85 % of links	44	44	100%	40	33	83%		
700 - 2,700 vph	±15%	> 85 % of links	2	2	100%	3	3	100%		
> 2,700 vph	±400 vph	> 85 % of links	0	0	0%	0	0	0%		
	GEH Criteria									
GEH Statistic for individual links < 5		> 85 % of links	46	44	96%	43	36	84%		

- 11.3.7 The matrix estimation process has increased the calibration counts to 100% of links having a GEH value of less than 5 for all three peaks. Despite the percentage of validation counts with a GEH below 5 not reaching 85% across all three peaks, the model is considered to be matched well to the observed data as taking the calibration and validation counts combined, the percentage of links with a GEH is at 92% for the AM peak, 94% for the interpeak and 89% for the PM peak
- 11.3.8 Table 11.10, table 11.11 and table 11.12 show the GEH breakdown for AM peak, interpeak and PM peak respectively.

Table 11.10 - AM Peak GEH summary

GEH RANGE	Calibration		V۵	VALIDATION		OMBINED
GEH < 2	40	87%	19	44%	59	66%
GEH < 4	44	96%	34	79%	78	88%
GEH < 6	46	100%	37	86%	83	93%
GEH < 8	46	100%	41	95%	87	98%
GEH < 10	46	100%	41	95%	87	98%
GEH <5	46	100%	36	84%	82	92%

Table 11.11 - Inter Peak GEH summary

GEH RANGE	Calibr	CALIBRATION VALIDATION		LIDATION	COMBINED	
GEH < 2	42	91%	25	58%	67	75%
GEH < 4	46	100%	34	79%	80	90%
GEH < 6	46	100%	39	91%	85	96%
GEH < 8	46	100%	40	93%	86	97%
GEH < 10	46	100%	40	93%	86	97%
GEH <5	46	100%	38	88%	84	94%

Table 11.12 - PM Peak GEH summary

GEH RANGE	Calibration		VA	VALIDATION		OMBINED
GEH < 2	36	78%	17	40%	53	60%
GEH < 4	44	96%	30	70%	74	83%
GEH < 6	46	100%	36	84%	82	92%
GEH < 8	46	100%	37	86%	83	93%
GEH < 10	46	100%	39	91%	85	96%
GEH <5	46	100%	33	77%	79	89%

- 11.3.9 The GEH summaries show that all three peaks have at least 85% of the combined counts have a GEH value of less than 5. These results show that the model is well validated and calibrated.
- 11.3.10 Appendix E contains all link counts used for validation and calibration. Plots are also provided showing the GEH performance of counts near the bridge crossings.

### JOURNEY TIME PERFORMANCE

- 11.3.11 Appendix F contains journey time graphs across all three time periods.
- 11.3.12 The journey time routes which can be seen in Figure 5.7 also indicate that the model reflects the observed data.
- 11.3.13 A summary of the modelled journey times compared to the observed is given for the AM peak in table 11.13.

Table 11.13 - AM peak journey time route comparison

ID	Name	OBSERVED (S)	MODELLED (S)	DIFF	%	Pass?
1	1 - Northbound	341	367	-26	-8%	Yes
2	1 - Southbound	367	338	29	8%	Yes
3	2 - Northbound	521	583	-62	-12%	Yes
4	2 - Southbound	599	538	61	10%	Yes
5	3 - Eastbound	290	308	-17	-6%	Yes
6	3 - Westbound	289	287	2	1%	Yes
7	4 - Northbound	216	183	33	15%	Yes
8	4 - Southbound	222	187	36	16%	Yes
9	5 - Northbound	637	648	-11	-2%	Yes
10	5 - Southbound	553	537	16	3%	Yes
11	6 - Eastbound	689	608	81	12%	Yes
12	6 - Westbound	598	541	57	10%	Yes
13	7 - Eastbound	449	419	30	7%	Yes
14	7 - Westbound	391	344	46	12%	Yes
15	8 - Eastbound	723	698	25	3%	Yes
16	8 - Westbound	712	725	-13	-2%	Yes
17	9 - Northbound	462	354	107	23%	No
18	9 - Southbound	390	332	57	15%	Yes

- The results show that seventeen of the eighteen journey times pass the criteria set out in Table 3.3. Journey time route 9 in the northbound direction is marginally outside the required criteria. Along the majority of this route the modelled travel time matches well to the observed travel time, the section between the A146 Beccles Road / Cotmer Road signals and western Mutford Bridge is shown to be modelled faster compared to the observed data leading to the journey time route falling outside the 15% band.
- Table 11.14 shows that sixteen of the eighteen journey times pass the criteria in the inter peak. Both routes outside the criteria are shown in the journey time graphs to generally match well between the modelled travel time and observed travel time for the majority of the route.

Table 11.14 - Inter peak journey time route comparison

ID	Name	OBSERVED (S)	MODELLED (S)	DIFF	%	Pass?
1	1 - Northbound	345	341	3	1%	Yes
2	1 - Southbound	373	331	42	11%	Yes
3	2 - Northbound	549	506	42	8%	Yes
4	2 - Southbound	669	526	143	21%	No
5	3 - Eastbound	305	340	-35	-11%	Yes
6	3 - Westbound	369	317	52	14%	Yes
7	4 - Northbound	216	185	31	14%	Yes
8	4 - Southbound	210	188	23	11%	Yes
9	5 - Northbound	846	821	25	3%	Yes
10	5 - Southbound	600	540	60	10%	Yes
11	6 - Eastbound	705	718	-13	-2%	Yes
12	6 - Westbound	646	539	107	17%	No
13	7 - Eastbound	396	419	-24	-6%	Yes
14	7 - Westbound	394	351	43	11%	Yes
15	8 - Eastbound	721	707	15	2%	Yes
16	8 - Westbound	745	738	7	1%	Yes
17	9 - Northbound	430	377	52	12%	Yes
18	9 - Southbound	346	329	17	5%	Yes

- 11.3.16 The results of the PM peak journey times can be seen in Table 11.15. Journey time route 1 southbound is shown to be marginally outside the required criteria.
- Journey time route 3 westbound is outside the criteria, however the modelled journey time along this route is relatively consistent along this route across all three peaks, however there are notable differences in the observed journey time along this route. The section of the route between Peto Way and the western Mutford Bridge is shown to be modelled faster in the model compared to the observed data.
- Journey time route 9 shows a notable increase the observed journey time in the PM peak, whereas the modelled journey time remains relatively consistent between the three peaks. The PM peak model does capture some of the delay along this route, with this route slowest in the PM peak model. The section of the route on the A12 Bloodmoor Road between the A12 Tower Road and A12 Tom Crisp Way shows a delay in the observed data which is not fully replicated in the model.

Table 11.15 - PM peak journey time route comparison

ID	Name	OBSERVED (S)	MODELLED (S)	DIFF	%	Pass?
1	1 - Northbound	335	353	-18	-5%	Yes
2	1 - Southbound	449	354	95	21%	No
3	2 - Northbound	525	511	14	3%	Yes
4	2 - Southbound	592	537	55	9%	Yes
5	3 - Eastbound	287	294	-7	-3%	Yes
6	3 - Westbound	440	274	165	38%	No
7	4 - Northbound	202	188	14	7%	Yes
8	4 - Southbound	193	191	3	1%	Yes
9	5 - Northbound	910	772	138	15%	Yes
10	5 - Southbound	508	549	-40	-8%	Yes
11	6 - Eastbound	710	674	36	5%	Yes
12	6 - Westbound	597	618	-21	-4%	Yes
13	7 - Eastbound	392	421	-29	-7%	Yes
14	7 - Westbound	376	349	28	7%	Yes
15	8 - Eastbound	861	730	131	15%	Yes
16	8 - Westbound	825	824	1	0%	Yes
17	9 - Northbound	623	417	206	33%	No
18	9 - Southbound	312	351	-39	-13%	Yes

11.3.19 The journey times show that the link speeds and delays are accurately modelled on the key routes for all three time periods.

### MANUAL CLASSIFIED COUNTS

11.3.20 Table 11.16 to table 11.18 show the performance of the manual classified counts across all three peaks. Overall, the model matches well to the observed turning movements in terms of GEH for individual turns.

Table 11.16 - AM peak manual classified count performance

ID	DESCRIPTION	GEH<5	GEH < 7.5	GEH < 10
1	London Road/Arbor Lane/A12/Tower Road	76%	80%	88%
2	Tom Crisp Way/Stadbroke Road/Elm Tree Road	69%	94%	97%
3	Somerleyton Road/Oulton Street/Hall Lane/Gorleston Road	81%	88%	88%
4	Yarmouth Road/Gorleston Road	67%	78%	100%
5	Yarmouth Road/Leisure Way/Foxburrow Hill/Bentley Drive	88%	94%	94%
6	Yarmouth Road/Corton Road	56%	78%	89%
7	Millennium Way/Oulton Road/Peto Way	63%	81%	88%
8	Horn Hill/Maconochie Way/A12/Waveney Drive	88%	94%	100%
9	A12/Corton Long Lane/A12/Lowestoft Link Road	56%	75%	88%
10	A12 Waveney Road/Station Square	100%	100%	100%
11	Commercial Road/Station Square	78%	100%	100%
12	A12 Pier Terrace/London Road South/Belvedere Road	89%	89%	89%
13	A12 Belvedere Road/Kirkley Rise	36%	48%	52%
14	Denmark Road/Katwijk Way	67%	89%	89%
15	Katwijk Way/Raglan Street	56%	81%	81%
16	A12 Waveney Road/Suffolk Road	67%	78%	100%
17	A12 Tom Crisp Way/Blackheath Road	88%	100%	100%
18	Saltwater Way/Victoria Road	100%	100%	100%
19	Normanston Drive/Gorleston Road	67%	89%	100%
20	Fir Lane/A117 Normanston Drive/Peto Way	80%	100%	100%
21	A12/Gordon Road/Whapload Road	50%	69%	88%
22	A12/St Peters Street	56%	72%	92%

ID	DESCRIPTION	GEH < 5	GEH < 7.5	GEH<10
23	A1144/Katwijk Way	22%	44%	78%
24	A146 Beccles Road/Cotmer Road	100%	100%	100%

11.3.21 As detailed in section 5, interpeak turning movements were not carried out at junctions 10 to 24.

Table 11.17 - Interpeak manual classified count performance

ID	DESCRIPTION	GEH<5	GEH < 7.5	GEH<10
1	London Road/Arbor Lane/A12/Tower Road	76%	84%	92%
2	Tom Crisp Way/Stadbroke Road/Elm Tree Road	61%	97%	97%
3	Somerleyton Road/Oulton Street/Hall Lane/Gorleston Road	88%	94%	100%
4	Yarmouth Road/Gorleston Road	89%	100%	100%
5	Yarmouth Road/Leisure Way/Foxburrow Hill/Bentley Drive	81%	100%	100%
6	Yarmouth Road/Corton Road	67%	89%	100%
7	Millennium Way/Oulton Road/Peto Way	63%	81%	100%
8	Horn Hill/Maconochie Way/A12/Waveney Drive	81%	94%	100%
9	A12/Corton Long Lane/A12/Lowestoft Link Road	63%	69%	100%

Table 11.18 - PM peak manual classified count performance

ID	Description	GEH<5	GEH < 7.5	GEH < 10
1	London Road/Arbor Lane/A12/Tower Road	76%	88%	92%
2	Tom Crisp Way/Stadbroke Road/Elm Tree Road	64%	78%	97%
3	Somerleyton Road/Oulton Street/Hall Lane/Gorleston Road	69%	75%	88%
4	Yarmouth Road/Gorleston Road	78%	78%	89%
5	Yarmouth Road/Leisure Way/Foxburrow Hill/Bentley Drive	75%	94%	100%
6	Yarmouth Road/Corton Road	56%	78%	89%
7	Millennium Way/Oulton Road/Peto Way	31%	56%	88%
8	Horn Hill/Maconochie Way/A12/Waveney Drive	81%	81%	94%
9	A12/Corton Long Lane/A12/Lowestoft Link Road	63%	69%	81%
10	A12 Waveney Road/Station Square	67%	89%	100%
11	Commercial Road/Station Square	67%	89%	100%
12	A12 Pier Terrace/London Road South/Belvedere Road	78%	89%	89%
13	A12 Belvedere Road/Kirkley Rise	40%	48%	56%
14	Denmark Road/Katwijk Way	78%	78%	89%
15	Katwijk Way/Raglan Street	69%	81%	100%
16	A12 Waveney Road/Suffolk Road	78%	78%	100%
17	A12 Tom Crisp Way/Blackheath Road	69%	94%	100%
18	Saltwater Way/Victoria Road	33%	78%	89%
19	Normanston Drive/Gorleston Road	56%	78%	89%
20	Fir Lane/A117 Normanston Drive/Peto Way	60%	80%	92%
21	A12/Gordon Road/Whapload Road	50%	69%	88%
22	A12/St Peters Street	64%	88%	88%
23	A1144/Katwijk Way	56%	67%	89%
24	A146 Beccles Road/Cotmer Road	78%	78%	89%

### 11.4 MODELLED FLOW AND JUNCTION DELAY

11.4.1 Appendix G contains plots of the link flow and junction performance in the vicinity of the river crossings

# 12 SUMMARY OF MODEL DEVELOPMENT, STANDARDS ACHIEVED AND FITNESS FOR PURPOSE

### 12.1 SUMMARY OF MODEL DEVELOPMENT

- 12.1.1 The previous 2001 Lowestoft Traffic Model was rebuilt with a comprehensive check of the model network and a revised zone system of sufficient detail based on 2011 census geography.
- An observed prior matrix was derived from ANPR data which formed a cordon around the main study area and major internal locations. A gravity model was then used to form a synthetic matrix based on NTEM version 6.2 trip ends and 2011 census data. The synthetic matrix was used to infill the prior matrix for traffic movements not represented in the ANPR matrix.
- 12.1.3 Adjustments were made to the prior matrix using scaling of calibration counts to match the modelled flow to the observed flow. Matrix estimation was then carried out to produce a final assignment.

### 12.2 SUMMARY OF STANDARDS ACHIEVED

- The base year model validation has been developed closely following TAG M3.1 'Highway Assignment Modelling' guidance (January 2014).
- The model is shown to satisfactorily converge across all three peaks which is important as the model will be taken forward for testing of a major scheme business case. In these instances it is required that models are converged so that the benefits of the scheme are the result of the infrastructure improvements and not changes to model convergence.
- 12.2.3 Screenlines within the model which capture the key strategic movements within the model have been shown to closely match the observed flows to the modelled flows. Across all three peaks, all calibration screenlines are shown to achieve a GEH below 4, with the majority of validation screenlines also achieving this standard.
- Link validation is show to be consistently high in terms of both flow and GEH across all three peaks. Combining the observed counts within calibration and validation, 92% of counts in the AM peak, 94% of counts in the interpeak and 89% of counts in the PM peak achieve a GEH of 5 or lower above the minimum threshold of 85%.
- Journey time performance reaches the required standard of 85% of modelled journey time routes being within 15% of the observed journey time data in the AM peak and interpeak. In the AM peak, 94% of journey time routes achieve this standard, whilst 89% achieve this in the inter-peak. In the PM peak, journey time performance is marginally below the required standard at 83%, however this is not deemed a significant concern.
- 12.2.6 Manual classified turning counts were carried out a major junctions across the network, with the model shown to align well with the observed movements at these junctions.

### 12.3 ASSESSMENT OF FITNESS FOR PURPOSE

- The latest 2015 Lowestoft Transport Model is deemed fit for purpose in terms of its ability to replicate existing strategic traffic movements within the Area of Detailed Modelling (ADM). The base year model forms a suitable basis from which forecast year models can be built to create reference case, do minimum and do something scheme testing.
- 12.3.2 The model provides a suitable evidence base to underpin a major scheme business case and determine the benefits of a third crossing in Lowestoft.

### Appendix A

MCC TOTALS USED TO FACTOR ANPR DATA

Table A-1 – AM peak MCC totals used for doubly constrained furness of ANPR matrix

	Citt Decopination	Dip	C	AR	LG	SV	НС	eV.
	SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
1	A12 London Road	Inbound Outbound	608 0	0 430	117 0	0 150	30 0	0 44
2	A146 Beccles Road	Inbound Outbound	587 0	0 625	85 0	0 125	45 0	0 56
3	A12 Yarmouth Road	Inbound Outbound	746 0	0 1178	142 0	0 135	44 0	0 40
4	Coast Road	Inbound Outbound	61	0 54	7 0	0	2	0 3
	A12 Pier Terrace (Eastern Bascule bridge)	NB	326	998	44	120	18	25
5		SB	369	322	113	56	28	10
	A146 Bridge Road	NB	545	235	90	49	17	8
6	(Western Mutford bridge)	SB	442	274	105	47	18	18
7	D4075 Couloston Dood	NB	334	234	45	31	3	6
/	B1375 Gorleston Road	SB	276	81	65	7	10	1
8	A1117 Millennium Way	NB	218	110	27	13	8	8
0		SB	234	189	29	16	13	2
9	A12 Yarmouth Road	NB	302	204	43	24	23	7
Ŭ	7112 Tallilodii Rodd	SB	347	234	77	15	21	0
10	A12 Tom Crisp Way	NB	525	192	64	23	12	6
.0	The roll of the	SB	199	100	59	19	17	11
11	B1532 London Road	NB	233	205	29	27	9	6
	South	SB	199	110	47	18	10	4
12	B1074 Blundeston Road	Inbound Outbound	164 0	0 99	40 0	0 15	4 0	0
13	Flixton Road	Inbound Outbound	78 0	0 49	11 0	0 9	2 0	<u>0</u> 3
4.4	DAFOA Wasser Di	EB	258	85	28	7	9	0
14	B1531 Waveney Drive	WB	40	96	9	11	3	2
15	North Quay Retail Park	Entry	36	107	6	9	0	0
10	North Quay Retail Palk	Exit	0	71	0	0	0	0
16	Links Road Car Park	Entry	3	0	0	0	0	0
10	LIIINS NOAU OAI FAIR	Exit	1	3	0	0	0	0

	CITE DECORPTION	Dup	C/	AR	LG	ev.	НС	€V
	SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
17	Swimming Pool Road	Entry	0	1	0	0	0	0
17	Car Park	Exit	0	0	0	0	0	0
18	Shopping Centre Car Park (Battery Green Rd	Entry	0	0	0	0	0	0
10	exit)	Exit	0	0	1	0	0	0
19	Shopping Centre Car Park (Gordon Road	Entry	0	32	0	0	0	0
19	entry)	Exit	0	0	0	0	0	0
20	Surrey St Car Park	Entry	8	14	0	0	0	0
20	entry	Exit	0	0	0	0	0	0
21	Surrey St Car Park exit	Entry	0	0	0	0	0	0
۷۱	(onto Clapham Road)	Exit	0	3	0	0	0	0
22	Clapham Road Car	Entry	3	24	0	0	0	0
22	Park	Exit	3	6	0	0	0	0
23	St Johns Rd Car Park	Entry	0	0	0	0	0	0
23	St Johns Nu Cai Faik	Exit	0	2	0	0	0	0
24	Kirkley Rise Car Park	Entry	4	21	0	0	0	0
24	(Northern access)	Exit	0	9	0	0	0	0
25	Kirkley Rise Car Park	Entry	2	3	0	0	0	0
25	(Southern access)	Exit	0	0	0	0	0	0
26	Kirkley Cliff Road Car	Entry	0	0	0	0	0	0
20	Park	Exit	0	0	0	0	0	0
27	Claremont Road Car	Entry	0	0	0	0	0	0
<u> </u>	Park	Exit	0	0	0	0	0	0
28	Marine Parade Car	Entry	0	5	0	0	0	0
20	Park	Exit	0	0	0	0	0	0
29	Asda Car Park	Entry	155	60	12	2	0	0
20	, load Oal I ailk	Exit	23	132	13	0	0	0

Table A-2 – Inter peak MCC totals used for doubly constrained furness of ANPR matrix

	0: 0	Din	CA	AR	LO	SV	НС	<b>SV</b>
	SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
1	A12 London Road	Inbound	511	0	90	0	33	0
	A440 D	Outbound Inbound	0 457	526 0	0 93	85 0	0 38	38 0
2	A146 Beccles Road	Outbound	0	467	0	86	0	39
3	A12 Yarmouth Road	Inbound Outbound	704 0	0 711	119 0	0 118	37 0	0 35
4	Coast Road	Inbound	52	0	5	0	2	0
	Oddi Rodd	Outbound	0	58	0	7	0	3
5	•	NB	323	547	40	87	12	32
	bridge)	SB	624	252	86	39	37	14
6	A146 Bridge Road (Western Mutford	NB	428	390	60	70	22	13
	bridge)	SB	391	389	61	59	13	18
7	B1375 Gorleston Road	NB	163	207	29	33	1	15
,	D 1070 Contolon Road	SB	292	106	52	10	13	1
8	8 A1117 Millennium Way	NB	220	161	30	15	6	8
J		SB	217	120	35	11	11	3
9	A12 Yarmouth Road	NB	292	183	45	26	15	8
J	7112 Tallilodii Rodd	SB	344	116	52	16	25	3
10	A12 Tom Crisp Way	NB	297	137	41	31	13	5
	THE FORM SHOP Way	SB	179	254	31	33	11	15
11	B1532 London Road	NB	143	138	25	26	13	5
	South	SB	180	149	31	15	10	8
12	B1074 Blundeston Road	Inbound	90 0	0 80	20 0	0 18	3 0	0 3
40		Outbound Inbound	57	0	9	0	1	0
13	Flixton Road	Outbound	0	41	0	7	0	1
14	B1531 Waveney Drive	EB	169	44	22	5	4	4
	, 2	WB	53	163	8	21	4	5
15	North Quay Retail Park	Entry	147	230	9	19	1	0
	Quay redain runk	Exit	0	373	0	0	0	0
16	Links Road Car Park	Entry	7	3	0	0	0	0
10	Ening Road Oal Laik	Exit	4	5	0	1	0	0

	0 D	D	C,	AR	LO	ev.	НС	eV
	SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
17	Swimming Pool Road	Entry	0	7	0	0	0	0
17	Car Park	Exit	5	0	0	0	0	0
18	Shopping Centre Car Park (Battery Green Rd	Entry	0	0	0	0	0	0
10	exit)	Exit	48	0	1	0	0	0
19	Shopping Centre Car Park (Gordon Road	Entry	6	39	0	1	0	0
19	entry)	Exit	0	0	0	0	0	0
20	Surrey St Car Park	Entry	34	26	1	0	0	0
20	entry	Exit	0	0	0	0	0	0
21	Surrey St Car Park exit	Entry	0	0	0	0	0	0
<b>4</b> 1	(onto Clapham Road)	Exit	33	33	1	1	0	0
22	Clapham Road Car	Entry	25	78	0	0	0	0
	Park	Exit	82	24	0	3	0	0
23	St Johns Rd Car Park	Entry	0	4	2	0	0	0
	Occomine the Gail Failt	Exit	2	1	0	1	0	0
24	Kirkley Rise Car Park	Entry	6	4	0	0	0	0
- 1	(Northern access)	Exit	11	0	0	0	0	0
25	Kirkley Rise Car Park	Entry	2	1	0	0	0	0
	(Southern access)	Exit	0	0	0	0	0	0
26	Kirkley Cliff Road Car	Entry	0	0	0	0	0	0
	Park	Exit	0	0	0	0	0	0
27	Claremont Road Car	Entry	1	11	0	0	0	0
	Park	Exit	6	5	2	0	0	0
28	Marine Parade Car	Entry	4	34	0	3	0	0
	Park	Exit	29	7	0	0	0	1
29	Asda Car Park	Entry	265	72	15	1	1	1
	3.5.5	Exit	81	259	3	13	1	0

Table A-3 – PM peak MCC totals used for doubly constrained furness of ANPR matrix

		Curr Draonunguou	Din	C	AR	LO	SV	НС	<b>SV</b>
		SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
	1	A12 London Road	Inbound	611	0	104	0	14	0
_			Outbound Inbound	0 871	668 0	0 136	103 0	0 19	15 0
	2	A146 Beccles Road	Outbound	0	673	0	53	0	17
	3	A12 Yarmouth Road	Inbound	1388 0	0 909	173	0 91	18	0 19
H	_		Outbound Inbound	84	909	0 7	0	0 3	0
	4	Coast Road	Outbound		52	0	5	0	3
	5	A12 Pier Terrace (Eastern Bascule	NB	358	608	32	78	5	23
	Ü	bridge)	SB	1086	333	107	40	15	10
	6	A146 Bridge Road (Western Mutford	NB	419	538	52	88	6	11
		bridge)	SB	331	672	40	79	4	7
	7	B1375 Gorleston Road	NB	115	277	17	49	1	3
_			SB	455	188	65	35	6	1
	8	A1117 Millennium Way	NB	247	221	12	25	2	5
	-		SB	227	247	34	30	4	1
	9	A12 Yarmouth Road	NB	429	265	44	26	7	8
			SB	397	167	46	11	17	3
	10	A12 Tom Crisp Way	NB	232	217	31	40	5	4
			SB	297	471	19	44	3	6
	11	B1532 London Road	NB	187	239	14	25	7	4
		South	SB	222	229	19	23	8	3
	12	B1074 Blundeston Road	Inbound Outbound	167 0	0 111	32 0	0 15	1 0	0
-	40		Inbound	59	0	13	0	1	0
	13	Flixton Road	Outbound		61	0	6	0	0
	14	B1531 Waveney Drive	EB	164	50	16	6	4	2
		2.33	WB	117	290	6	33	1	5
	15	North Quay Retail Park	Entry	99	175	7	17	0	0
	.0	Quay rolaii i air	Exit	0	309	0	0	0	0
	16	Links Road Car Park	Entry	5	4	0	0	0	0
	10	Linko Rodu Odi i dik	Exit	0	8	0	0	0	0

	0 0	D	C/	AR	LO	eV	НС	ev V
	SITE DESCRIPTION	Dir	ORIGIN	DEST	ORIGIN	DEST	ORIGIN	DEST
17	Swimming Pool Road	Entry	0	5	0	0	0	0
17	Car Park	Exit	15	0	0	0	0	0
18	Shopping Centre Car Park (Battery Green Rd	Entry	0	0	0	0	0	0
10	exit)	Exit	25	0	1	0	0	0
19	Shopping Centre Car Park (Gordon Road	Entry	0	1	0	0	0	0
19	entry)	Exit	0	0	0	0	0	0
20	Surrey St Car Park	Entry	3	0	0	0	0	0
20	entry	Exit	0	0	0	0	0	0
21	Surrey St Car Park exit	Entry	0	0	0	0	0	0
۷۱	(onto Clapham Road)	Exit	11	4	0	0	0	0
22	Clapham Road Car	Entry	7	15	0	0	0	0
22	Park	Exit	35	12	0	3	0	0
23	St Johns Rd Car Park	Entry	8	0	0	0	0	0
23	St Johns Ru Cai Paik	Exit	3	1	0	0	0	0
24	Kirkley Rise Car Park	Entry	0	2	0	0	0	0
<b>24</b>	(Northern access)	Exit	10	0	0	0	0	0
25	Kirkley Rise Car Park	Entry	0	0	0	0	0	0
25	(Southern access)	Exit	1	1	0	0	0	0
26	Kirkley Cliff Road Car	Entry	0	0	0	0	0	0
20	Park	Exit	1	0	0	0	0	0
27	Claremont Road Car	Entry	5	10	0	2	0	0
	Park	Exit	9	1	0	0	0	0
28	Marine Parade Car	Entry	1	16	0	0	0	0
<b>2</b> 6	Park	Exit	22	1	4	0	0	0
20	Ando Cor Port	Entry	184	104	11	8	0	0
29	Asda Car Park	Exit	61	254	6	15	0	0

## Appendix B

**GRAVITY MODEL TLD AND MATRIX CHANGES** 

### AM peak gravity model

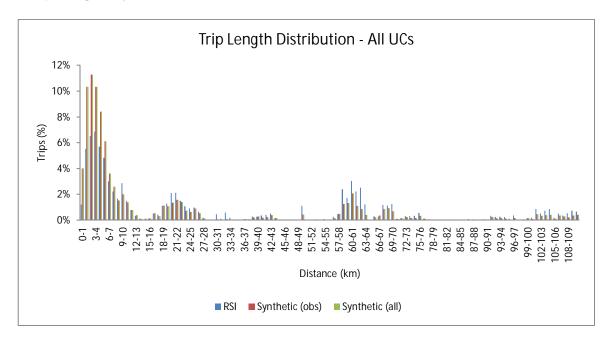


Figure B.1 – AM peak - Overall trip length distribution (UC1 to UC3)

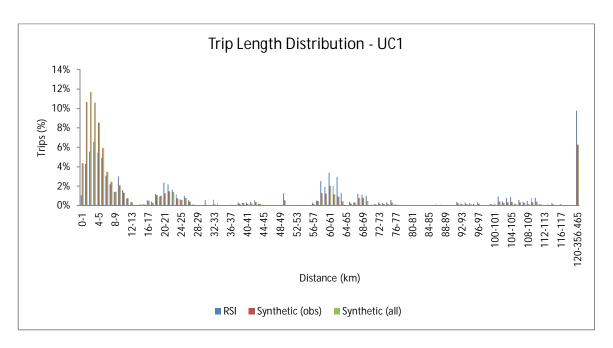


Figure B.2 – AM peak – UC1 trip length distribution

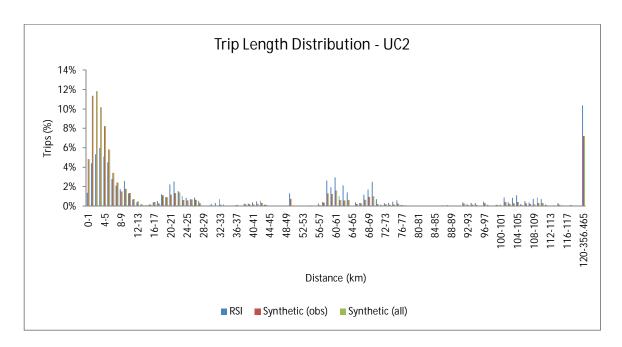


Figure B.3 – AM peak – UC2 trip length distribution

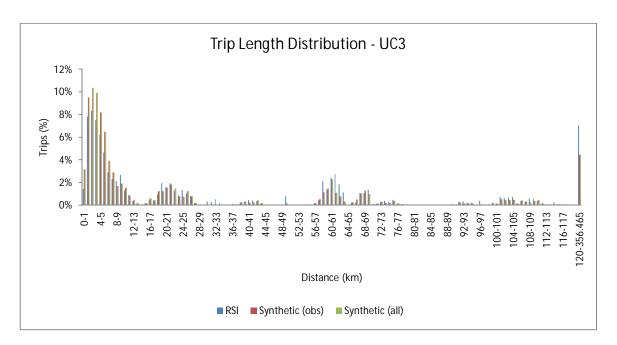


Figure B.4 – AM peak – UC3 trip length distribution

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	31	16	47
2	0	0	0	326	145	471
3	0	0	0	301	153	454
4	42	188	260	361	239	1090
5	35	172	236	622	400	1465
Total	77	360	496	1641	953	3527

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	13	16	17	10	58
2	28	69	101	243	154	595
3	27	77	43	273	148	568
4	32	202	317	1483	530	2564
5	36	226	307	957	1040	2566
Total	125	587	784	2973	1882	6351

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	13	16	17	10	58
2	28	69	101	244	154	596
3	27	77	43	273	148	568
4	32	202	317	1484	530	2565
5	36	226	307	958	1040	2567
Total	125	587	784	2976	1882	6354

### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	1%
2	0%	0%	0%	9%	4%	13%
3	0%	0%	0%	9%	4%	13%
4	1%	5%	7%	10%	7%	31%
5	1%	5%	7%	18%	11%	42%
Total	2%	10%	14%	47%	27%	100%

### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	2%	4%	2%	9%
3	0%	1%	1%	4%	2%	9%
4	1%	3%	5%	23%	8%	40%
5	1%	4%	5%	15%	16%	40%
Total	2%	9%	12%	47%	30%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	2%	4%	2%	9%
3	0%	1%	1%	4%	2%	9%
4	1%	3%	5%	23%	8%	40%
5	1%	4%	5%	15%	16%	40%
Total	2%	9%	12%	47%	30%	100%

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	4	2	6
2	0	0	0	40	18	58
3	0	0	0	36	19	55
4	6	27	36	44	35	148
5	4	19	26	64	41	154
Total	10	46	62	188	115	421

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	2	1	7
2	4	11	16	26	17	74
3	4	12	7	29	17	69
4	3	22	36	184	66	311
5	3	23	32	102	116	276
Total	14	70	93	343	217	737

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	2	1	7
2	4	11	16	26	17	74
3	4	12	7	29	17	69
4	3	22	36	185	66	312
5	3	23	32	102	116	276
Total	14	70	93	344	217	738

### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	1%
2	0%	0%	0%	10%	4%	14%
3	0%	0%	0%	9%	5%	13%
4	1%	6%	9%	10%	8%	35%
5	1%	5%	6%	15%	10%	37%
Total	2%	11%	15%	45%	27%	100%

### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	1%	1%	2%	4%	2%	10%
3	1%	2%	1%	4%	2%	9%
4	0%	3%	5%	25%	9%	42%
5	0%	3%	4%	14%	16%	37%
Total	2%	9%	13%	47%	29%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	1%	1%	2%	4%	2%	10%
3	1%	2%	1%	4%	2%	9%
4	0%	3%	5%	25%	9%	42%
5	0%	3%	4%	14%	16%	37%
Total	2%	9%	13%	47%	29%	100%

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	12	12	24
2	0	0	0	134	130	264
3	0	0	0	132	147	279
4	17	87	121	177	297	699
5	14	75	114	313	352	868
Total	31	162	235	768	938	2134

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	15	12	31
2	4	9	14	171	144	342
3	4	11	7	200	150	372
4	20	112	179	642	381	1334
5	18	102	145	412	552	1229
Total	46	236	347	1440	1239	3308

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	15	12	31
2	4	9	14	171	144	342
3	4	11	7	200	150	372
4	20	112	179	642	382	1335
5	18	102	145	412	552	1229
Total	46	236	347	1440	1240	3309

### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	1%
2	0%	0%	0%	6%	6%	12%
3	0%	0%	0%	6%	7%	13%
4	1%	4%	6%	8%	14%	33%
5	1%	4%	5%	15%	16%	41%
Total	1%	8%	11%	36%	44%	100%

### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	0%	0%	5%	4%	10%
3	0%	0%	0%	6%	5%	11%
4	1%	3%	5%	19%	12%	40%
5	1%	3%	4%	12%	17%	37%
Total	1%	7%	10%	44%	37%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	0%	0%	5%	4%	10%
3	0%	0%	0%	6%	5%	11%
4	1%	3%	5%	19%	12%	40%
5	1%	3%	4%	12%	17%	37%
Total	1%	7%	10%	44%	37%	100%

### Inter peak gravity model

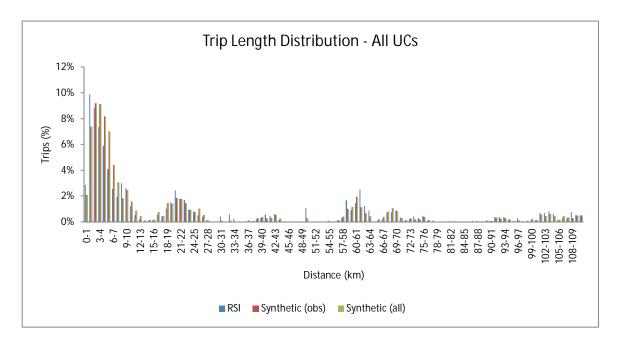


Figure B.5 – Interpeak - Overall trip length distribution (UC1 to UC3)

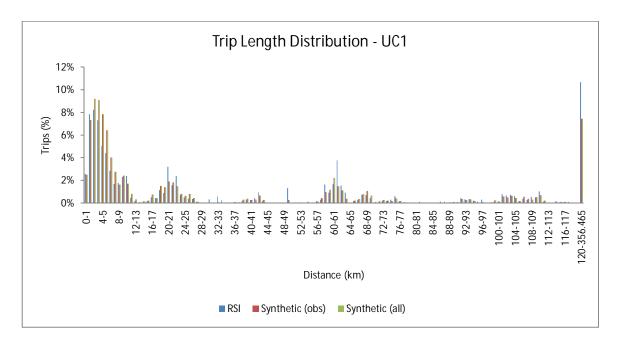


Figure B.6 – Interpeak – UC1 trip length distribution

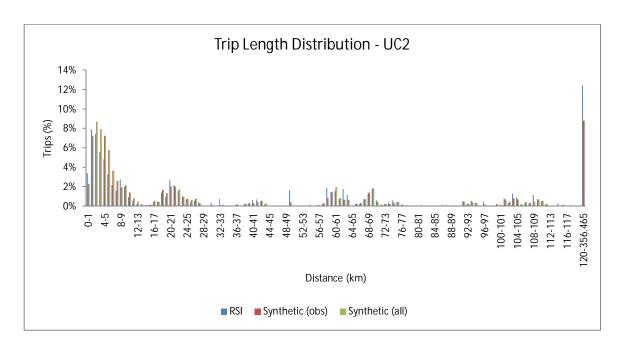


Figure B.7 – Interpeak – UC2 trip length distribution

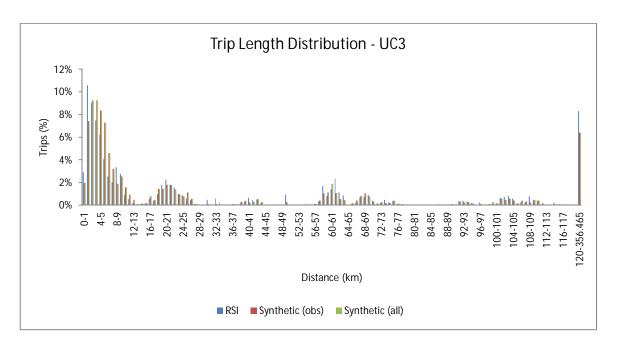


Figure B.8 – Interpeak – UC3 trip length distribution

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	18	7	25
2	0	0	0	117	39	156
3	0	0	0	126	37	163
4	12	68	50	228	79	437
5	12	59	38	224	126	459
Total	24	127	88	713	288	1240

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	3	2	17	10	32
2	3	10	9	108	67	197
3	3	12	5	116	68	204
4	18	99	76	327	172	692
5	18	100	72	281	235	706
Total	42	224	164	849	552	1831

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	3	2	17	10	32
2	3	10	9	108	67	197
3	3	12	5	116	68	204
4	18	99	76	328	172	693
5	18	100	72	281	235	706
Total	42	224	164	850	552	1832

### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	2%
2	0%	0%	0%	9%	3%	13%
3	0%	0%	0%	10%	3%	13%
4	1%	5%	4%	18%	6%	35%
5	1%	5%	3%	18%	10%	37%
Total	2%	10%	7%	58%	23%	100%

### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	2%
2	0%	1%	0%	6%	4%	11%
3	0%	1%	0%	6%	4%	11%
4	1%	5%	4%	18%	9%	38%
5	1%	5%	4%	15%	13%	39%
Total	2%	12%	9%	46%	30%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	2%
2	0%	1%	0%	6%	4%	11%
3	0%	1%	0%	6%	4%	11%
4	1%	5%	4%	18%	9%	38%
5	1%	5%	4%	15%	13%	39%
Total	2%	12%	9%	46%	30%	100%

NB - Intra-zonals are removed

#### **RSI Matrix - Total Trips**

	1	2	3	4	5	Total
1	0	0	0	5	2	7
2	0	0	0	29	15	44
3	0	0	0	29	15	44
4	8	43	29	76	51	207
5	4	22	16	44	39	125
Total	12	65	45	183	122	427

#### Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	1	1	6	3	11
2	1	5	5	36	23	70
3	1	6	3	39	23	72
4	8	47	36	117	70	278
5	6	36	27	81	65	215
Total	16	95	72	279	184	646

## Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	1	1	6	3	11
2	1	5	5	36	23	70
3	1	6	3	39	23	72
4	8	47	36	117	70	278
5	6	36	27	81	65	215
Total	16	95	72	279	184	646

#### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	2%
2	0%	0%	0%	7%	4%	10%
3	0%	0%	0%	7%	4%	10%
4	2%	10%	7%	18%	12%	48%
5	1%	5%	4%	10%	9%	29%
Total	3%	15%	11%	43%	29%	100%

#### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	2%
2	0%	1%	1%	6%	4%	11%
3	0%	1%	0%	6%	4%	11%
4	1%	7%	6%	18%	11%	43%
5	1%	6%	4%	13%	10%	33%
Total	2%	15%	11%	43%	28%	100%

		1	2	3	4	5	Total
	1	0%	0%	0%	1%	0%	2%
	2	0%	1%	1%	6%	4%	11%
	3	0%	1%	0%	6%	4%	11%
	4	1%	7%	6%	18%	11%	43%
	5	1%	6%	4%	13%	10%	33%
1	Total	2%	15%	11%	43%	28%	100%

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	34	34	68
2	0	0	0	234	237	471
3	0	0	0	269	241	510
4	49	293	241	702	782	2067
5	39	219	142	494	817	1711
Total	88	512	383	1733	2111	4827

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	1	8	7	45	38	99
2	10	35	34	312	268	659
3	10	47	21	367	297	742
4	54	326	273	1063	860	2576
5	49	297	236	864	967	2413
Total	124	713	571	2651	2430	6489

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	1	8	7	45	38	99
2	10	35	34	312	268	659
3	10	47	21	367	297	742
4	54	326	273	1064	860	2577
5	49	297	236	864	967	2413
Total	124	713	571	2652	2430	6490

#### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	1%
2	0%	0%	0%	5%	5%	10%
3	0%	0%	0%	6%	5%	11%
4	1%	6%	5%	15%	16%	43%
5	1%	5%	3%	10%	17%	35%
Total	2%	11%	8%	36%	44%	100%

#### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	2%
2	0%	1%	1%	5%	4%	10%
3	0%	1%	0%	6%	5%	11%
4	1%	5%	4%	16%	13%	40%
5	1%	5%	4%	13%	15%	37%
Total	2%	11%	9%	41%	37%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	2%
2	0%	1%	1%	5%	4%	10%
3	0%	1%	0%	6%	5%	11%
4	1%	5%	4%	16%	13%	40%
5	1%	5%	4%	13%	15%	37%
Total	2%	11%	9%	41%	37%	100%

#### PM peak gravity model

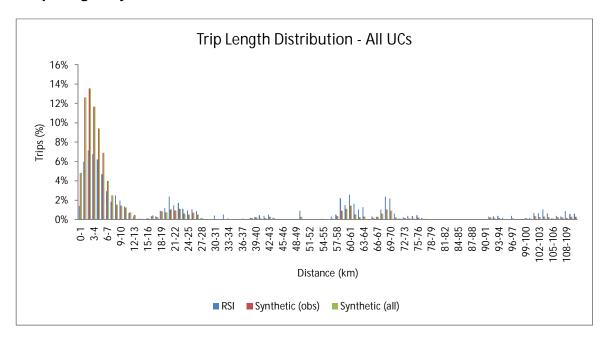


Figure B.9 – PM peak - Overall trip length distribution (UC1 to UC3)

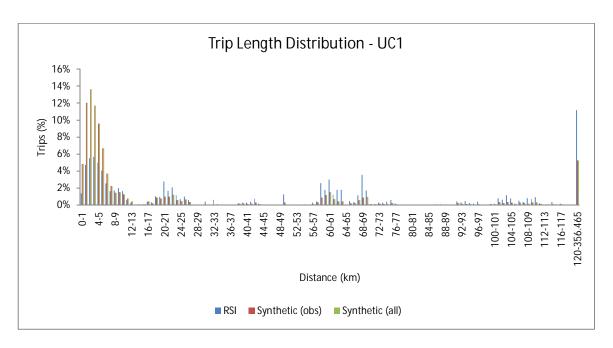


Figure B.10 – PM peak – UC1 trip length distribution

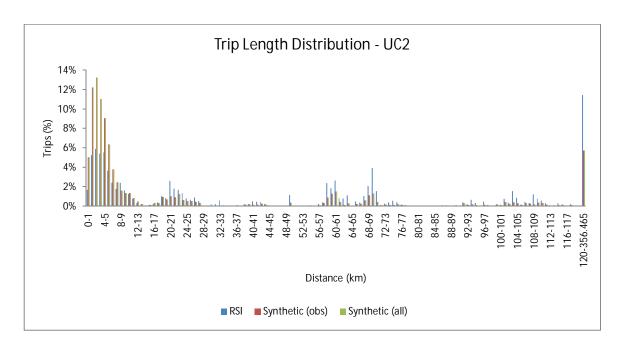


Figure B.11 – PM peak – UC2 trip length distribution

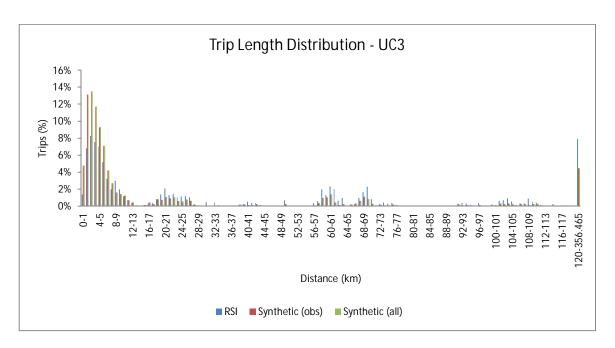


Figure B.12 – PM peak – UC3 trip length distribution

NB - Intra-zonals are removed

#### **RSI Matrix - Total Trips**

	1	2	3	4	5	Total
1	0	0	0	38	14	52
2	0	0	0	255	96	351
3	0	0	0	341	176	517
4	34	196	180	320	282	1012
5	27	135	133	352	240	887
Total	61	331	313	1306	808	2819

#### Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	14	12	21	13	62
2	16	47	49	192	121	425
3	22	78	32	311	171	614
4	29	201	219	1786	617	2852
5	30	217	207	1050	1183	2687
Total	99	557	519	3360	2105	6640

## Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	14	12	21	13	62
2	16	47	49	192	121	425
3	22	78	32	311	171	614
4	29	201	219	1787	618	2854
5	30	217	207	1051	1183	2688
Total	99	557	519	3362	2106	6643

#### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	2%
2	0%	0%	0%	9%	3%	12%
3	0%	0%	0%	12%	6%	18%
4	1%	7%	6%	11%	10%	36%
5	1%	5%	5%	12%	9%	31%
Total	2%	12%	11%	46%	29%	100%

#### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	5%	3%	9%
4	0%	3%	3%	27%	9%	43%
5	0%	3%	3%	16%	18%	40%
Total	1%	8%	8%	51%	32%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	5%	3%	9%
4	0%	3%	3%	27%	9%	43%
5	0%	3%	3%	16%	18%	40%
Total	1%	8%	8%	51%	32%	100%

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	5	2	7
2	0	0	0	32	14	46
3	0	0	0	43	25	68
4	8	46	41	59	64	218
5	4	20	21	41	35	121
Total	12	66	62	180	140	460

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	3	2	9
2	3	8	8	26	17	62
3	4	13	5	43	24	89
4	5	37	40	279	101	462
5	5	37	35	148	172	397
Total	17	97	90	499	316	1019

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	0	2	2	3	2	9
2	3	8	8	26	17	62
3	4	13	5	43	24	89
4	5	37	40	280	101	463
5	5	37	35	148	172	397
Total	17	97	90	500	316	1020

#### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	0%	2%
2	0%	0%	0%	7%	3%	10%
3	0%	0%	0%	9%	5%	15%
4	2%	10%	9%	13%	14%	47%
5	1%	4%	5%	9%	8%	26%
Total	3%	14%	13%	39%	30%	100%

#### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	4%	2%	9%
4	0%	4%	4%	27%	10%	45%
5	0%	4%	3%	15%	17%	39%
Total	2%	10%	9%	49%	31%	100%

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	4%	2%	9%
4	0%	4%	4%	27%	10%	45%
5	0%	4%	3%	15%	17%	39%
Total	2%	10%	9%	49%	31%	100%

NB - Intra-zonals are removed

**RSI Matrix - Total Trips** 

	1	2	3	4	5	Total
1	0	0	0	31	30	61
2	0	0	0	228	223	451
3	0	0	0	320	394	714
4	42	279	282	497	987	2087
5	34	189	189	406	635	1453
Total	76	468	471	1482	2269	4766

Synthetic (Observed) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	15	14	24	22	77
2	17	55	60	238	222	592
3	24	92	42	411	325	894
4	30	235	276	2312	1164	4017
5	27	224	229	1165	1933	3578
Total	100	621	621	4150	3666	9158

Synthetic (Full) Matrix - Total Trips

	1	2	3	4	5	Total
1	2	15	14	24	22	77
2	17	55	60	238	222	592
3	24	92	42	411	325	894
4	30	235	276	2314	1164	4019
5	27	224	229	1166	1933	3579
Total	100	621	621	4153	3666	9161

#### **RSI Matrix - % of Total**

	1	2	3	4	5	Total
1	0%	0%	0%	1%	1%	1%
2	0%	0%	0%	5%	5%	9%
3	0%	0%	0%	7%	8%	15%
4	1%	6%	6%	10%	21%	44%
5	1%	4%	4%	9%	13%	30%
Total	2%	10%	10%	31%	48%	100%

#### Synthetic (Observed) Matrix - % of Total

	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	4%	4%	10%
4	0%	3%	3%	25%	13%	44%
5	0%	2%	3%	13%	21%	39%
Total	1%	7%	7%	45%	40%	100%

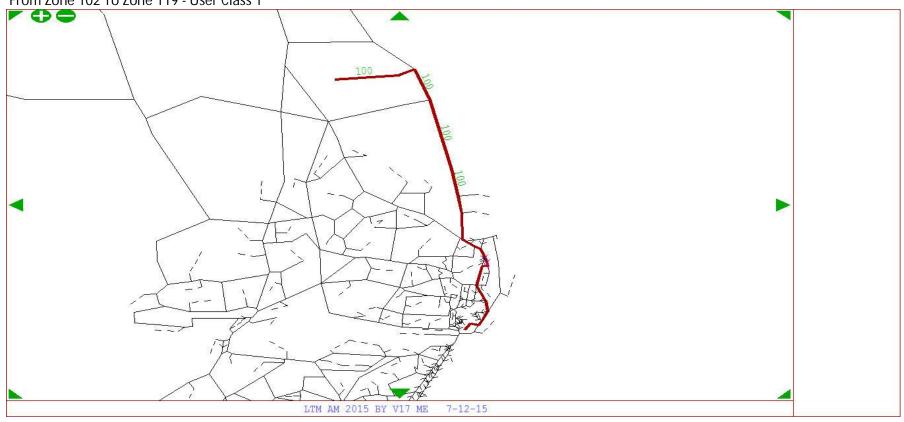
	1	2	3	4	5	Total
1	0%	0%	0%	0%	0%	1%
2	0%	1%	1%	3%	2%	6%
3	0%	1%	0%	4%	4%	10%
4	0%	3%	3%	25%	13%	44%
5	0%	2%	2%	13%	21%	39%
Total	1%	7%	7%	45%	40%	100%

# Appendix C

**ORIGIN-DESTINATION TREES** 

# Lowestoft: OD Tree Plots - AM Peak

From Zone 102 To Zone 119 - User Class 1



From Zone 102 To Zone 119 - User Class 2

7-12-15

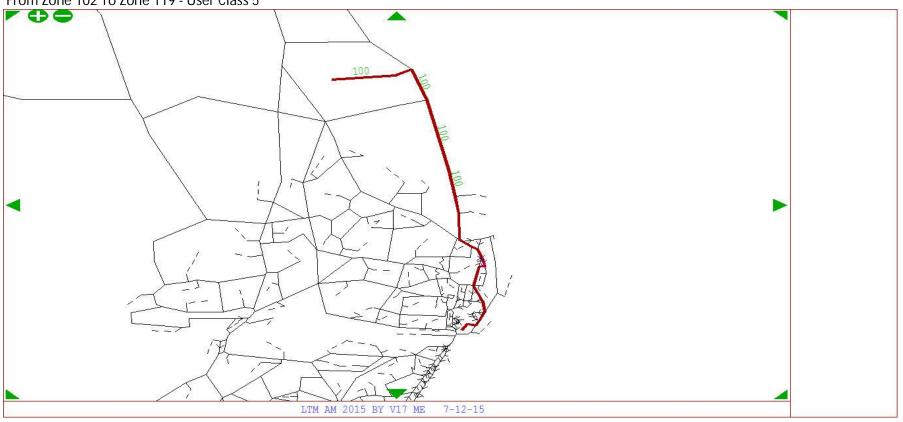
From Zone 102 To Zone 119 - User Class 3

7-12-15

From Zone 102 To Zone 119 - User Class 4

7-12-15

From Zone 102 To Zone 119 - User Class 5



From Zone 102 To Zone 122 - User Class 1

From Zone 102 To Zone 122 - User Class 2

From Zone 102 To Zone 122 - User Class 3

From Zone 102 To Zone 122 - User Class 4

From Zone 102 To Zone 122 - User Class 5

From Zone 102 To Zone 130 - User Class 1

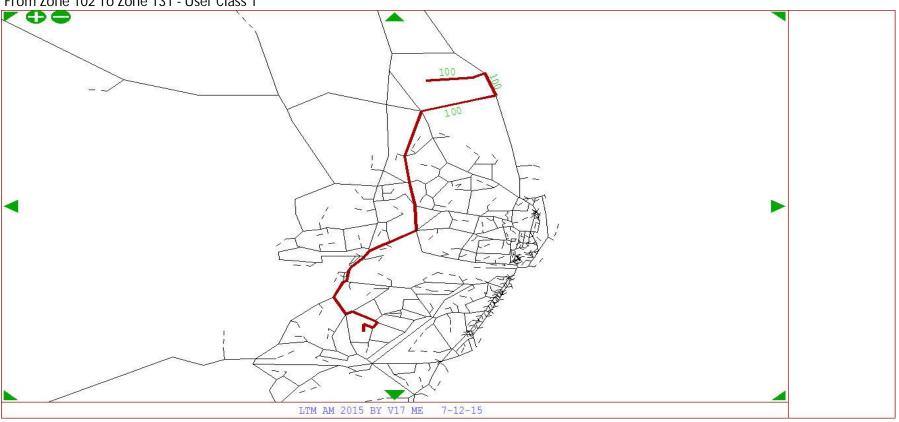
From Zone 102 To Zone 130 - User Class 2

From Zone 102 To Zone 130 - User Class 3

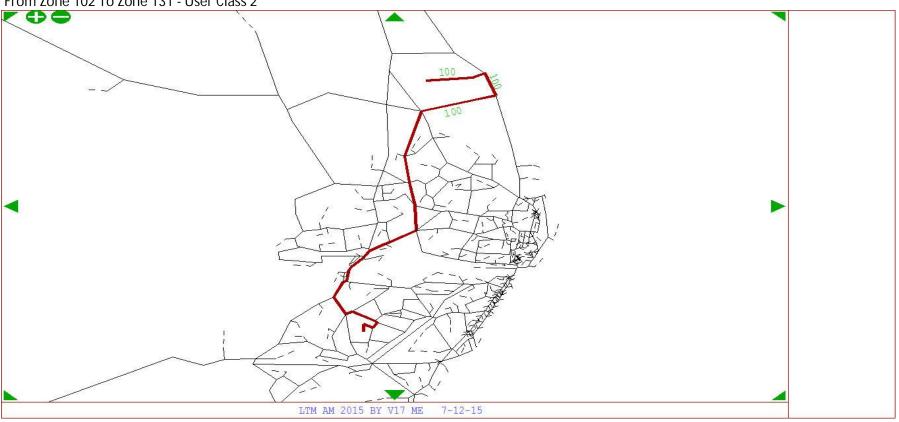
From Zone 102 To Zone 130 - User Class 4

From Zone 102 To Zone 130 - User Class 5

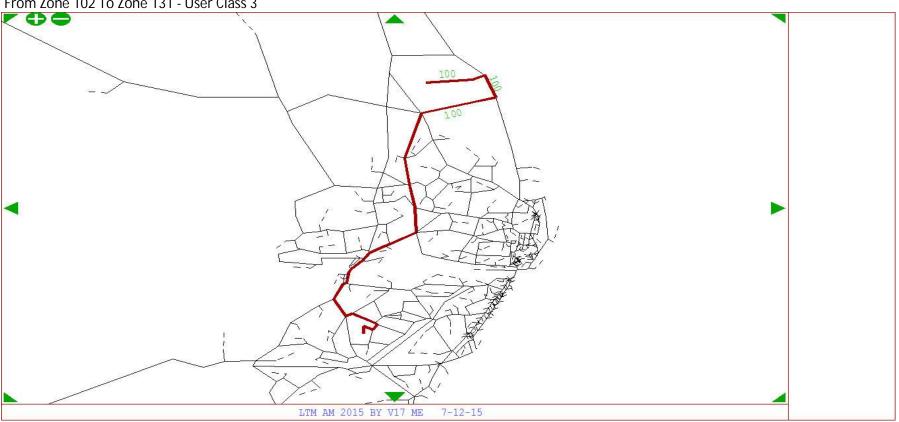
From Zone 102 To Zone 131 - User Class 1



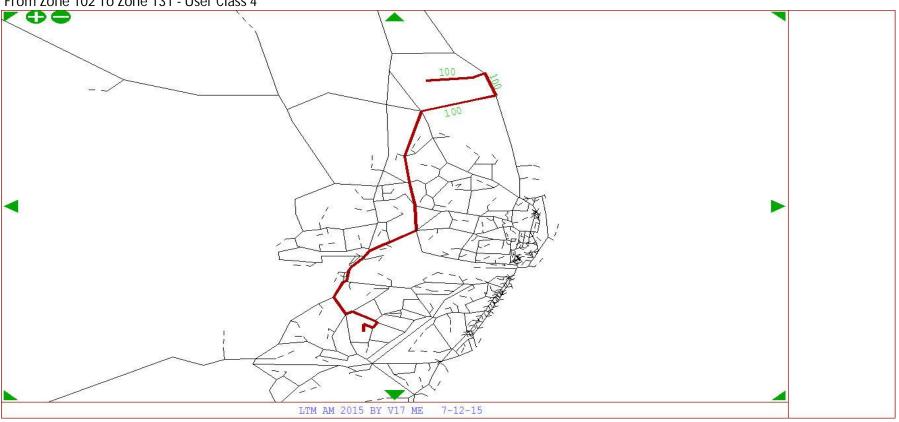
From Zone 102 To Zone 131 - User Class 2



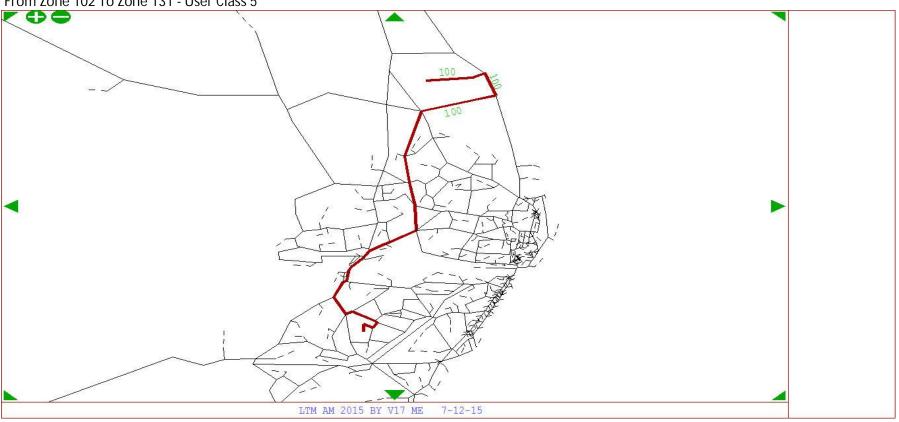
From Zone 102 To Zone 131 - User Class 3



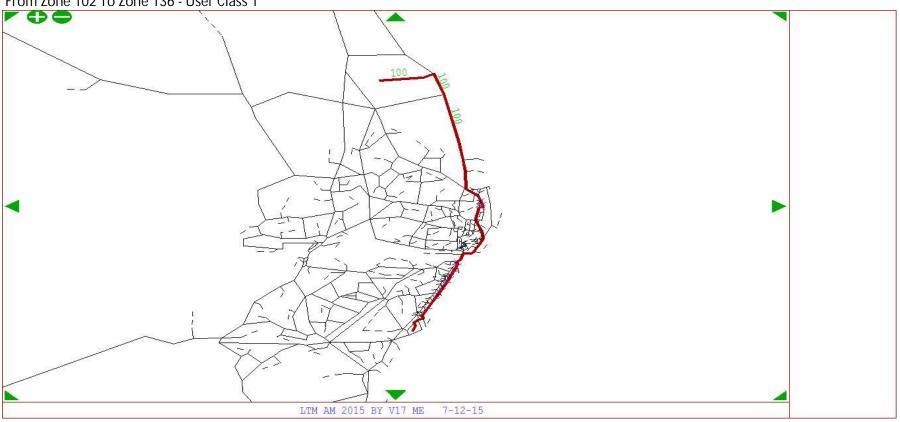
From Zone 102 To Zone 131 - User Class 4



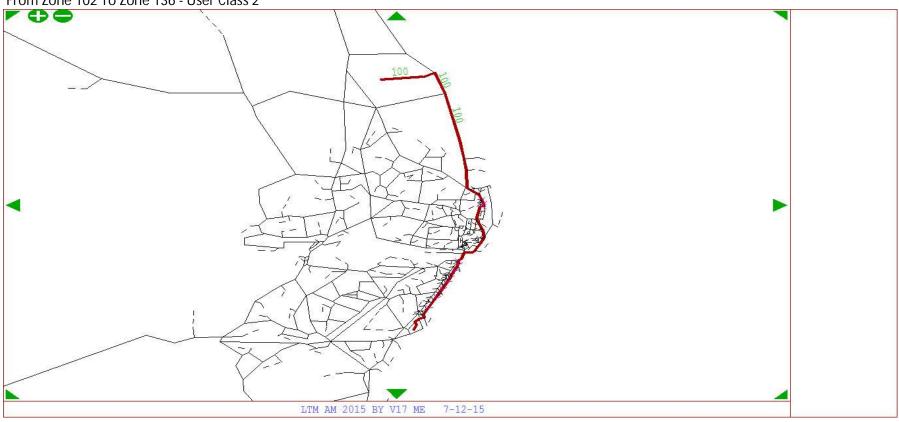
From Zone 102 To Zone 131 - User Class 5



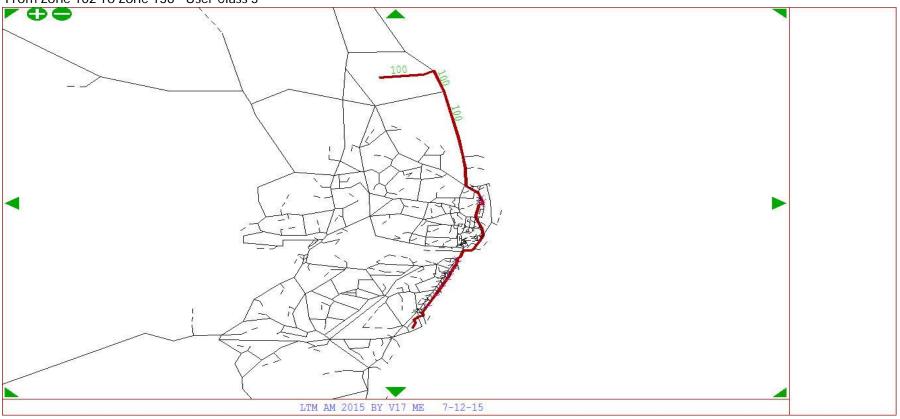
From Zone 102 To Zone 136 - User Class 1



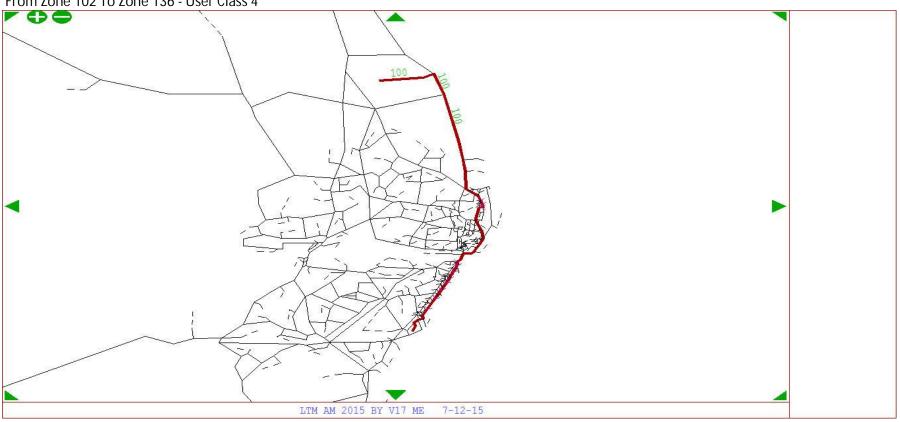
From Zone 102 To Zone 136 - User Class 2



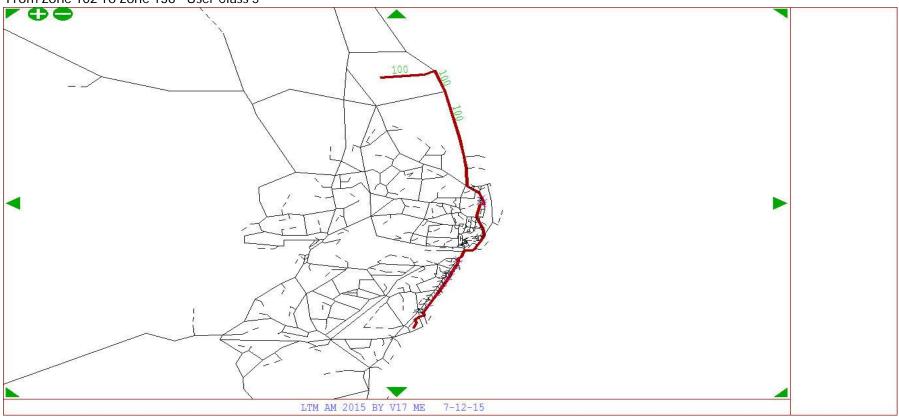
From Zone 102 To Zone 136 - User Class 3



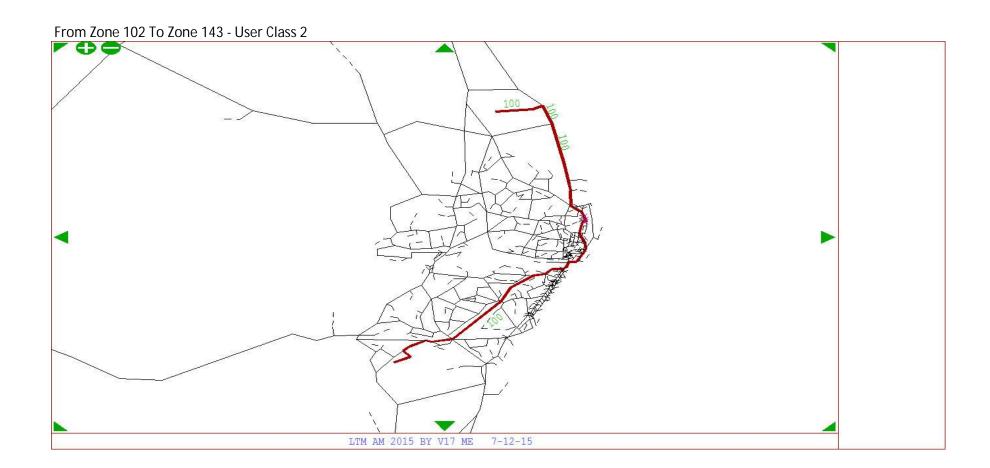
From Zone 102 To Zone 136 - User Class 4

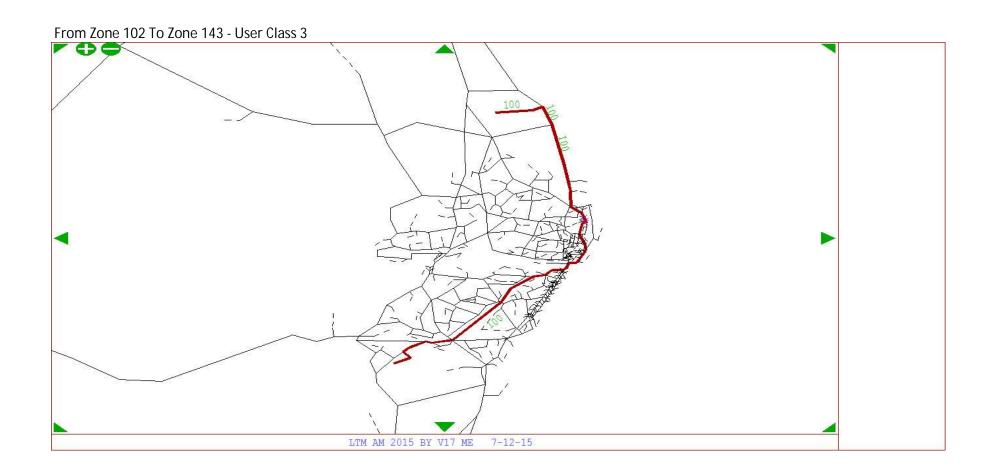


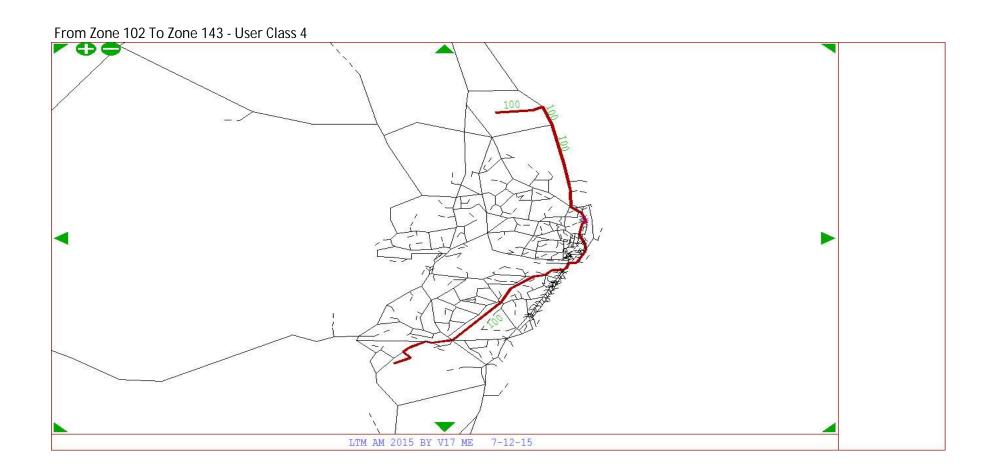
From Zone 102 To Zone 136 - User Class 5



From Zone 102 To Zone 143 - User Class 1 LTM AM 2015 BY V17 ME







From Zone 102 To Zone 143 - User Class 5 LTM AM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 1 LTM AM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 2 LTM AM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 3 LTM AM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 4 LTM AM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 5 LTM AM 2015 BY V17 ME 7-12-15

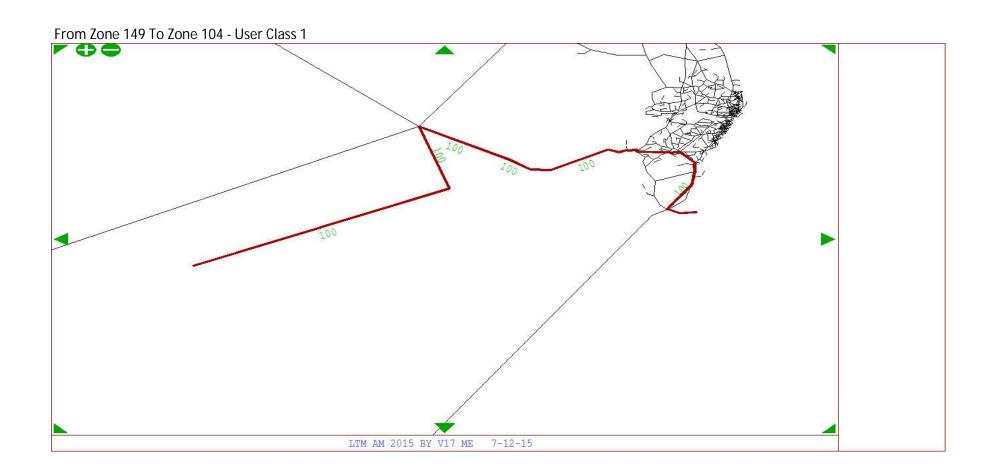
From Zone 149 To Zone 101 - User Class 1

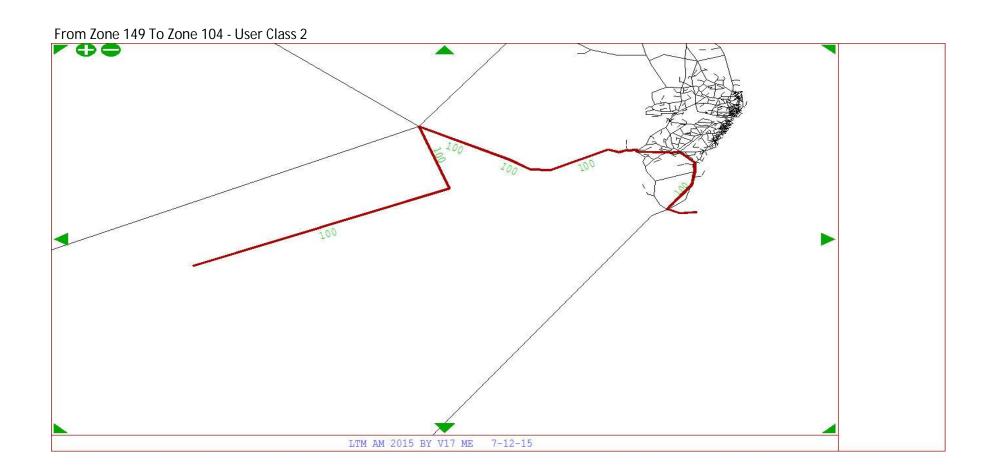
From Zone 149 To Zone 101 - User Class 2

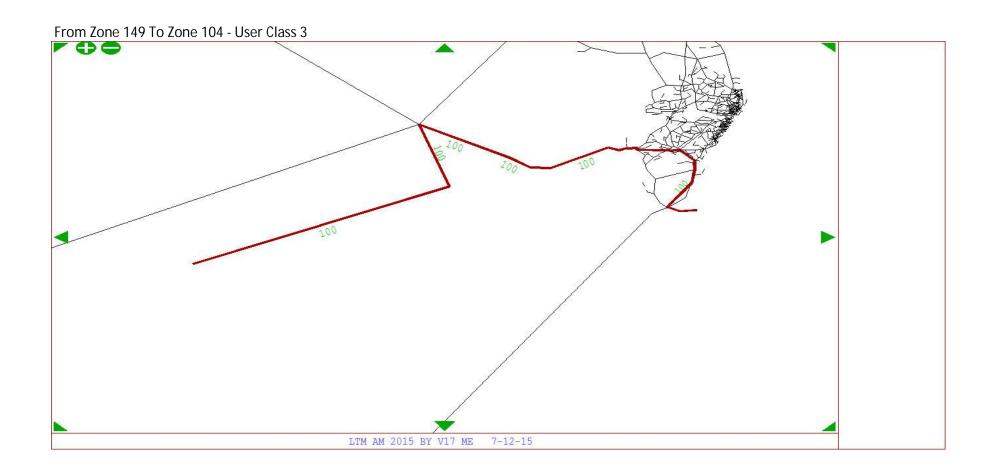
From Zone 149 To Zone 101 - User Class 3

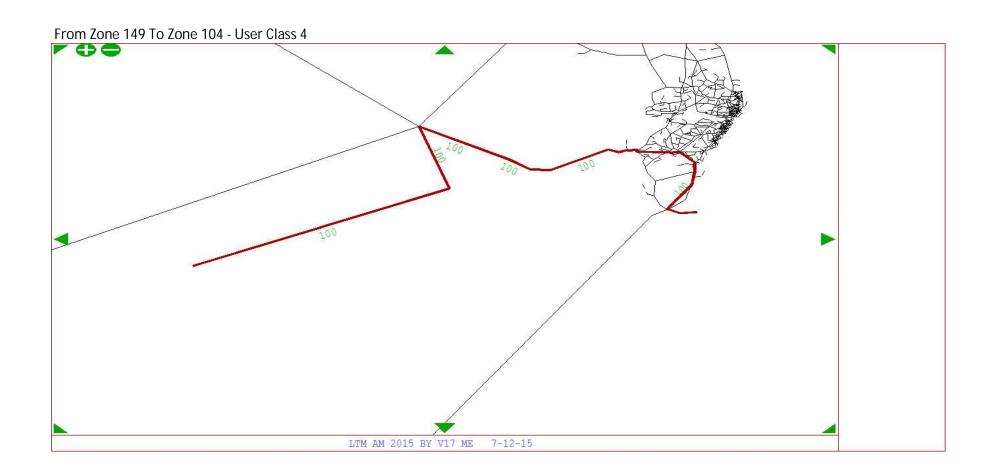
From Zone 149 To Zone 101 - User Class 4

From Zone 149 To Zone 101 - User Class 5



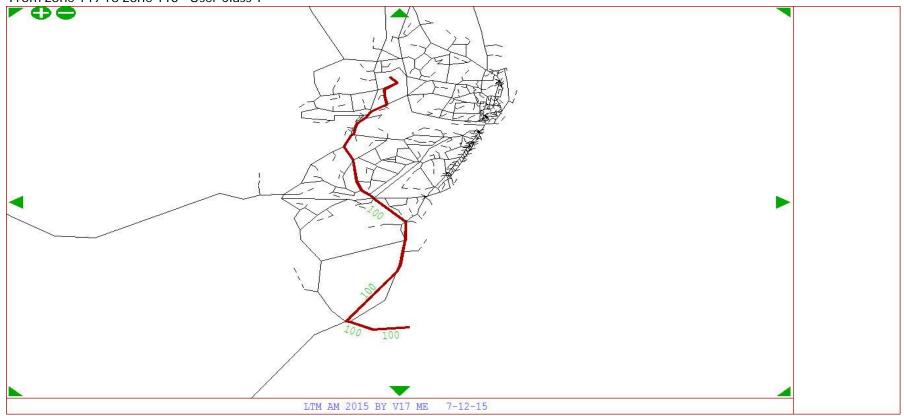




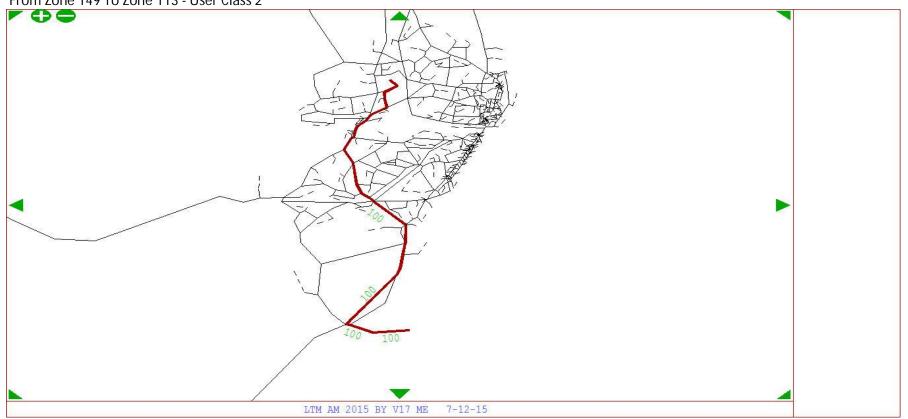


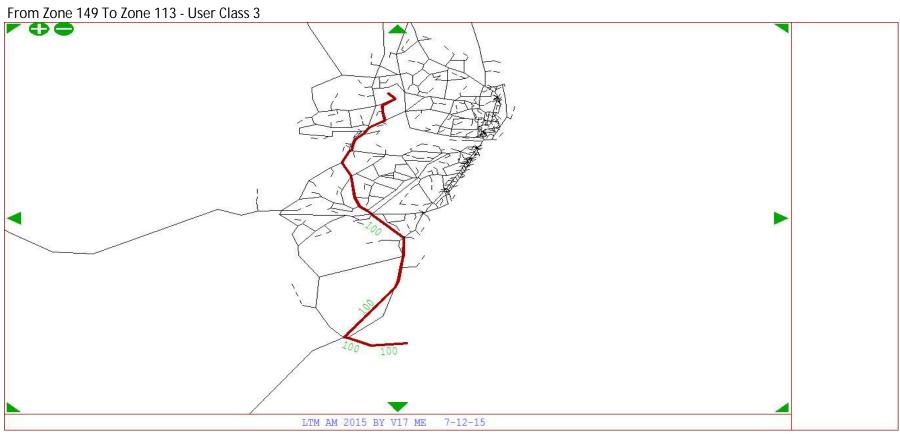
From Zone 149 To Zone 104 - User Class 5 LTM AM 2015 BY V17 ME

From Zone 149 To Zone 113 - User Class 1



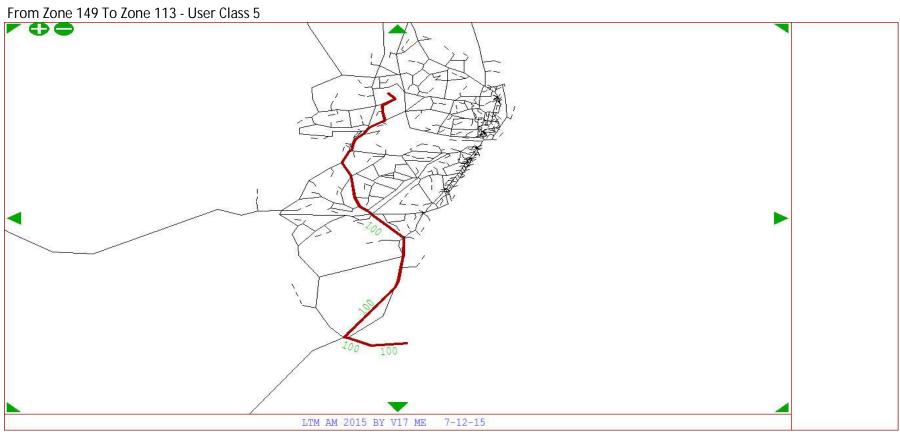
From Zone 149 To Zone 113 - User Class 2





From Zone 149 To Zone 113 - User Class 4





From Zone 149 To Zone 114 - User Class 1 LTM AM 2015 BY V17 ME 7-12-15

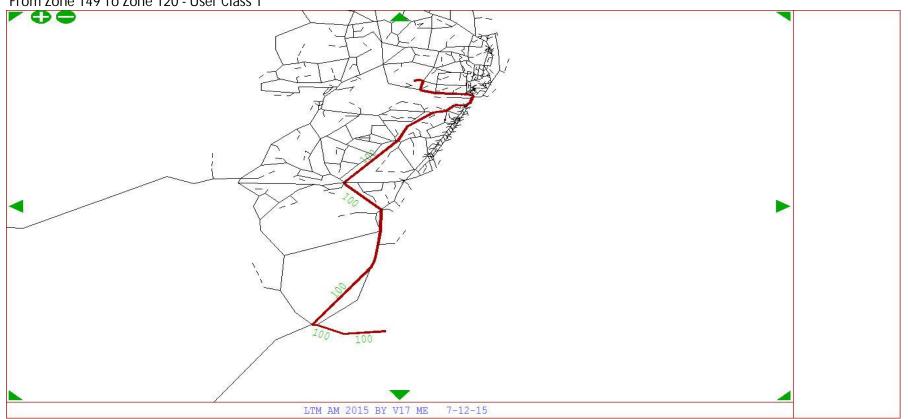
From Zone 149 To Zone 114 - User Class 2 LTM AM 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 114 - User Class 3

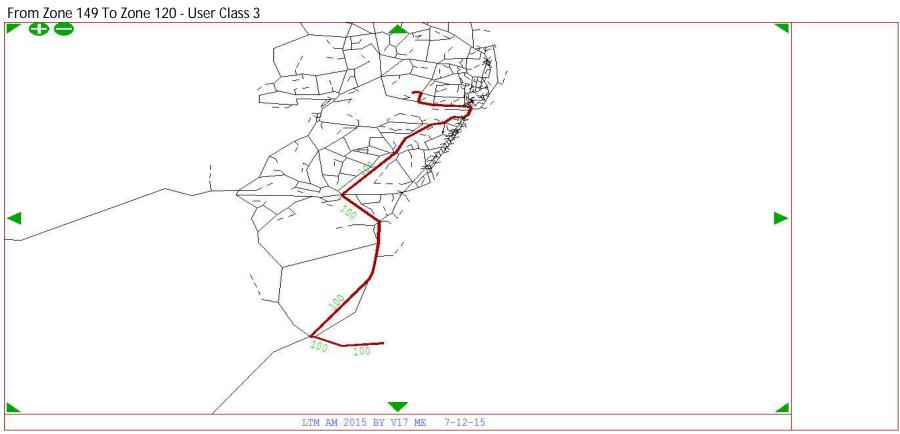
From Zone 149 To Zone 114 - User Class 4 LTM AM 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 114 - User Class 5

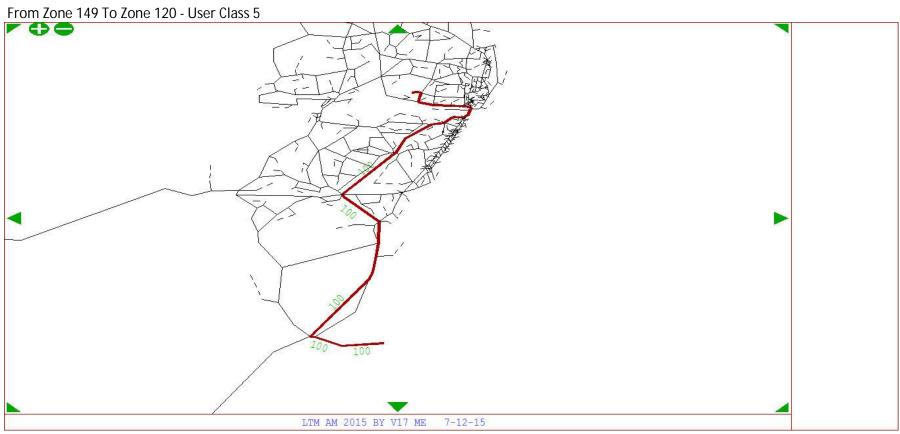
From Zone 149 To Zone 120 - User Class 1



From Zone 149 To Zone 120 - User Class 2



From Zone 149 To Zone 120 - User Class 4



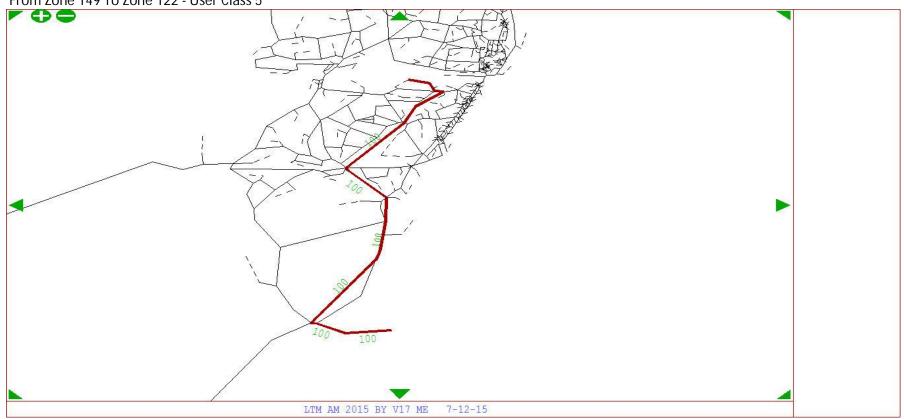
From Zone 149 To Zone 122 - User Class 1

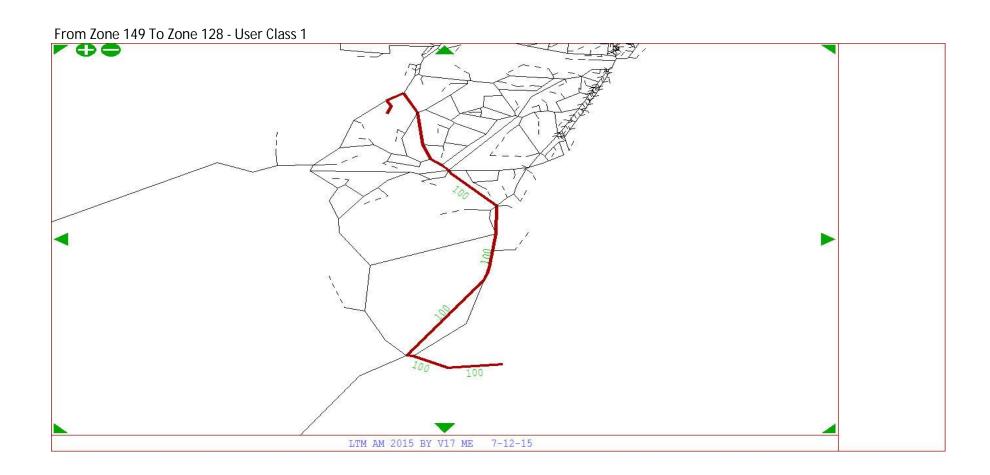
From Zone 149 To Zone 122 - User Class 2

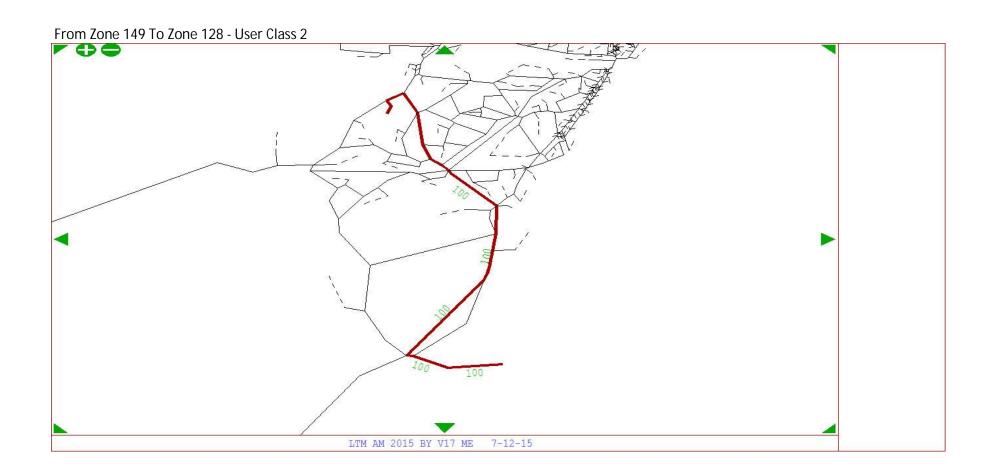
From Zone 149 To Zone 122 - User Class 3

From Zone 149 To Zone 122 - User Class 4

From Zone 149 To Zone 122 - User Class 5





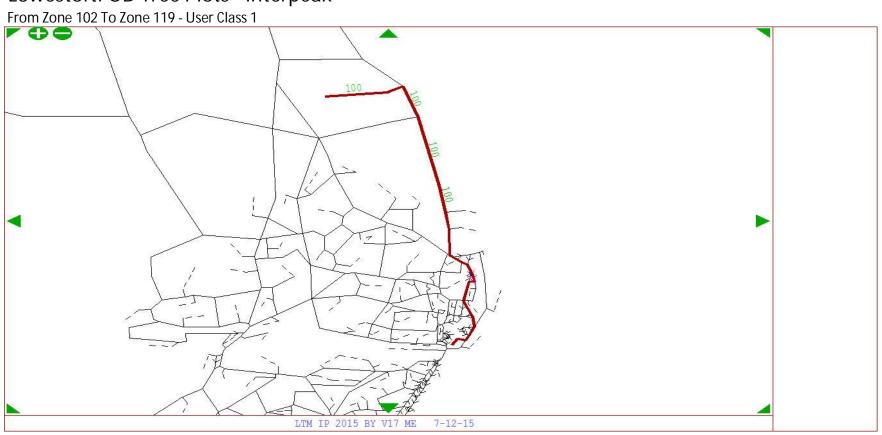


From Zone 149 To Zone 128 - User Class 3 LTM AM 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 128 - User Class 4 LTM AM 2015 BY V17 ME 7-12-15

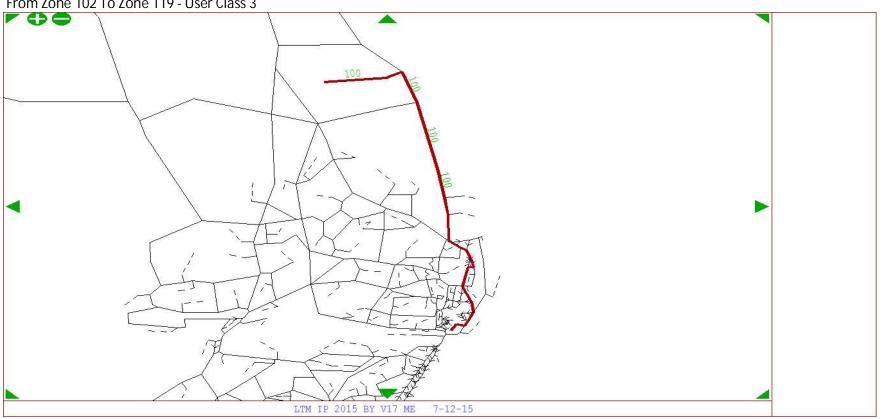
From Zone 149 To Zone 128 - User Class 5 LTM AM 2015 BY V17 ME 7-12-15

## Lowestoft: OD Tree Plots - Interpeak



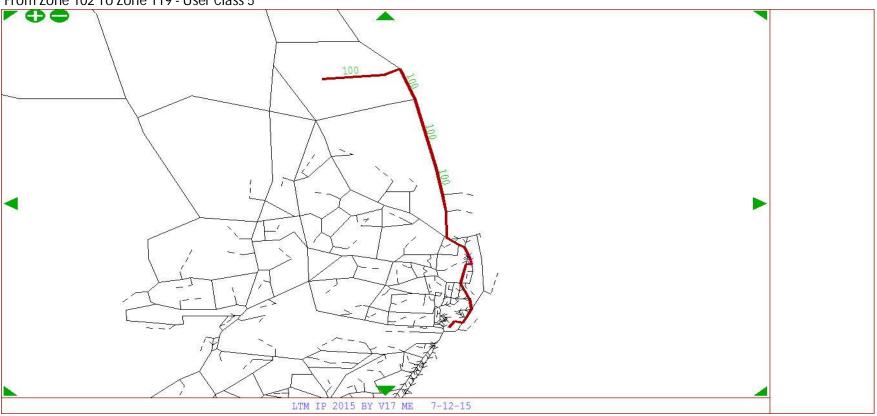
From Zone 102 To Zone 119 - User Class 2

From Zone 102 To Zone 119 - User Class 3



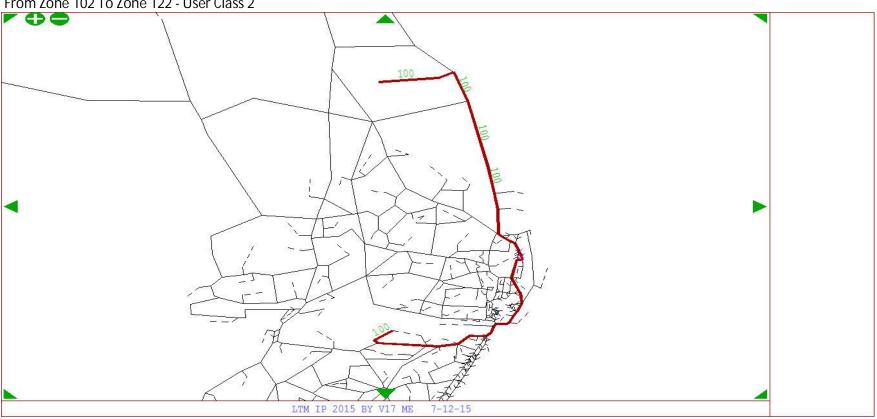
From Zone 102 To Zone 119 - User Class 4

From Zone 102 To Zone 119 - User Class 5

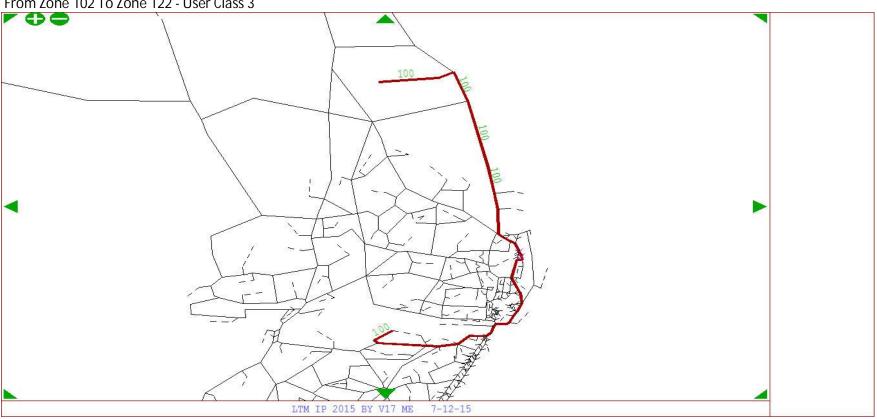


From Zone 102 To Zone 122 - User Class 1

From Zone 102 To Zone 122 - User Class 2

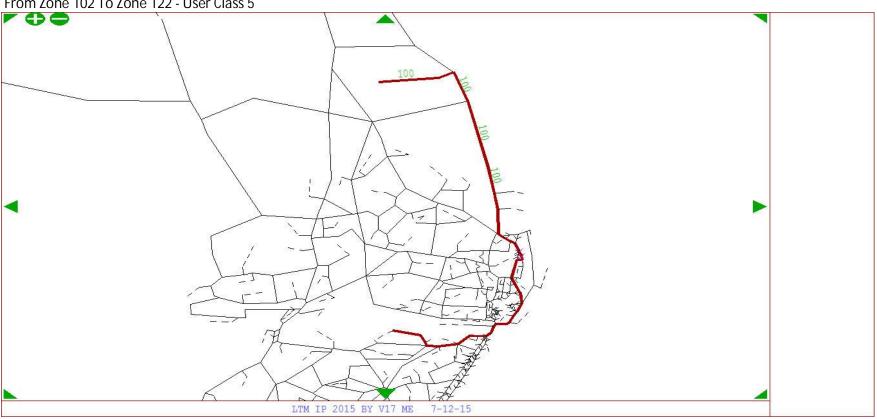


From Zone 102 To Zone 122 - User Class 3



From Zone 102 To Zone 122 - User Class 4

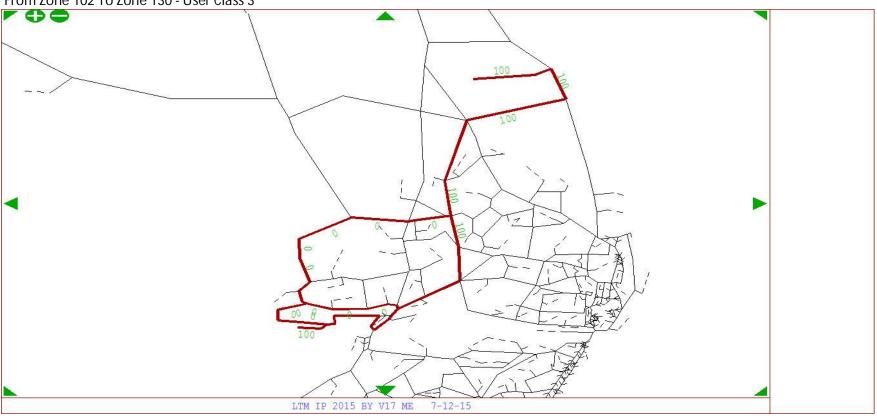
From Zone 102 To Zone 122 - User Class 5



From Zone 102 To Zone 130 - User Class 1

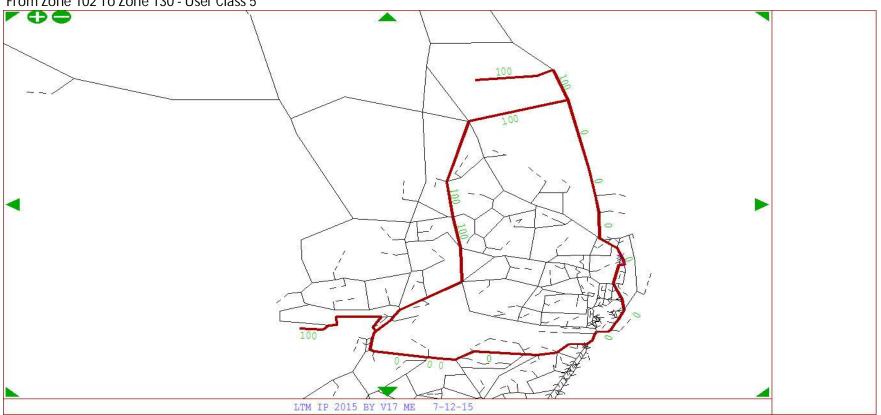
From Zone 102 To Zone 130 - User Class 2

From Zone 102 To Zone 130 - User Class 3

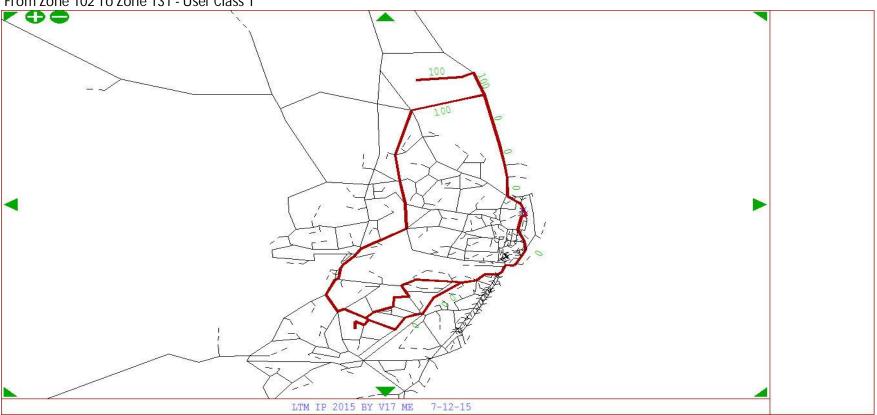


From Zone 102 To Zone 130 - User Class 4

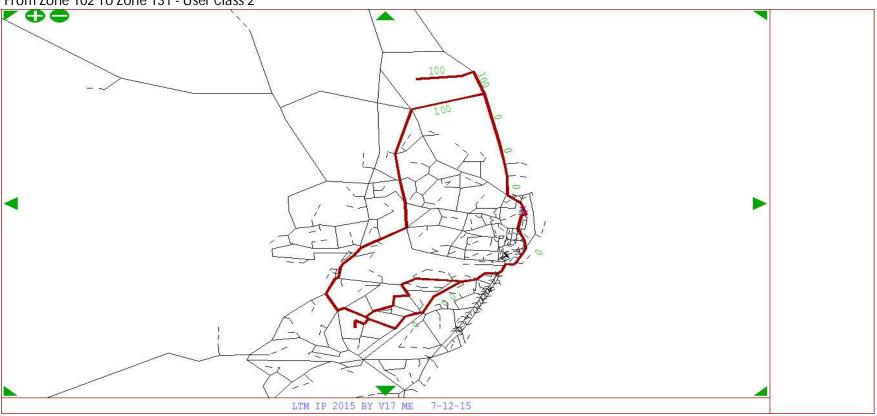
From Zone 102 To Zone 130 - User Class 5



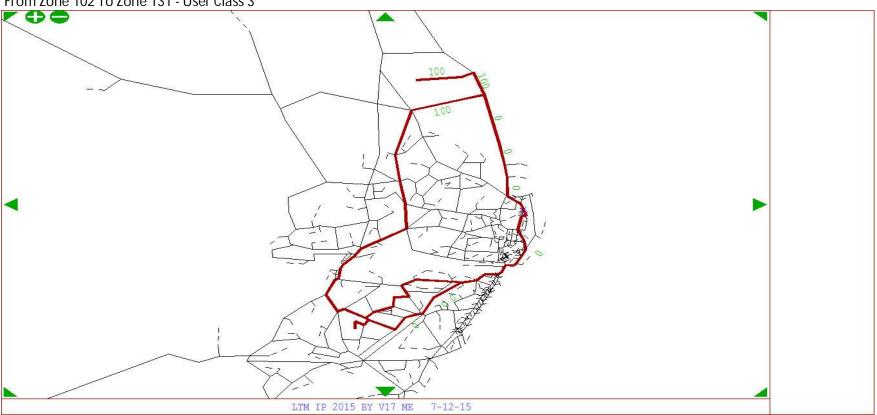
From Zone 102 To Zone 131 - User Class 1



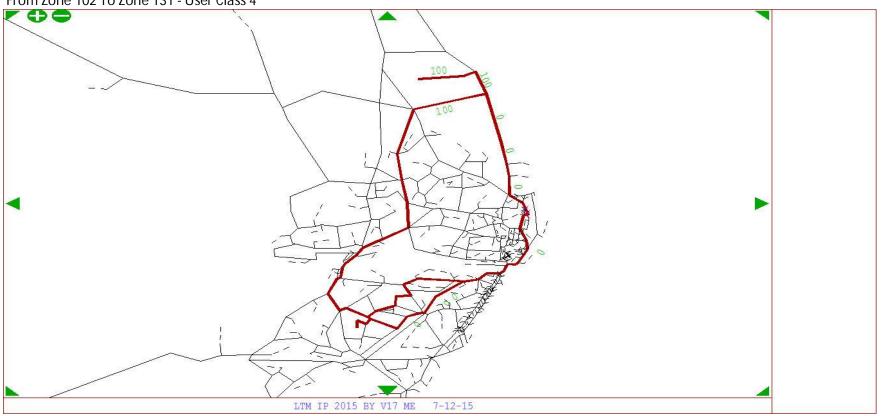
From Zone 102 To Zone 131 - User Class 2



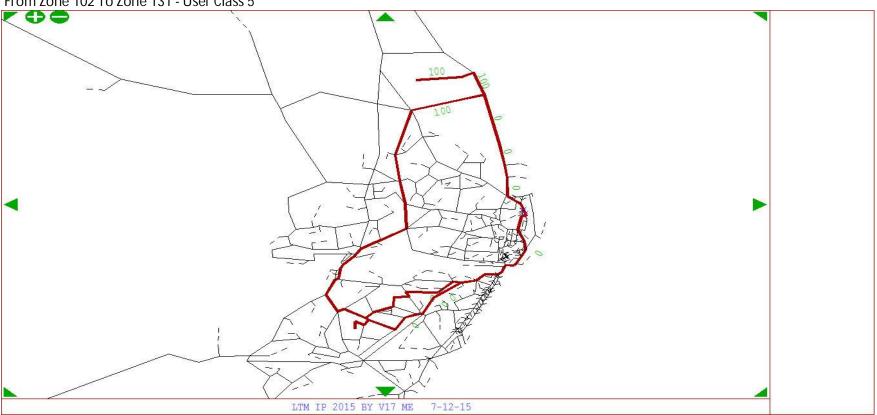
From Zone 102 To Zone 131 - User Class 3



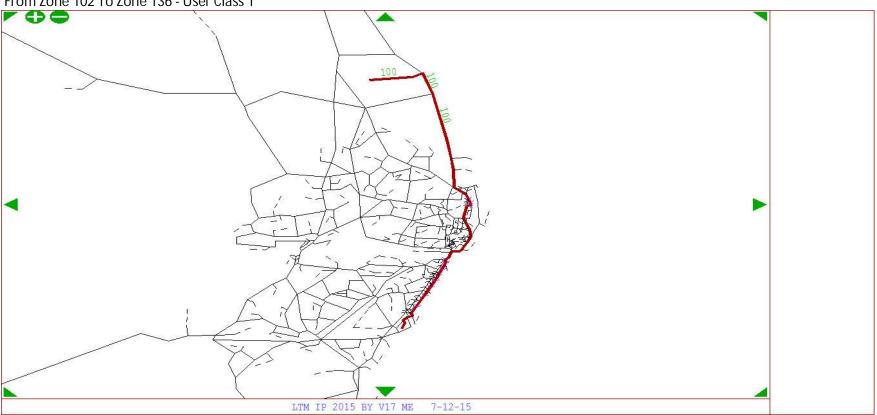
From Zone 102 To Zone 131 - User Class 4



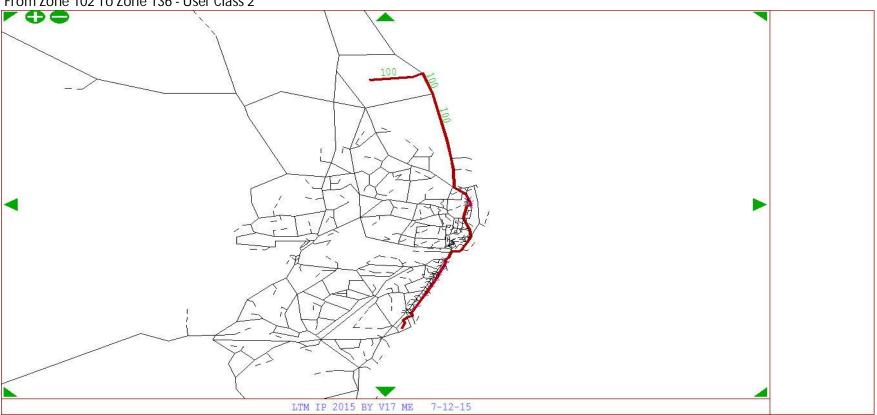
From Zone 102 To Zone 131 - User Class 5



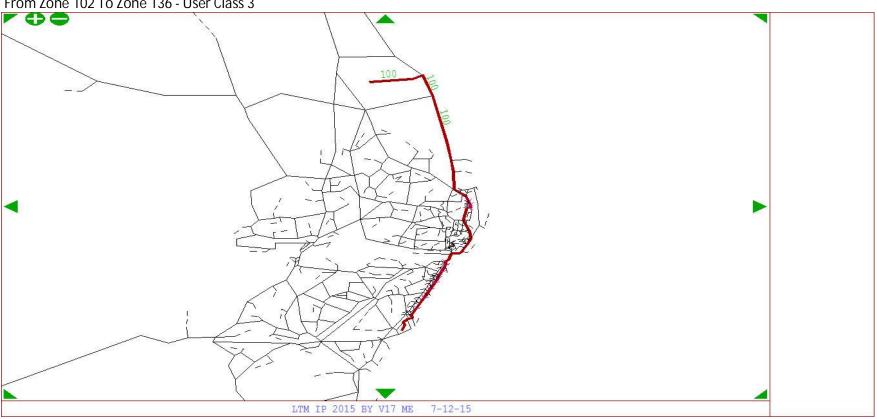
From Zone 102 To Zone 136 - User Class 1



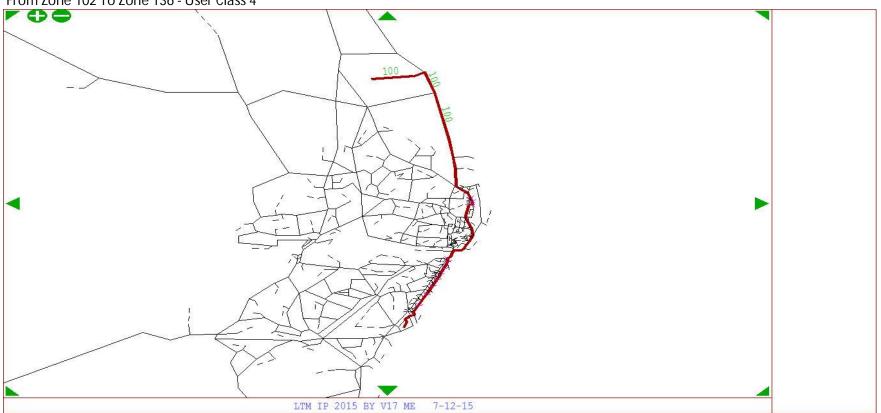
From Zone 102 To Zone 136 - User Class 2



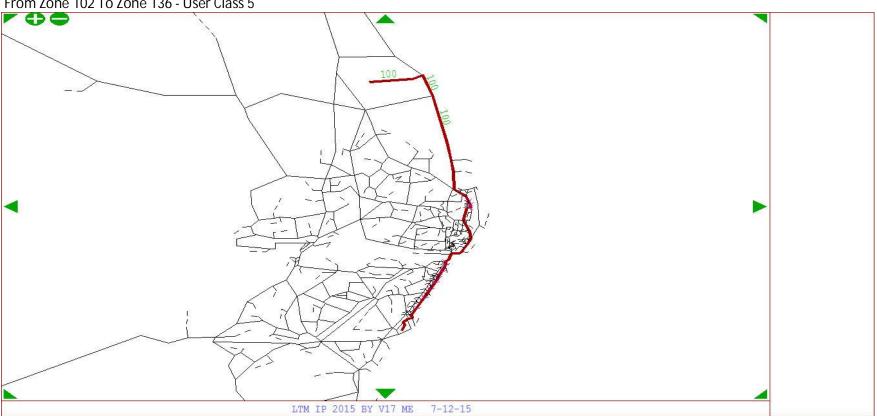
From Zone 102 To Zone 136 - User Class 3

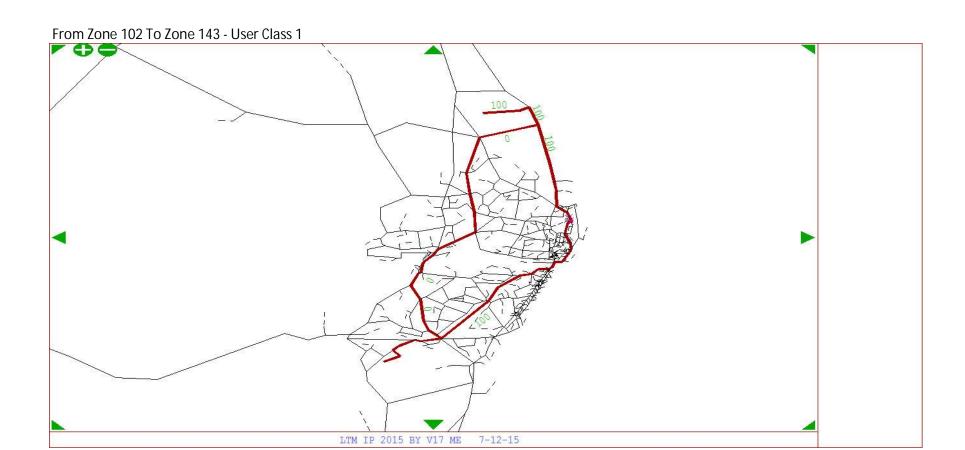


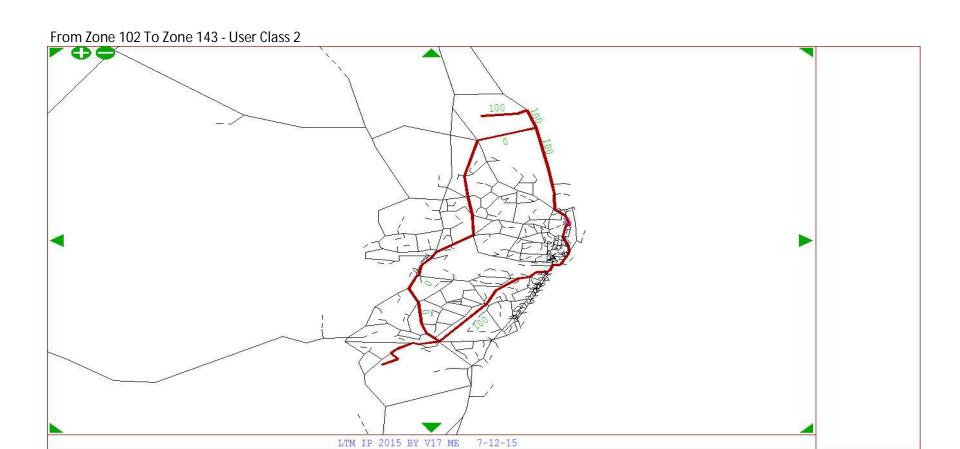
From Zone 102 To Zone 136 - User Class 4



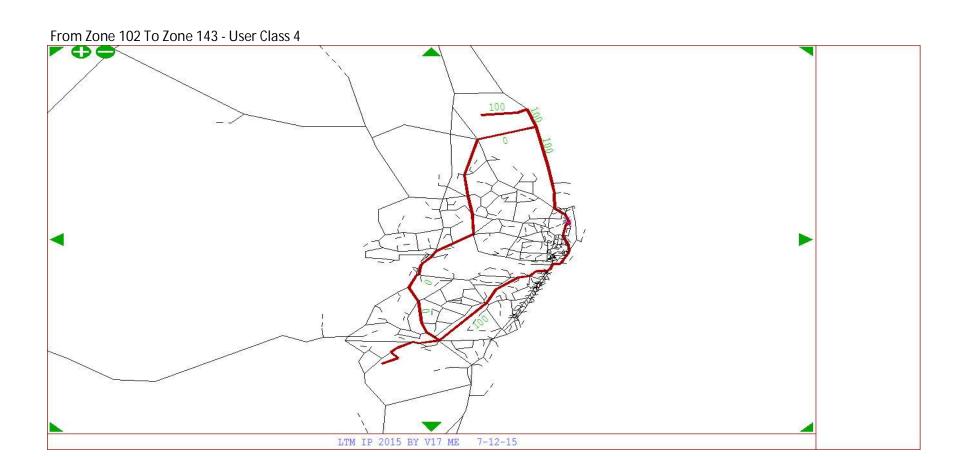
From Zone 102 To Zone 136 - User Class 5







From Zone 102 To Zone 143 - User Class 3



From Zone 102 To Zone 143 - User Class 5

From Zone 102 To Zone 149 - User Class 1 LTM IP 2015 BY V17 ME 7-12-15

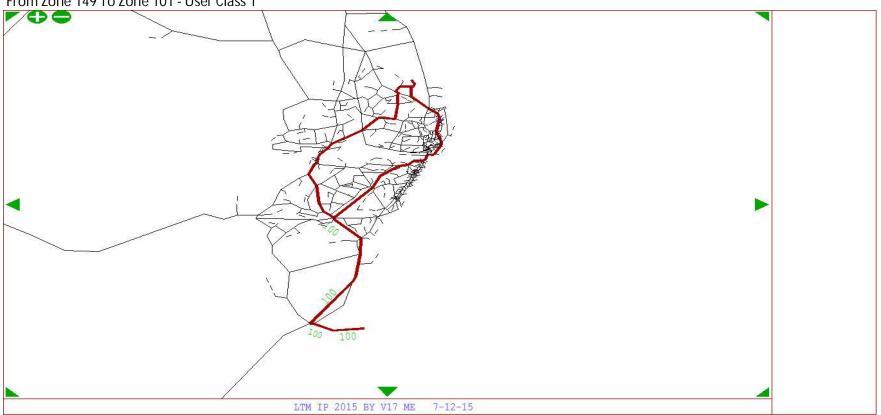
From Zone 102 To Zone 149 - User Class 2

From Zone 102 To Zone 149 - User Class 3

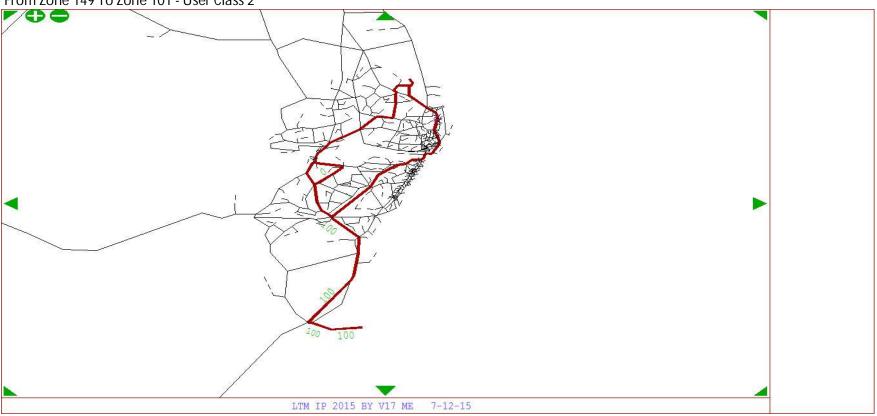
From Zone 102 To Zone 149 - User Class 4 LTM IP 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 5

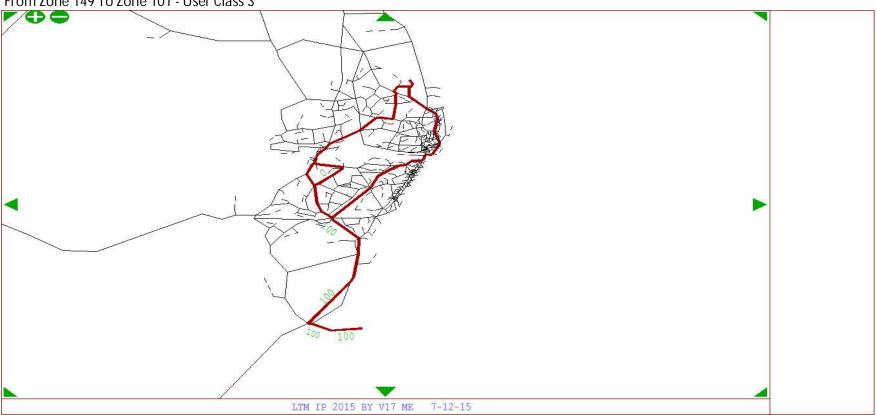
From Zone 149 To Zone 101 - User Class 1



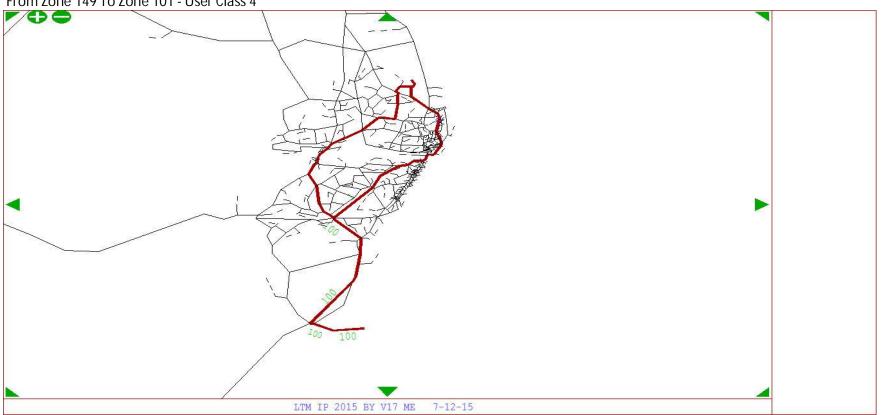
From Zone 149 To Zone 101 - User Class 2



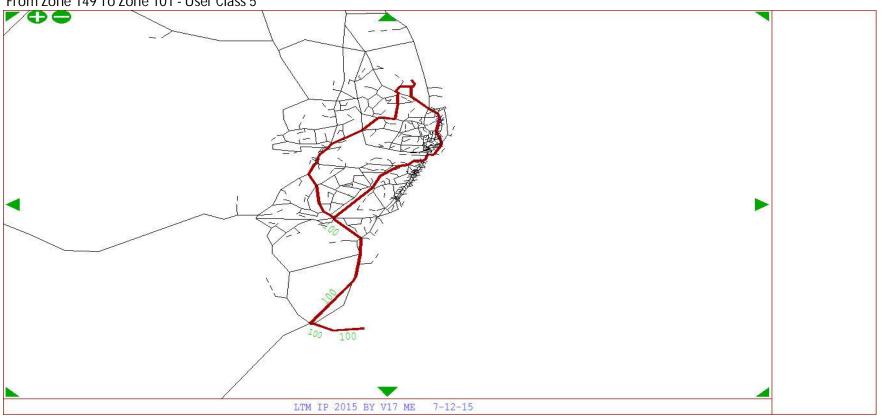
From Zone 149 To Zone 101 - User Class 3



From Zone 149 To Zone 101 - User Class 4



From Zone 149 To Zone 101 - User Class 5



From Zone 149 To Zone 104 - User Class 1 LTM IP 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 104 - User Class 2 LTM IP 2015 BY V17 ME 7-12-15

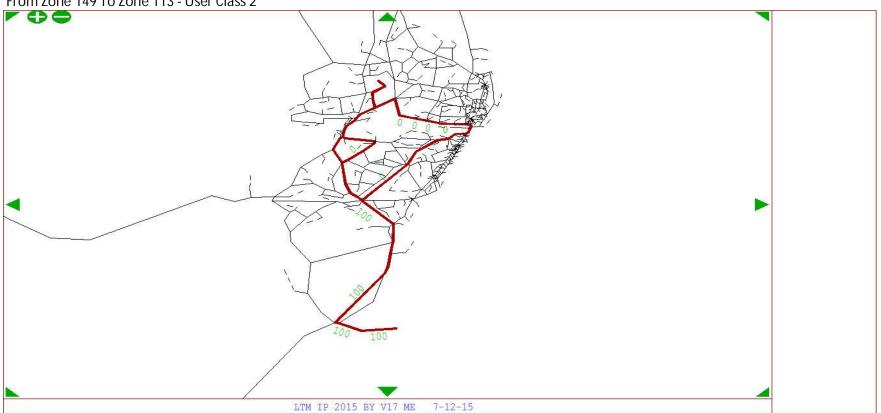
From Zone 149 To Zone 104 - User Class 3 LTM IP 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 104 - User Class 4 LTM IP 2015 BY V17 ME 7-12-15

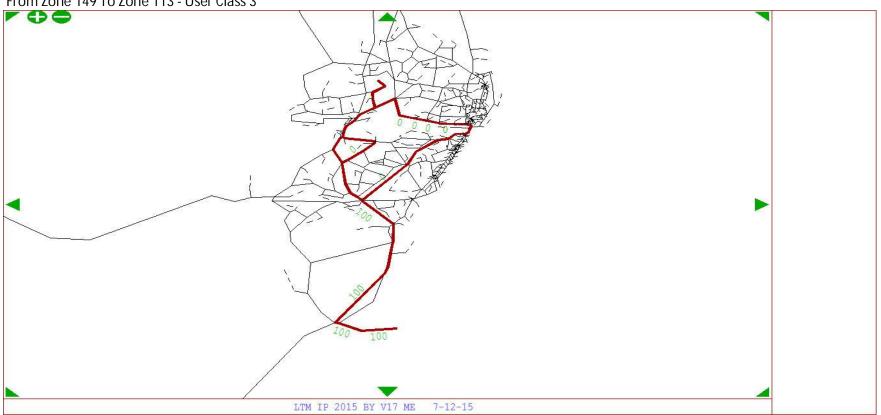
From Zone 149 To Zone 104 - User Class 5

From Zone 149 To Zone 113 - User Class 1

From Zone 149 To Zone 113 - User Class 2

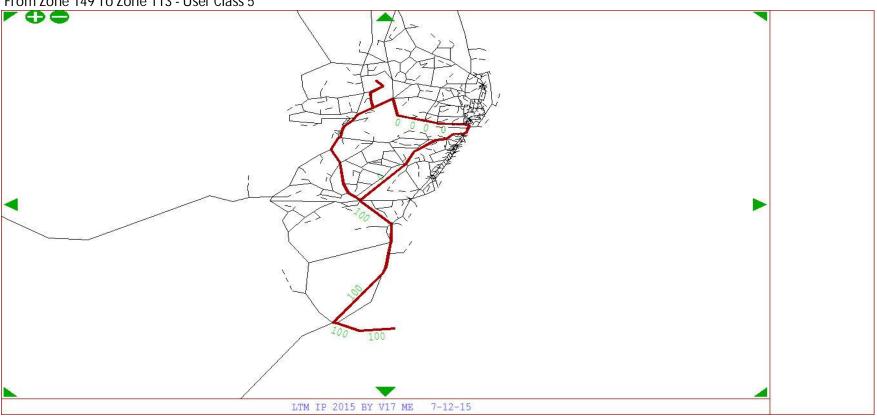


From Zone 149 To Zone 113 - User Class 3

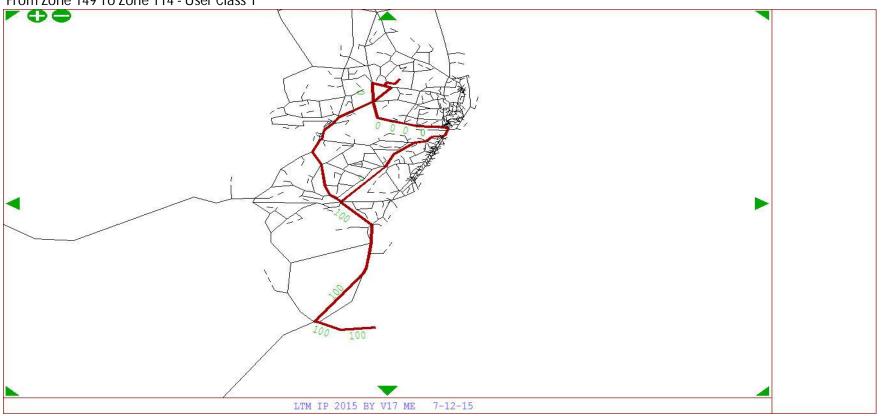


From Zone 149 To Zone 113 - User Class 4

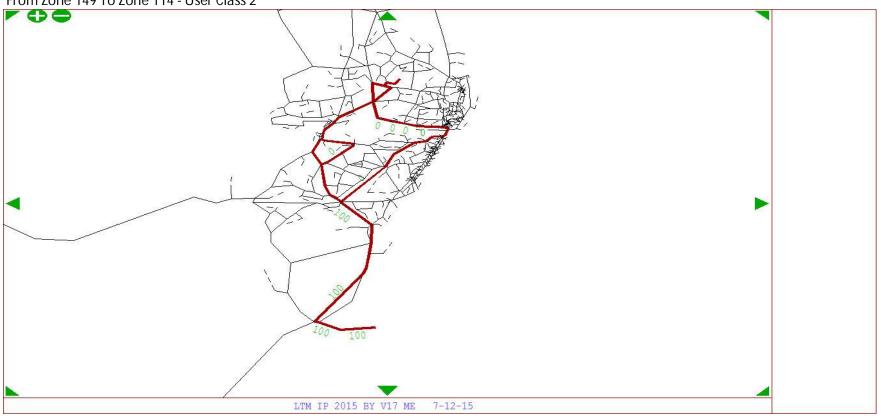
From Zone 149 To Zone 113 - User Class 5



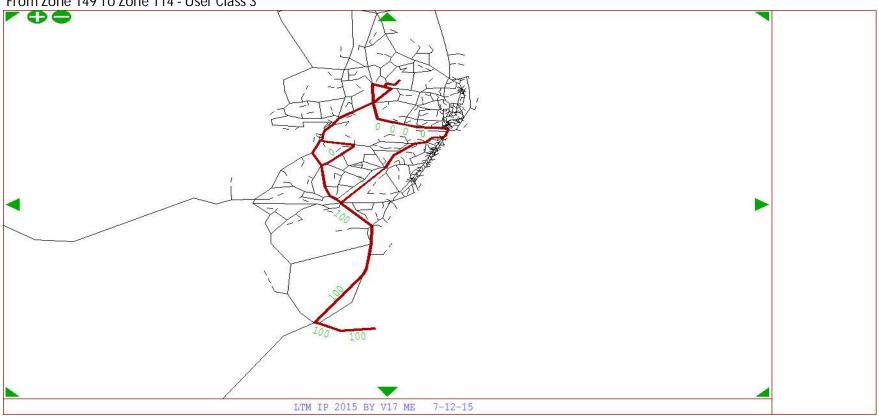
From Zone 149 To Zone 114 - User Class 1



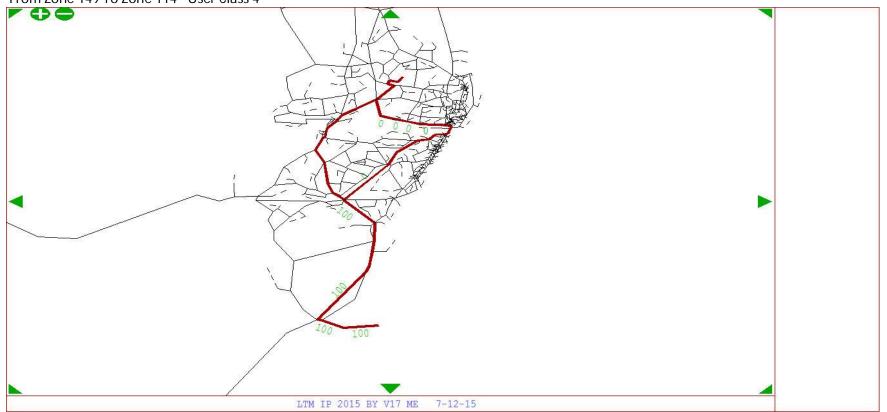
From Zone 149 To Zone 114 - User Class 2



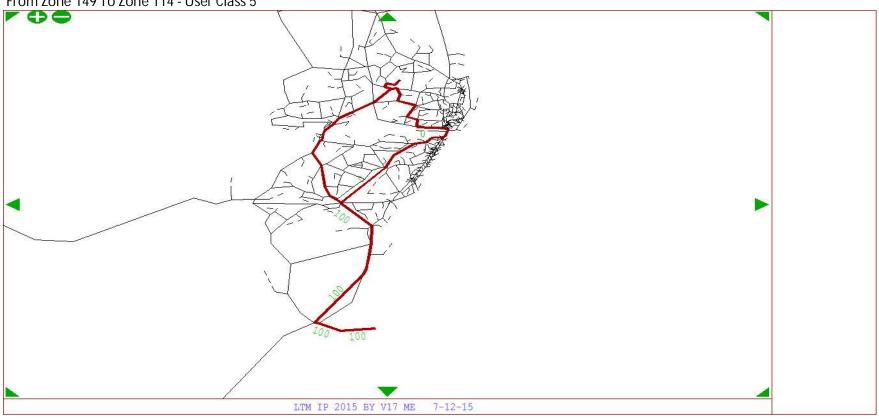
From Zone 149 To Zone 114 - User Class 3



From Zone 149 To Zone 114 - User Class 4



From Zone 149 To Zone 114 - User Class 5



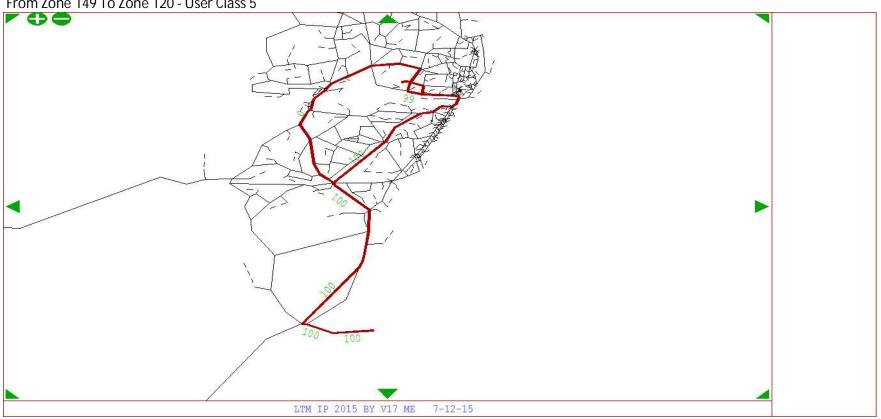
From Zone 149 To Zone 120 - User Class 1

From Zone 149 To Zone 120 - User Class 2

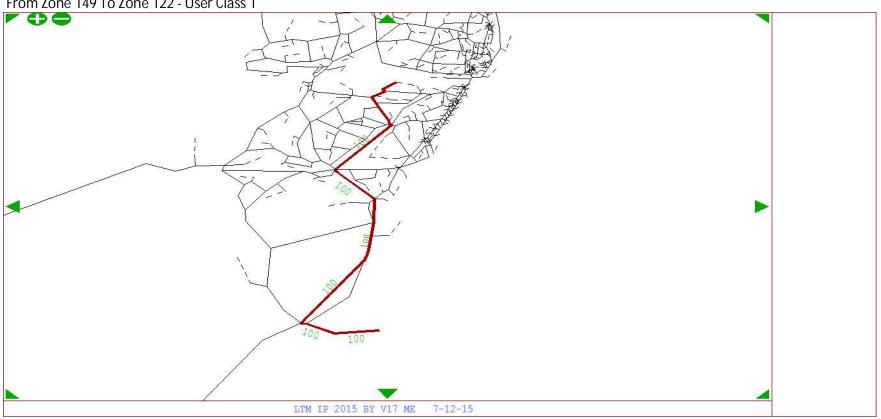
From Zone 149 To Zone 120 - User Class 3

From Zone 149 To Zone 120 - User Class 4

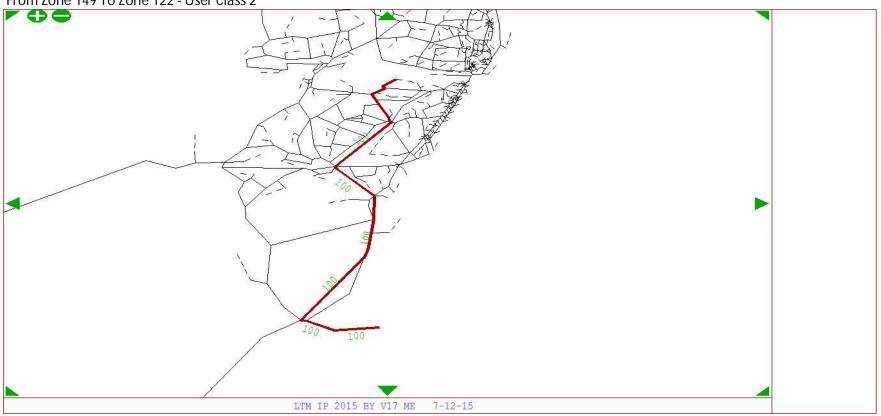
From Zone 149 To Zone 120 - User Class 5



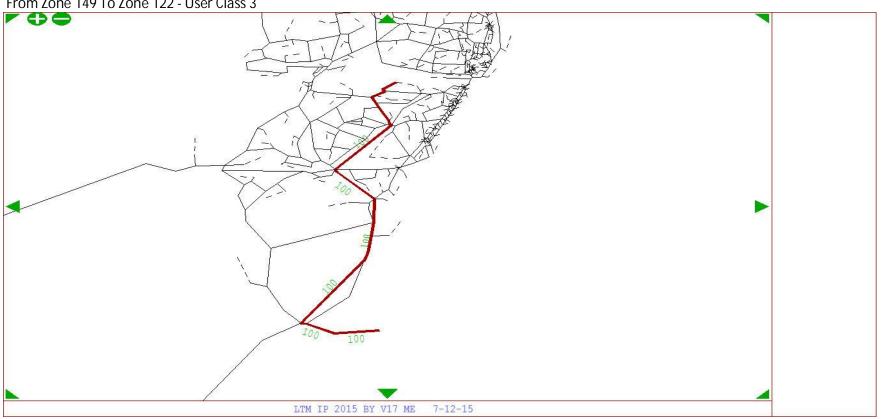
From Zone 149 To Zone 122 - User Class 1



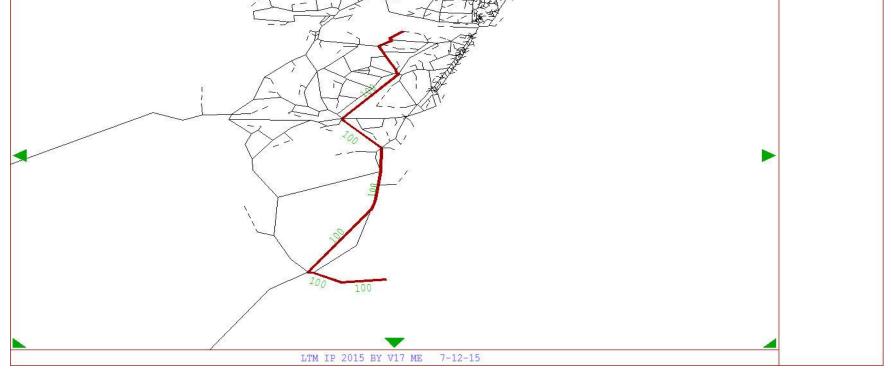
From Zone 149 To Zone 122 - User Class 2



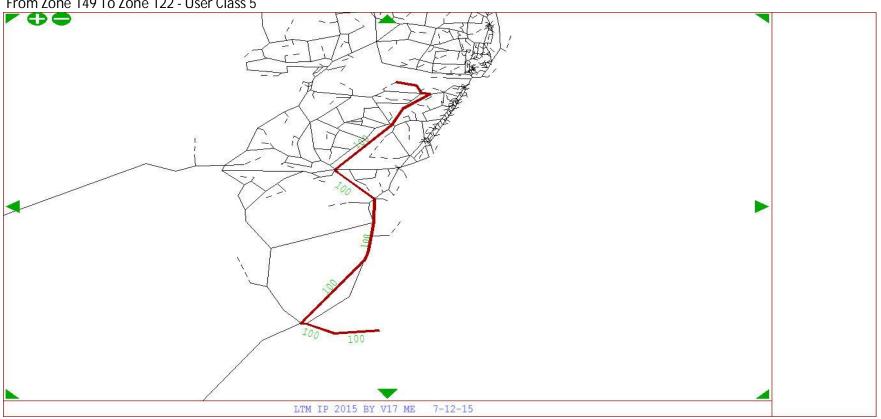
From Zone 149 To Zone 122 - User Class 3



From Zone 149 To Zone 122 - User Class 4



From Zone 149 To Zone 122 - User Class 5



From Zone 149 To Zone 128 - User Class 1 LTM IP 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 128 - User Class 2 

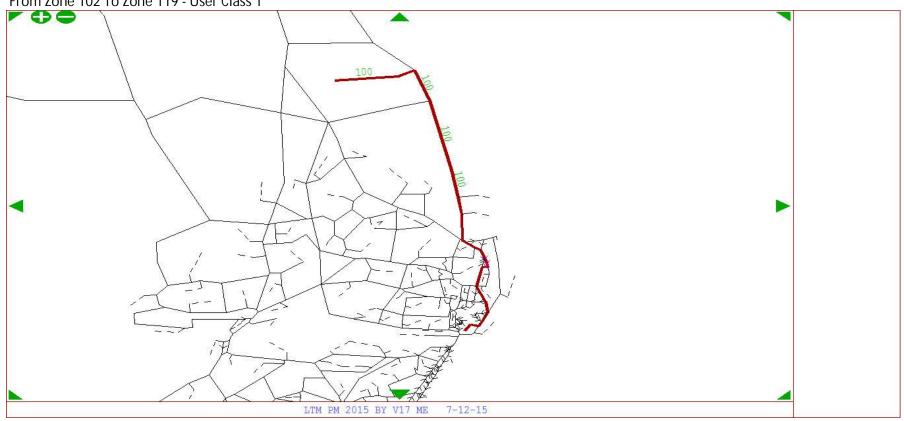
From Zone 149 To Zone 128 - User Class 3

From Zone 149 To Zone 128 - User Class 4 LTM IP 2015 BY V17 ME 7-12-15

From Zone 149 To Zone 128 - User Class 5

## Lowestoft: OD Tree Plots - PM Peak

From Zone 102 To Zone 119 - User Class 1

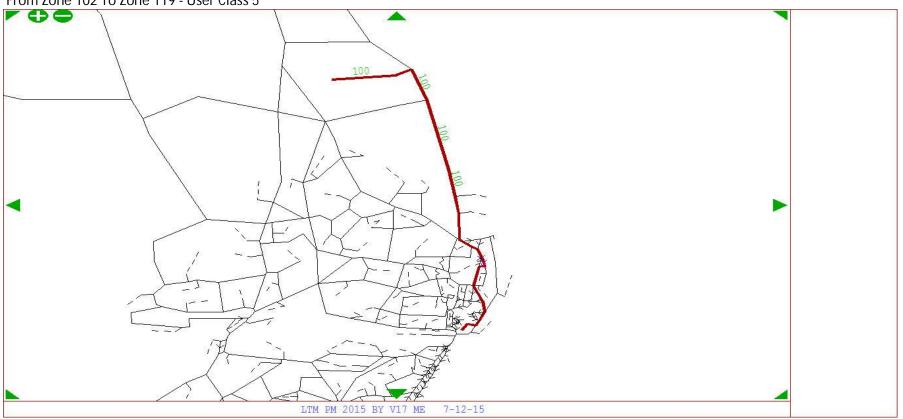


From Zone 102 To Zone 119 - User Class 2

From Zone 102 To Zone 119 - User Class 3

From Zone 102 To Zone 119 - User Class 4

From Zone 102 To Zone 119 - User Class 5



From Zone 102 To Zone 122 - User Class 1

From Zone 102 To Zone 122 - User Class 2

From Zone 102 To Zone 122 - User Class 3

From Zone 102 To Zone 122 - User Class 4

From Zone 102 To Zone 122 - User Class 5

From Zone 130 - User Class 1

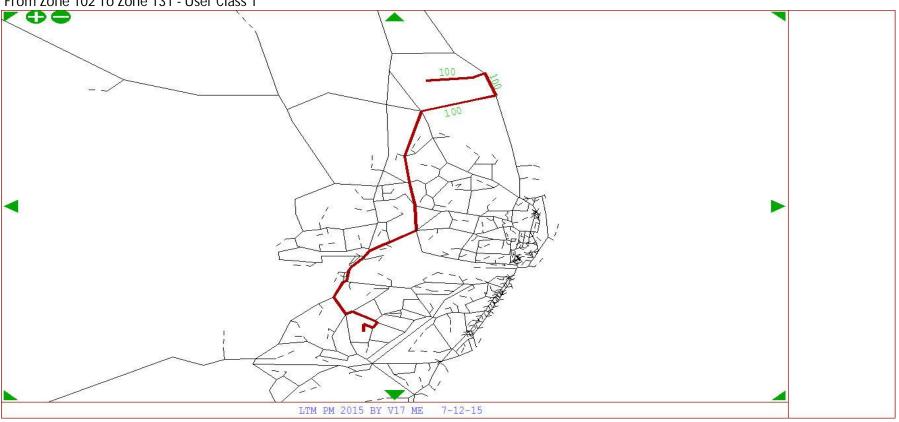
From Zone 102 To Zone 130 - User Class 2

From Zone 102 To Zone 130 - User Class 3

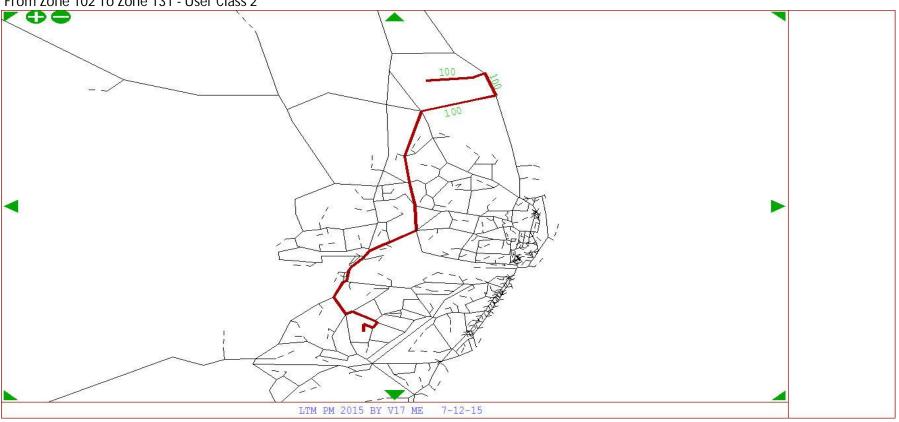
From Zone 102 To Zone 130 - User Class 4

From Zone 102 To Zone 130 - User Class 5

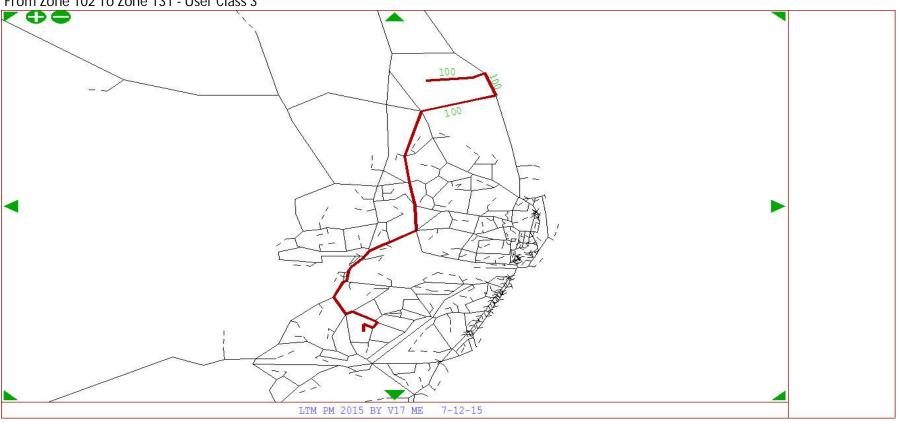
From Zone 102 To Zone 131 - User Class 1



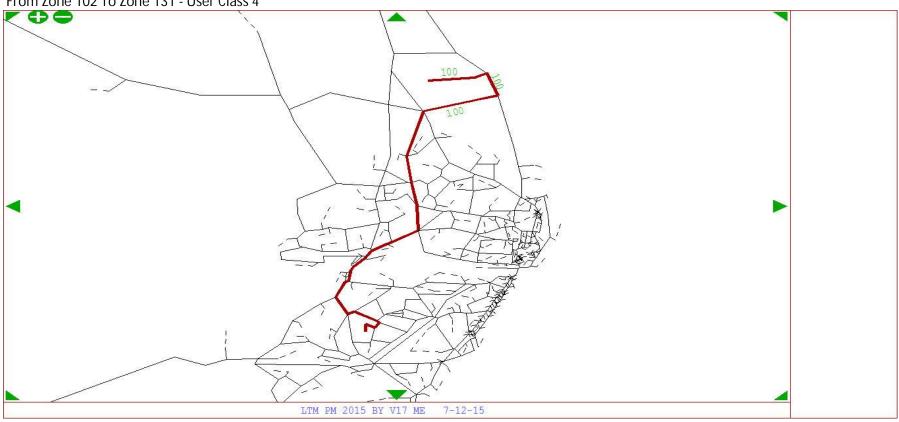
From Zone 102 To Zone 131 - User Class 2



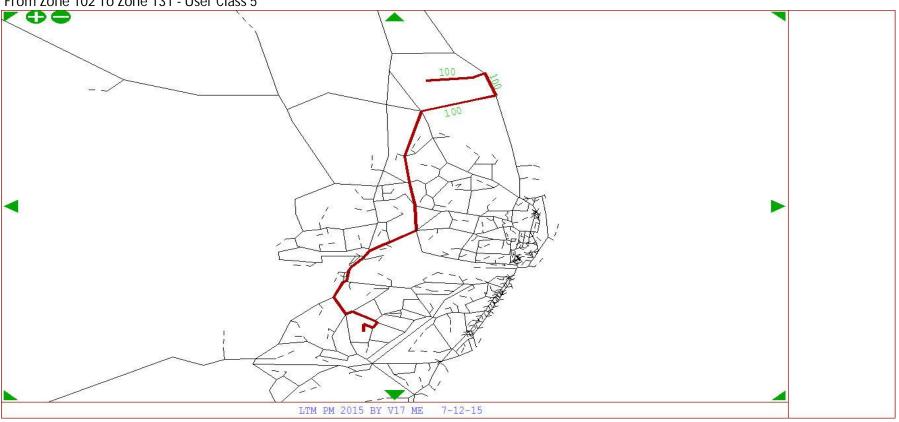
From Zone 102 To Zone 131 - User Class 3



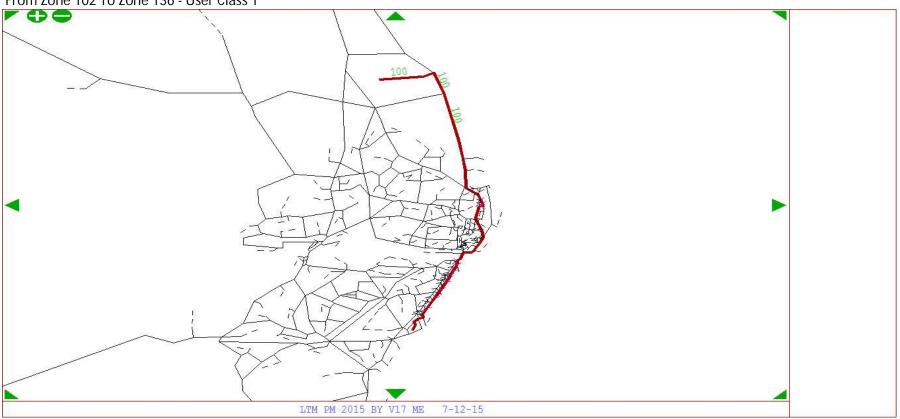
From Zone 102 To Zone 131 - User Class 4



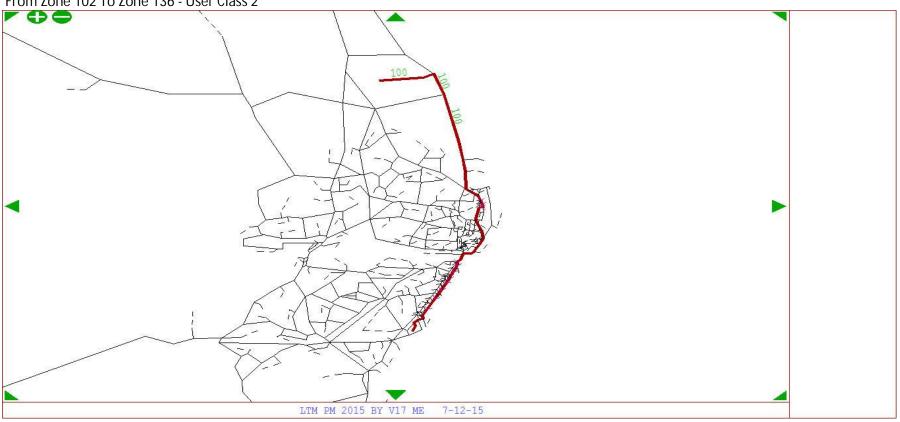
From Zone 102 To Zone 131 - User Class 5



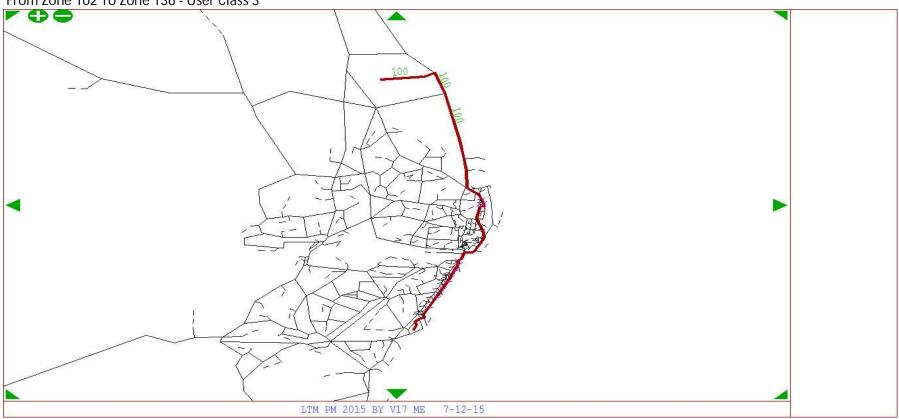
From Zone 102 To Zone 136 - User Class 1



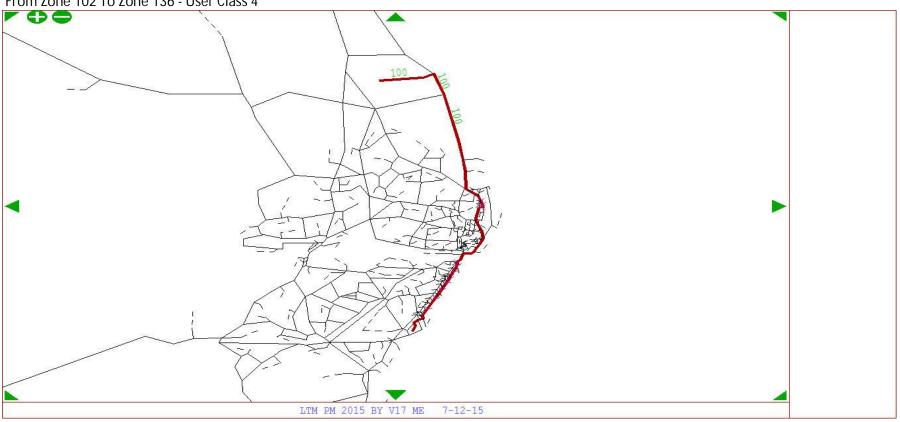
From Zone 102 To Zone 136 - User Class 2



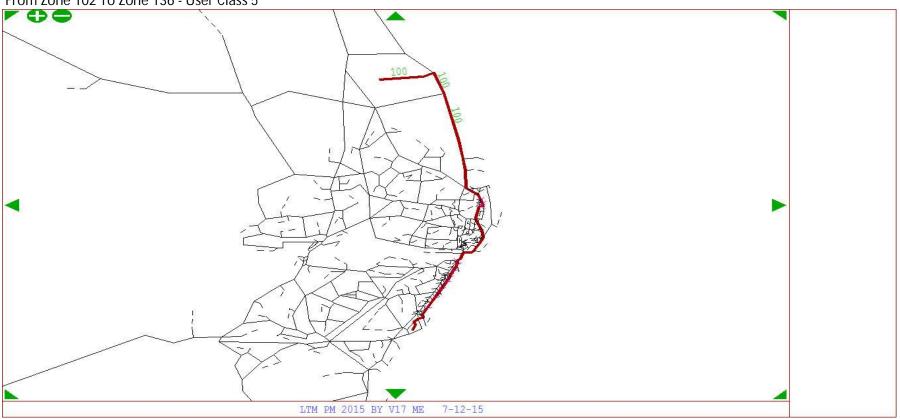
From Zone 102 To Zone 136 - User Class 3

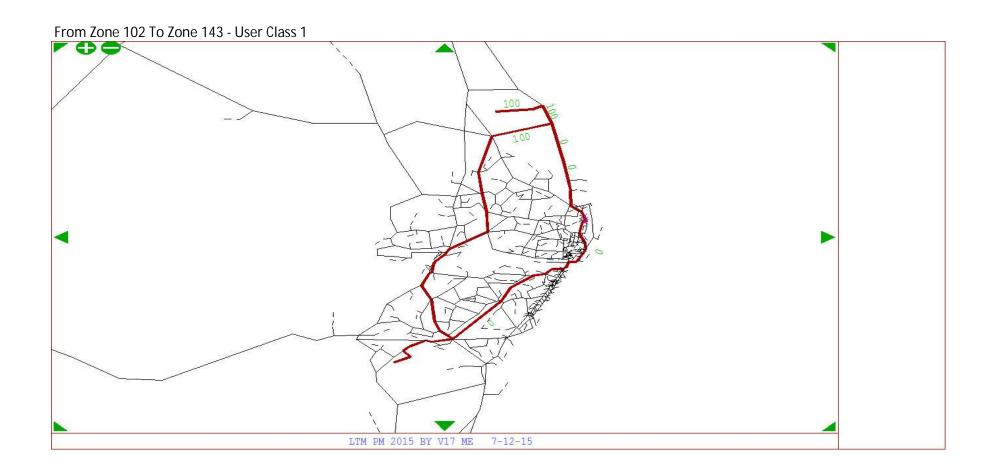


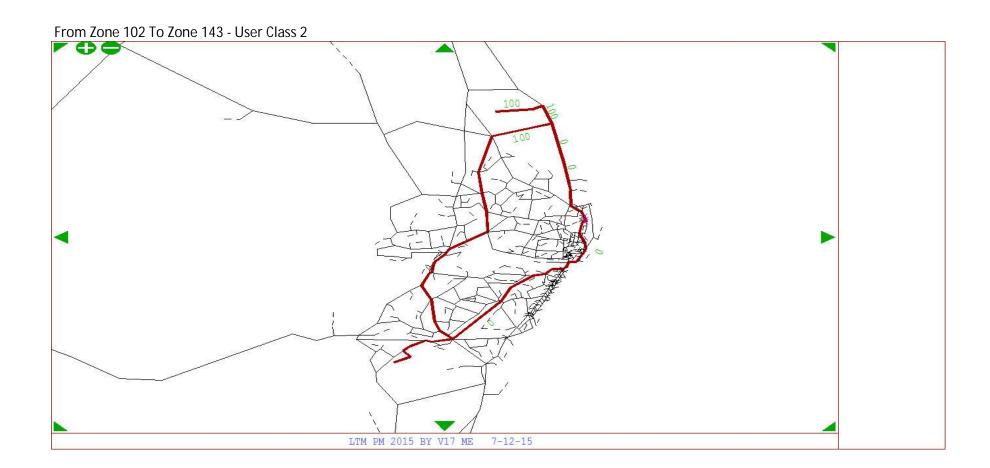
From Zone 102 To Zone 136 - User Class 4

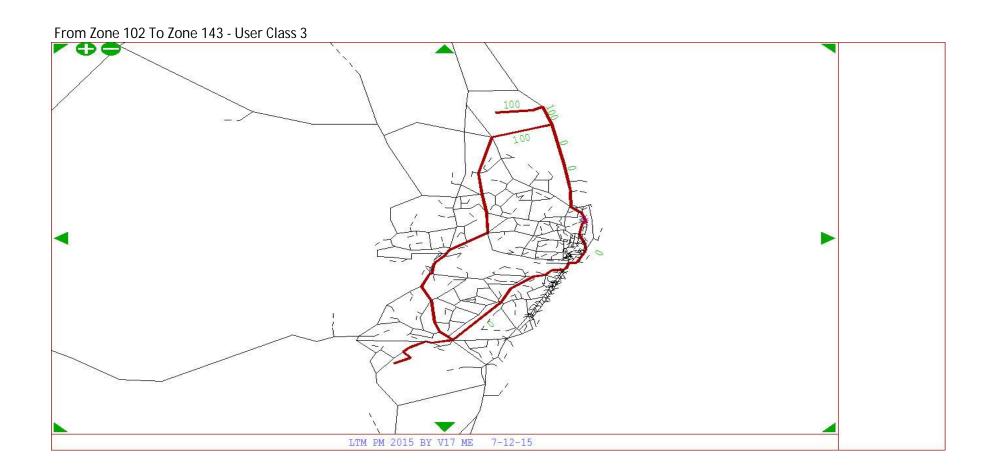


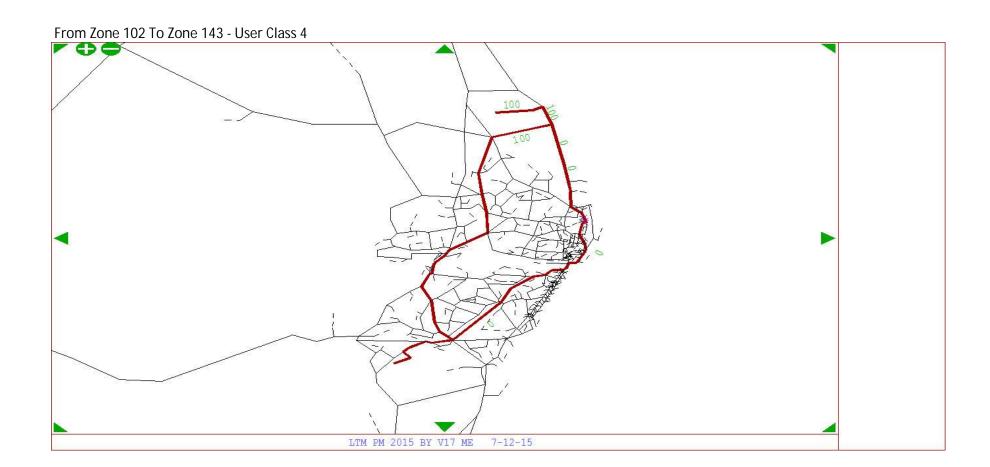
From Zone 102 To Zone 136 - User Class 5











From Zone 102 To Zone 143 - User Class 5 LTM PM 2015 BY V17 ME

From Zone 102 To Zone 149 - User Class 1 

LTM PM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 2 LTM PM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 3 LTM PM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 4 LTM PM 2015 BY V17 ME 7-12-15

From Zone 102 To Zone 149 - User Class 5 

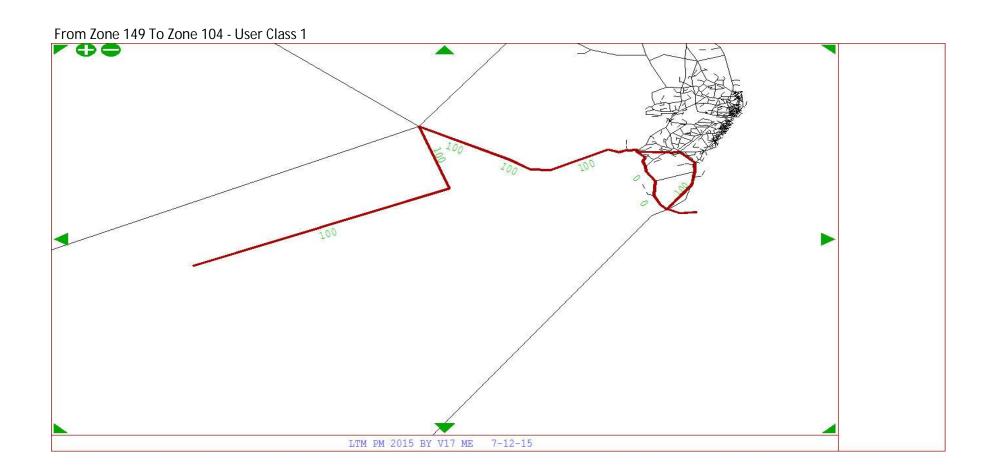
From Zone 149 To Zone 101 - User Class 1

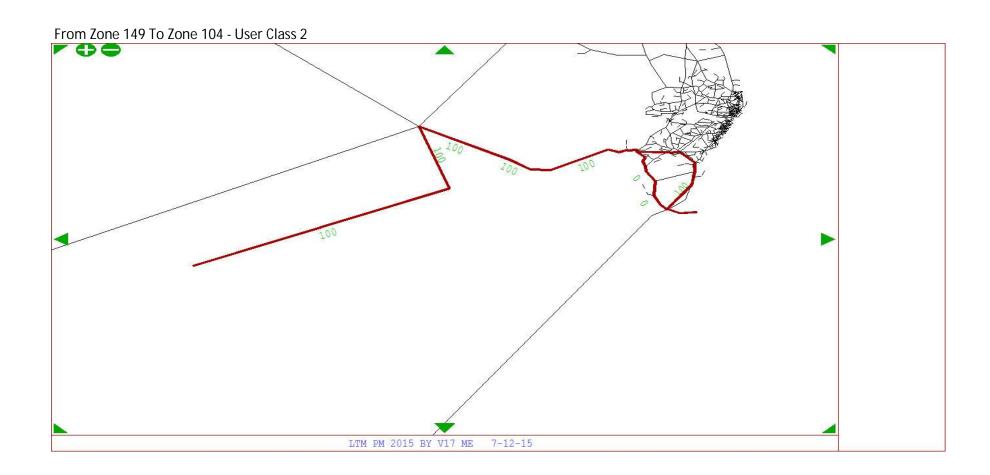
From Zone 149 To Zone 101 - User Class 2

From Zone 149 To Zone 101 - User Class 3

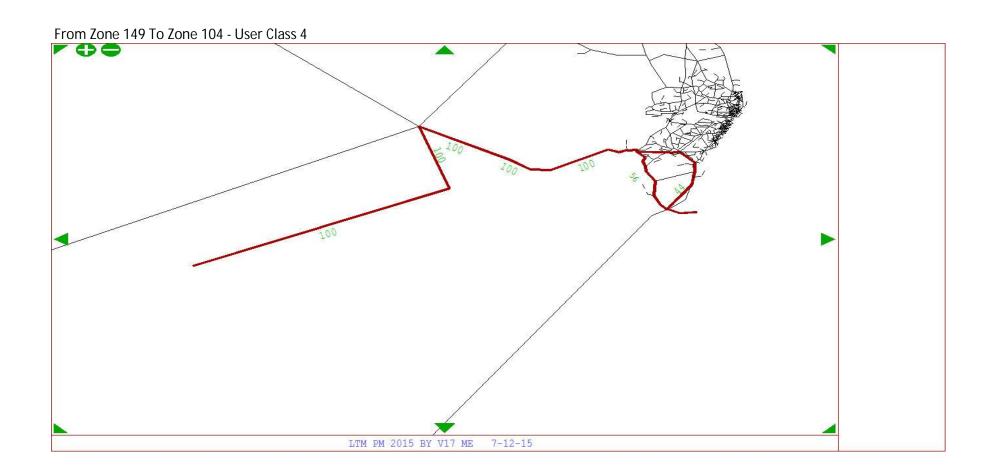
From Zone 149 To Zone 101 - User Class 4

From Zone 149 To Zone 101 - User Class 5



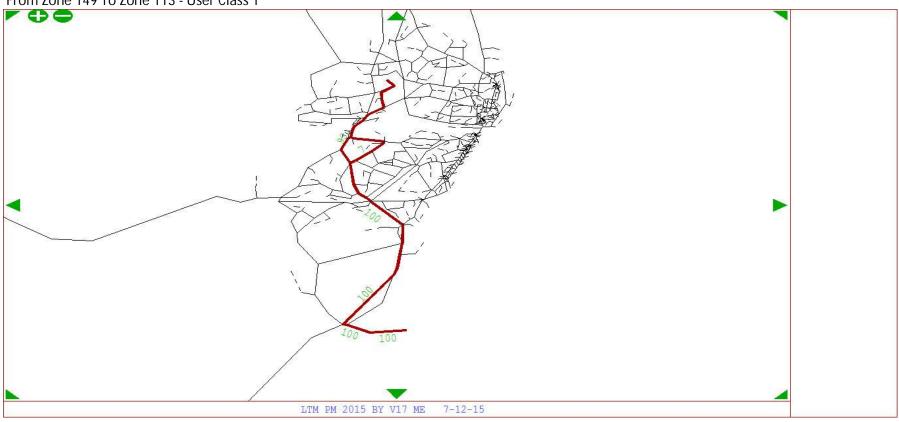


From Zone 149 To Zone 104 - User Class 3 LTM PM 2015 BY V17 ME

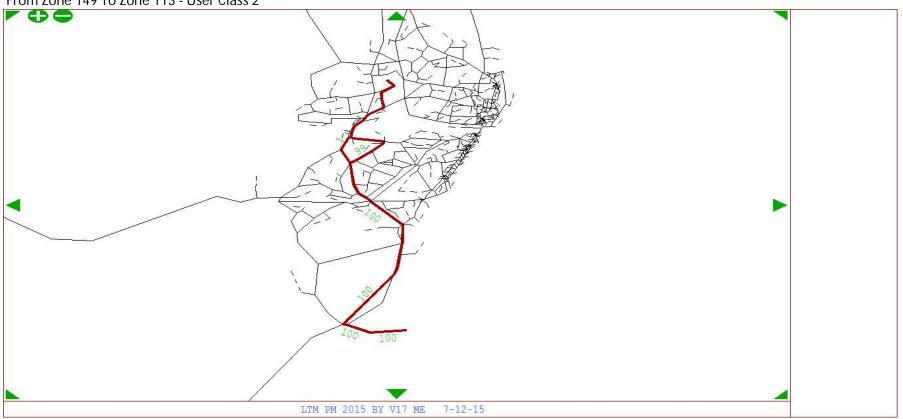


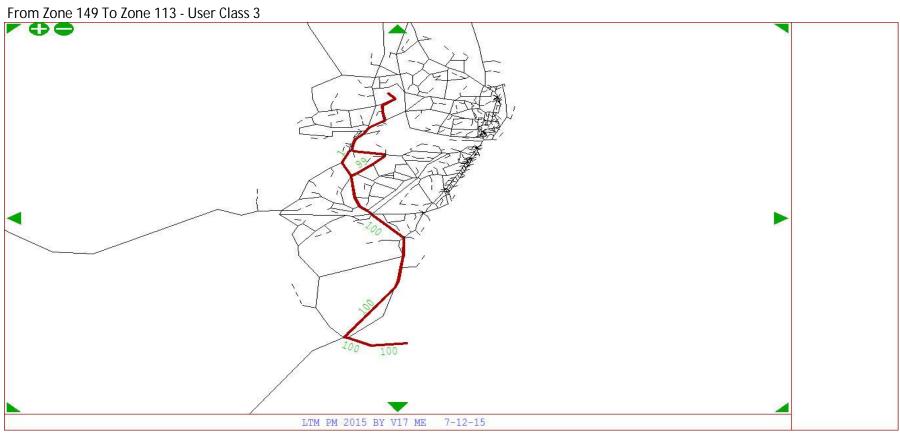
From Zone 149 To Zone 104 - User Class 5 LTM PM 2015 BY V17 ME

From Zone 149 To Zone 113 - User Class 1

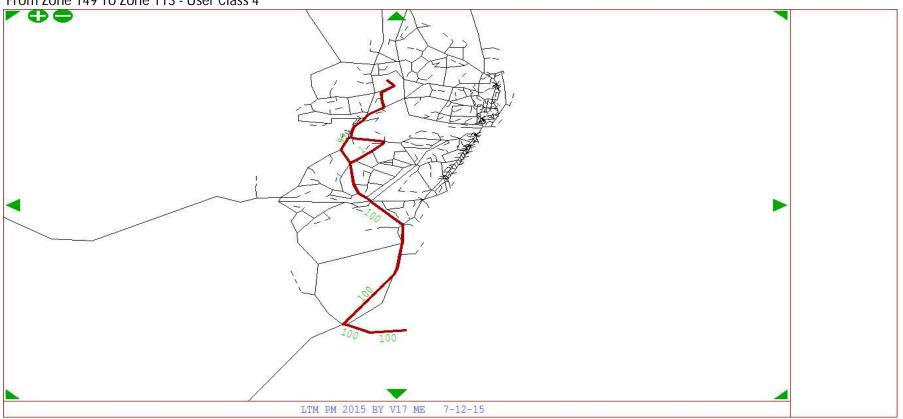


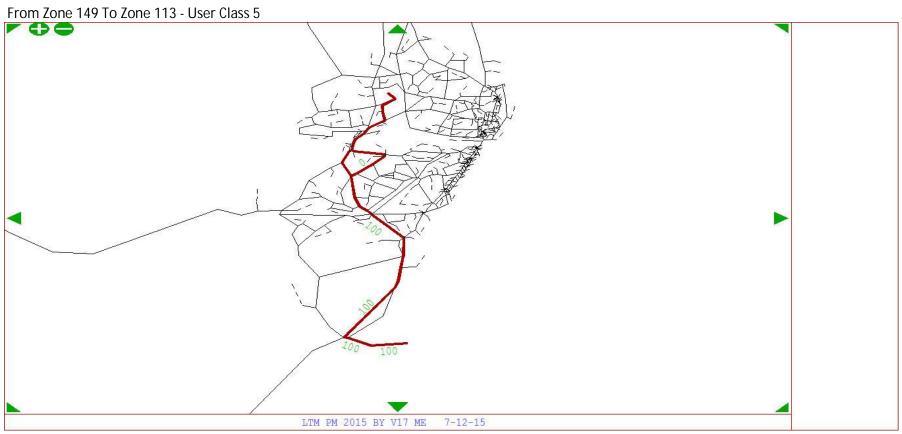
From Zone 149 To Zone 113 - User Class 2





From Zone 149 To Zone 113 - User Class 4





From Zone 149 To Zone 114 - User Class 1

From Zone 149 To Zone 114 - User Class 2 LTM PM 2015 BY V17 ME 7-12-15

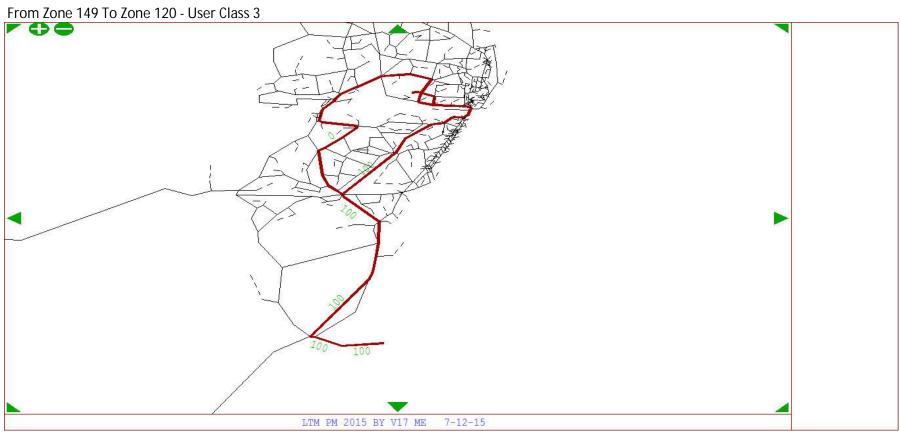
From Zone 149 To Zone 114 - User Class 3

From Zone 149 To Zone 114 - User Class 4 LTM PM 2015 BY V17 ME 7-12-15

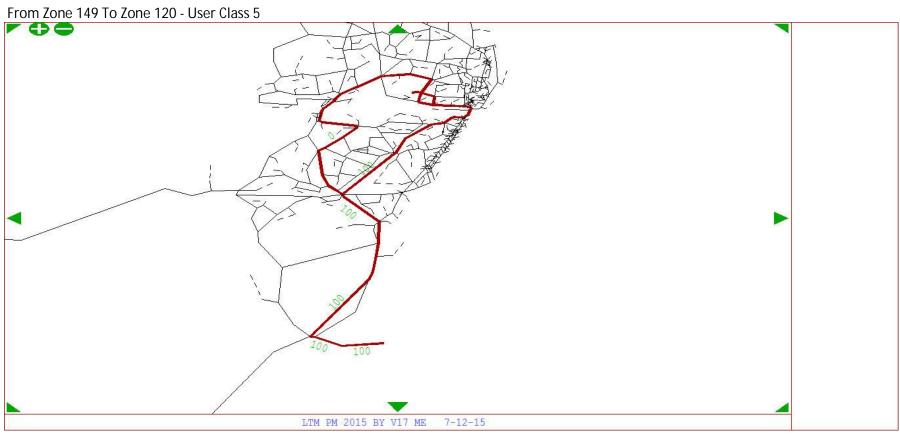
From Zone 149 To Zone 114 - User Class 5

From Zone 149 To Zone 120 - User Class 1

From Zone 149 To Zone 120 - User Class 2



From Zone 149 To Zone 120 - User Class 4

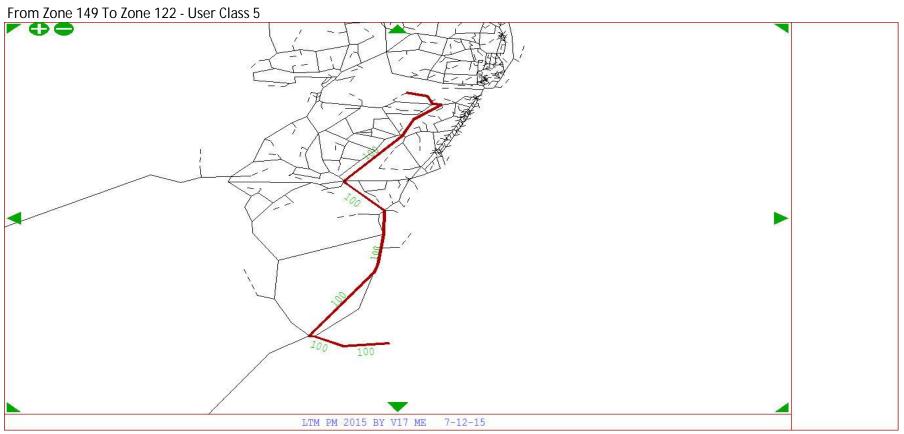


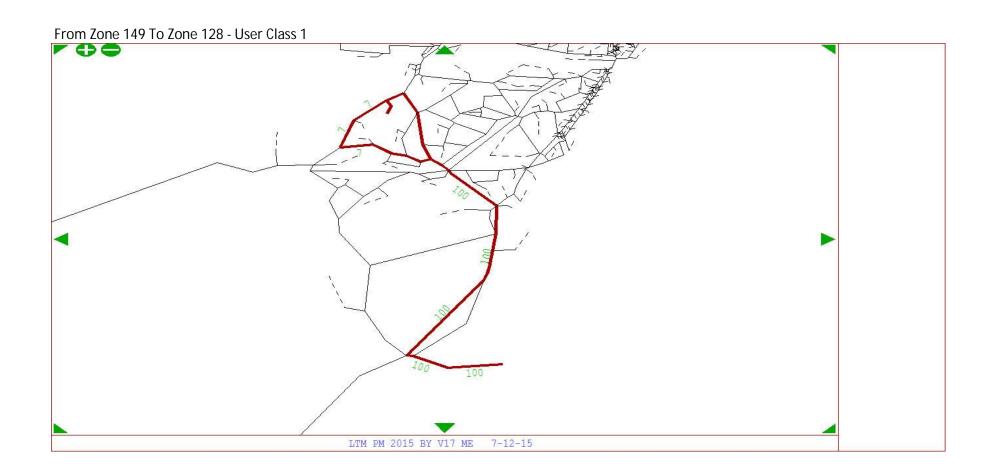
From Zone 149 To Zone 122 - User Class 1

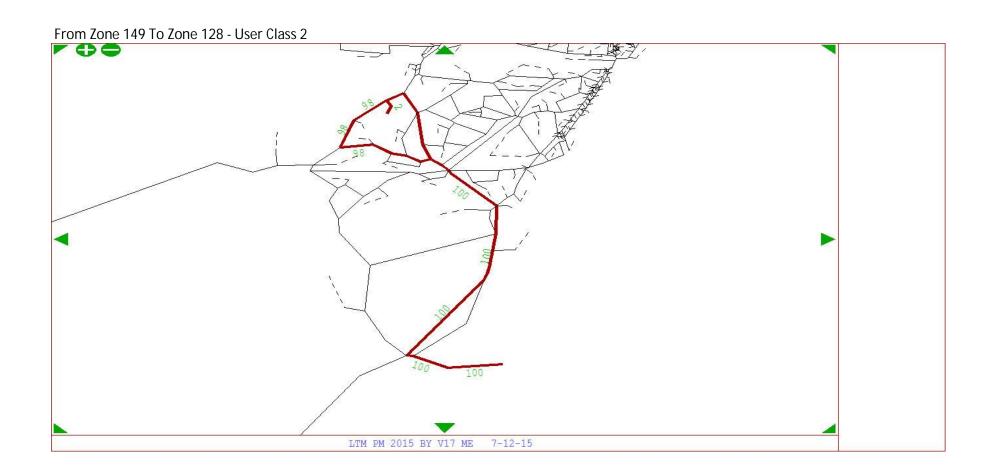
From Zone 149 To Zone 122 - User Class 2

From Zone 149 To Zone 122 - User Class 3

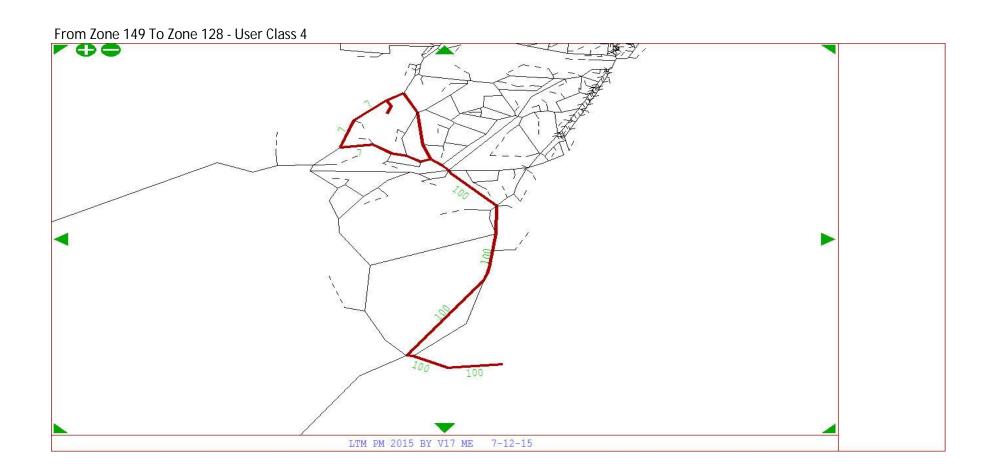
From Zone 149 To Zone 122 - User Class 4







From Zone 149 To Zone 128 - User Class 3 LTM PM 2015 BY V17 ME 7-12-15



From Zone 149 To Zone 128 - User Class 5 LTM PM 2015 BY V17 ME 7-12-15

# Appendix D

**POST ME SCREENLINE PERFORMANCE** 

Index

ID	Name	Link ID	Status	Site Location	Direction	A-Node	B-Node	AM	Interp	PM
		55	Calibration	B1385 Corton Road	NB	9460	9480	Peak	eak	Peak
1	Screenline 1 - NB	57	Calibration	A12 Yarmouth Road	NB	10257	6250			
	1-140	59	Calibration	B1375 Parkhill B1074 Bluderston	NB	10001	8070			
		61	Calibration	Road	NB	10025	20026			
				TOTAL		Cali		Yes	Yes	Yes
	Screenline	56	Calibration	B1385 Corton Road	SB	9480	9460			
2	1 - SB	58	Calibration	A12 Yarmouth Road	SB	6250	10257			
		60	Calibration	B1375 Parkhill B1074 Bluderston	SB	8070	10001			
		62	Calibration	Road	SB	20026	10025			
				TOTAL		Cali		Yes	Yes	Yes
	Screenline	49	Calibration	B1375 Gorleston Road	NB	8030	8040			
3	2 - NB	51	Calibration	A1117 Millennium Way	NB	7070	7080			
			•	TOTAL		Cali	oration	Yes	Yes	Yes
		50	Calibration	B1375 Gorleston Road	SB	8040	8030			
4	Screenline 2 - SB	52	Calibration	A1117 Millennium Way	SB	7080	7070			
				·						
				TOTAL			oration	Yes	Yes	Yes
5	Screenline	41	Calibration	Peto Way A1117 Normanston	NB	10190	7060			
3	3 - NB	43	Calibration	Drive	NEB	7050	7060			
				TOTAL		Cali		Yes	Yes	Yes
	Screenline	42	Calibration	Peto Way	SB	7060	10190			
6	3 - SB	44	Calibration	A1117 Normanston Drive	SWB	7060	7050			
				TOTAL		Cali	oration	Yes	Yes	Yes
		29	Calibration	Katwijk Way	NB	6040	10136			
7	Screenline 4 - NB	31	Calibration	A12 Battery Green	NB	6160	6150			
				Road TOTAL			oration	Yes	Yes	
			0.11		0.0			Tes	res	Yes
8	Screenline	30	Calibration	Katwijk Way A12 Battery Green	SB	10136	6040			
	4 - SB	32	Calibration	Road	SB	6150	6160			
				TOTAL		Cali		Yes	Yes	Yes
9	Screenline 5 - FR	22	Calibration	Kirkley Run	SEB	5270	10103			
	5 - EB	23	Calibration	A146 Waveney Drive	EB	10088	4010 oration	Yes	Yes	Yes
	Screenline	21	Calibration	Kirkley Run	NWB	10103	5270	res	res	res
10	5 - WB	21	Calibration	A146 Waveney Drive	WB	4010	10088			
				TOTAL		Cali	oration	Yes	Yes	Yes
		37	Calibration	Denmark Road	EB	7200	10139			
	Screenline	45	Calibration	A1144 Normanston	EB	9240	9130			
11	6 - EB	47	Calibration	Drive Oulton Road	EB	9270	10010			
		54	Calibration	A12 Yarmouth Road	SEB	10248	10242			
				TOTAL		Cali		Yes	Yes	Yes
		38	Calibration	Denmark Road	WB	10139	7200			
12	Screenline	46	Calibration	A1144 Normanston Drive	WB	9130	9240			
	6 - WB	48	Calibration	Oulton Road	WB	10010	9270			
		53	Calibration	A12 Yarmouth Road	NWB	10242	10248		ļ	
				TOTAL		Cali 9600	oration	Yes	Yes	Yes
	Screenline 7 - EB	5 7	Calibration Calibration				5010 4513			
			Janoranon	TOTAL	4514 Cali	oration	Yes	Yes	Yes	
	Screenline	6	Calibration	5010	9600					
	7 - WB	8	Calibration	Gisleham Road A146 Beccles Road	SB WB	4513	4514			
				TOTAL		Cali		Yes	Yes	Yes

		Flow < 5%	Calib	ration	Vali	dation
Screen	lines	All	14	88%	1	25%
Calibration	16	Car	14	88%	2	50%
Validation		LGV	13	81%	0	0%
						0.000

GEH < 4	Calib	ration	Vali	dation
All	16	100%	4	100%
Car		100%		75%
LGV		94%		50%
HGV		100%		100%

				AM Peak			Peak									
	,	All			С	ar			LC	3V			Н	GV		
Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	
96 567	97 566	1% 0%	0.089 0.047	81 456	82 456	-17% -24%	0.111 0.012	14 85	14 84	-1% -1%	0.033 0.082	1 27	1 26	0% -2%	0.000 0.122	
461	434	-6%	1.284	384	378	-24%	0.012	64	43	-33%	2.871	13	13	-1%	0.122	
179	180	0%	0.047	108	108	-66%	0.048	64	64	0%	0.031	8	8	-2%	0.044	
1304	1277	-2%	0.746	1028	1024	0%	0.133	227	205	10%	1.472	49	48	2%	0.132	
102 567	101 647	-1% 14%	0.062 3.252	81 411	80 490	-27% -19%	0.056 3.728	20 132	20 133	1% 1%	0.056 0.120	1 24	1 24	-27% -2%	0.344 0.076	
251	269	7%	1.106	178	196	-31%	1.304	65	65	1%	0.041	8	8	-4%	0.117	
113	122	8%	0.854	14	23	-665%	2.224	94	94	0%	0.000	5	5	-5%	0.110	
1032	1139	10%	3.235	683	789	16%	3.906	310	312	-1%	0.111	39	38	3%	0.214	
584	582	0%	0.065	455	453	-29%	0.101	109	109	0%	0.000	19	20	3%	0.129	
376	378	1%	0.124	296	298	-26%	0.093	60	60	1%	0.052	20	20	2%	0.090	
959	960	0%	0.027	752	751	0%	0.020	169	169	0%	0.031	39	40	-2%	0.155	
484	482	0%	0.078	377	375	-29%	0.125	91	91	0%	0.030	16	16	3%	0.108	
450	455	1%	0.254	375	379	-19%	0.206	59	60	2%	0.156	16	16	1%	0.050	
933	937	0%	0.121	752	754	0%	0.057	150	151	-1%	0.121	31	32	-2%	0.112	
396 687	386 699	-2% 2%	0.483 0.471	272 334	261 343	-49% -103%	0.694 0.467	116 327	116 329	0% 1%	0.000 0.110	7 25	9 27	25% 7%	0.624 0.352	
1082	1085	0%	0.086	607	604	0%	0.111	443	445	0%	0.095	32	36	-11%	0.612	
317	286	-10%	1.792	150	150	-111%	0.111	153	125	-18%	2.375	14	11	-11%	0.819	
506	509	1%	0.115	263	265	-92%	0.148	221	221	0%	0.013	23	23	2%	0.084	
824	795	-3%	1.002	413	415	1%	0.107	374	346	8%	1.486	36	34	7%	0.419	
411	364	-11%	2.388	261	231	-69%	1.902	122	107	-12%	1.387	28	26	-8%	0.448	
675	677	0%	0.077	289	290	-133%	0.042	357	357	0%	0.000	29	30	4%	0.237	
1086	1041	-4%	1.380	550	521	-5%	1.258	479	464	3%	0.683	57	56	2%	0.139	
134	123	-8%	0.970	87	87	-54%	0.054	34	34	0%	0.029	13	2	-85%	4.093	
571	570	0%	0.031	337	337	-69%	0.000	205	204	0%	0.035	29	29	-1%	0.046	
705 94	693 94	-2% 0%	0.444	424 67	424 67	0% -40%	0.024	239	238	0% -1%	0.043	43	31	27%	1.910 0.000	
94 347	94 344	-1%	0.017	212	211	-40% -64%	0.041	23 122	120	-1% -1%	0.035	13	4 13	-3%	0.000	
440	438	-1%	0.114	278	278	0%	0.013	145	143	1%	0.144	17	17	3%	0.107	
162 151	159 139	-2% -8%	0.263 0.978	110 68	110 67	-47% -123%	0.032 0.149	48 72	45 72	-7% 0%	0.464 0.013	4 10	4 0	4% -100%	0.084 4.570	
313	298	-5%	0.864	179	177	-1%	0.117	120	117	3%	0.301	14	4	72%	3.400	
215	214	0%	0.038	138	138	-55%	0.000	68	68	0%	0.027	8	8	-4%	0.117	
408	413	1%	0.272	225	229	-79%	0.249	167	169	1%	0.135	15	15	0%	0.000	
476 651	377 595	-21% -9%	4.789 2.248	263 401	263 401	-81% -62%	0.007 0.017	201 223	103 167	-49% -25%	7.919 4.040	12 27	11 27	-10% 0%	0.359 0.000	
1749	1599	-9%	3.668	1027	1031	0%	0.124	659	507	23%	6.313	63	61	2%	0.198	
304	342	13%	2.133	202	227	-38%	1.715	90	103	14%	1.300	12	12	4%	0.130	
190	190	0%	0.018	124	124	-53%	0.022	54	54	0%	0.034	12	12	2%	0.073	
246 460	246 460	0% 0%	0.028 0.005	149 298	149 298	-65% -54%	0.009 0.013	90 139	90 139	0% 0%	0.023 0.000	8 23	7 23	- <b>7%</b> 1%	0.206 0.070	
1200	1238	3%	1.096	773	798	3%	0.893	373	386	-3%	0.654	54	54	-1%	0.064	
21 639	5 639	- <b>76%</b> 0%	4.360 0.000	6 267	3 267	-307% -139%	1.308 0.000	14 312	1 312	-93% 0%	4.663 0.000	1 60	1 60	-21% 0%	0.250 0.000	
660	644	-2%	0.611	273	270	-1%	0.166	326	313	4%	0.705	61	61	0%	0.034	
17 670	18 670	3% 0%	0.127 0.000	7 185	6 185	-159% -262%	0.467 0.000	9 440	9 440	-4% 0%	0.110 0.000	1 45	3 45	221% 0%	1.474 0.000	
687	688	0%	0.020	192	191	-1%	0.087	440	449	0%	0.016	46	48	-4%	0.302	
									1				1			

Index

ID	Namo	Link ID	Statue	Sito Location	Direction	A-Nodo	P Nodo	AM	Interp	PM
	Screenline	13	Calibration	London Road South	NEB	9606	1040			
15	8 - NB	15	Calibration	A12 Tom Crisp Way	NEB	3000	10015			
	0 - ND	17	Calibration	A1117 Elm Tree Road	NB	3030	3040			
				TOTAL		Calil		Yes	Yes	Yes
	Screenline	14	Calibration	London Road South	SWB	1040	9606			
16	8 - SB	16	Calibration	A12 Tom Crisp Way	SWB	10015	3000			
	8 - SB	18	Calibration	A1117 Elm Tree Road	SB	3040	3030			
				TOTAL		Calil		Yes	Yes	Yes
19	Screenline	81	Validation	Saltwater Way	NB	2050	2060			
19	9 - NB	79	Validation	A12 Pier Terrace	NB	1260	10023			
				TOTAL		Vali	dation	Yes	Yes	Yes
20	Screenline	82	Validation	Saltwater Way	SB	2060	2050			
20	9 - SB	80	Validation	A12 Pier Terrace	SB	10023	1260			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	9	Validation	A1145 Castleton	EB	5110	5060			
21	10 - NB	11	Validation	A12 London Road	NB	5390	1000			
	IU - ND	19	Validation	A146 Beccles Road	NEB	10111	10109			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	10	Validation	A1145 Castleton	WB	5060	5110			
22	10 - SB	12	Validation	A12 London Road	SB	1000	5390			
	10 - SB	20	Validation	A146 Beccles Road	SWB	10109	10111			
				TOTAL		Vali	dation	Yes	Yes	Yes

		Flow < 5%	Calib	oration	Valid	dation
Screen		All	14	88%	1	25%
Calibration	16	Car	14	88%	2	50%
Validation		LGV	13	81%	0	0%
		HGV	12	75%	1	25%

GEH < 4	Calib	ration	Vali	dation
All		100%		100%
Car		100%		75%
LGV		94%		50%
HGV	16	100%	4	100%

							AM	Peak							
		All			C	ar			LC	SV .			H	3V	
Observed 452	Modelled 453	Difference 0%	0.035	Observed 247	Modelled 247	Difference -83%	0,008	Observed 188	Modelled 188	Difference 0%	0.036	Observed 18	Modelled 18	Difference 2%	0.089
823 310	819 309	0% 0%	0.143 0.043	623 167	619 166	-33% -86%	0.147 0.039	172 125	172 125	0% 0%	0.000 0.011	28 18	28 18	-2% -2%	0.084 0.088
1585	1581	0%	0.103	1036	1032	0%	0.133	484	485	0%	0.028	64	64	1%	0.055
356 381 359	357 381 359	0% 0% 0%	0.033 0.011 0.013	183 247 209	183 247 209	-95% -54% -72%	0.009 0.021 0.000	156 111 134	156 111 134	0% 0% 0%	0.040 0.021 0.022	18 23 16	18 23 16	1% -1% 0%	0.059 0.069 0.000
1096	1097	0%	0.033	639	639	0%	0.008	400	401	0%	0.049	57	57	0%	0.011
944 1531	973 1395	3% -9%	0.937 3.556	656 656	545 839	-61% -105%	4.520 6.688	242 810	383 500	58% -38%	7.974 12.103	46 65	45 56	-3% -14%	0.178 1.173
2475	2368	-4%	2.174	1312	1384	5%	1.964	1052	883	16%	5.426	111	101	9%	1.003
904 898	902 768	0% -14%	0.067 4.504	506 530	518 473	-76% -80%	0.532 2.555	367 322	344 256	-6% -20%	1.230 3.869	31 46	40 39	30% -15%	1.539 1.077
1802	1670	-7%	3.168	1036	991	-4%	1.420	689	600	13%	3.503	77	79	-3%	0.242
441 719 479	385 742 391	-13% 3% -18%	2.745 0.856 4.225	260 371 256	223 471 162	-84% -67% -124%	2.360 4.874 6.510	155 307 198	128 247 204	-17% -20% 3%	2.243 3.629 0.459	26 40 26	34 24 25	29% -41% -2%	1.374 2.895 0.100
1639	1518	-7%	3.040	887	856	-3%	1.043	660	579	12%	3.239	92	83	10%	1.001
343 595 435	337 654 302	-2% 10% -31%	0.337 2.379 6.928	173 324 288	122 403 94	-128% -59% -119%	4.233 4.159 14.024	140 229 127	187 229 190	33% 0% 50%	3.648 0.028 5.026	29 41 21	28 22 18	-5% -47% -12%	0.270 3.450 0.570
1373	1293	-6%	2.186	785	619	-21%	6.262	497	606	-22%	4.663	91	68	26%	2.618

					_			AM	Interp	PM
ID	Name	Link ID	Status	Site Location	Direction	A-Node	B-Node	Peak	eak	PM Peak
1	Screenline	55 57	Calibration Calibration	B1385 Corton Road A12 Yarmouth Road	NB NB	9460 10257	9480 6250			
•	1 - NB	59	Calibration	B1375 Parkhill	NB	10001	8070			
		61	Calibration	B1074 Bluderston Road	NB	10025	20026			
				TOTAL		Cali	bration	Yes	Yes	Yes
		56	Calibration	B1385 Corton Road	SB	9480	9460	103	163	163
2	Screenline	58	Calibration	A12 Yarmouth Road	SB	6250	10257			
	1 - SB	60	Calibration	B1375 Parkhill	SB	8070	10001			
		62	Calibration	B1074 Bluderston Road	SB	20026	10025			
				TOTAL		Cali	bration	Yes	Yes	Yes
	Screenline	49	Calibration	B1375 Gorleston Road	NB	8030	8040			
3	2 - NB	51	Calibration	A1117 Millennium Way	NB	7070	7080			
				TOTAL		Cali	bration	Yes	Yes	Yes
		50	Calibration	B1375 Gorleston Road	SB	8040	8030	165	165	165
4	Screenline 2 - SB	52	Calibration	A1117 Millennium Way	SB	7080	7070			
				TOTAL			bration	Yes	Yes	Yes
5	Screenline	41	Calibration	Peto Way A1117 Normanston	NB	10190	7060			
,	3 - NB	43	Calibration	Drive	NEB	7050	7060			
				TOTAL		Calil		Yes	Yes	Yes
	Screenline	42	Calibration	Peto Way	SB	7060	10190			
6	3 - SB	44	Calibration	A1117 Normanston Drive	SWB	7060	7050			
				TOTAL		Calil	bration	Yes	Yes	Yes
	Screenline	29	Calibration	Katwijk Way	NB	6040	10136			
7	4 - NB	31	Calibration	A12 Battery Green	NB	6160	6150			
				Road TOTAL		Cali	bration	Yes	Yes	Yes
		30	Calibration	Katwijk Way	SB	10136	6040	100	100	100
8	Screenline 4 - SB	32	Calibration	A12 Battery Green	SB	6150	6160			
				Road						
				TOTAL			bration	Yes	Yes	Yes
9	Screenline 5 - EB	22	Calibration Calibration	Kirkley Run A146 Waveney Drive	SEB EB	5270 10088	10103 4010			
				TOTAL		Calil	bration	Yes	Yes	Yes
10	Screenline	21	Calibration	Kirkley Run	NWB	10103	5270			
10	5 - WB	24	Calibration	A146 Waveney Drive	WB	4010	10088			
				TOTAL		Calil	bration	Yes	Yes	Yes
		37	Calibration	Denmark Road A1144 Normanston	EB	7200	10139			
11	Screenline 6 - EB	45	Calibration	Drive	EB	9240	9130			
	0-58	47 54	Calibration Calibration	Oulton Road A12 Yarmouth Road	EB SEB	9270 10248	10010 10242			
		54	Calibration	TOTAL	SEB		bration	Yes	Yes	Yes
		38	Calibration	Denmark Road	WB	10139	7200	.03	. 63	. 63
12	Screenline	46	Calibration	A1144 Normanston	WB	9130	9240			
12	6 - WB	48	Calibration	Drive Oulton Road	WB	10010	9270			
		53	Calibration	A12 Yarmouth Road	NWB	10242	10248		ļ	
				TOTAL			bration	Yes	Yes	Yes
	Screenline 7 - EB	5 7	Calibration Calibration	Gisleham Road A146 Beccles Road	NB EB	9600 4514	5010 4513			
	, - 25		Cambration	TOTAL	LU		bration	Yes	Yes	Yes
	Screenline	6	Calibration	Gisleham Road	SB	5010	9600			
	7 - WB	8	Calibration	A146 Beccles Road	WB	4513	4514		ļ	
				TOTAL		Cali		Yes	Yes	Yes
	Screenline	13	Calibration	London Road South	NEB	9606	1040			
15	8 - NB	15 17	Calibration Calibration	A12 Tom Crisp Way A1117 Elm Tree Road	NEB NB	3000 3030	10015 3040			
	1		Galloration	Liiii iiee Koau	IND	3030	3070			

Flow < 5%	Calib	oration	Valid	dation
All	16	100%	1	25%
Car		75%		
LGV		88%		
HGV		75%		

GEH < 4	Calib	oration	Valid	dation
		100%	3	
		100%	3	
		100%	4	100%
		100%	4	100%

											HGV	12	75%	0	0% Inter	peak	HGV	16	100%	4	100%				
											,	All .			С	ar	inter	p our	L	GV			Н	gV .	
ame	Link ID	Status	Site Location	Direction	A-Node		AM Peak	Interp eak	PM Peak	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH
enline	55 57	Calibration Calibration	B1385 Corton Road A12 Yarmouth Road	NB NB	9460 10257	9480 6250				88 495	87 489	-1% -1%	0.074 0.276	73 389	73 389	-20% -27%	0.019 0.018	13 80	12 74	-4% -7%	0.161 0.639	2 26	2 26	2% -1%	0.030 0.031
- NB	59	Calibration	B1375 Parkhill B1074 Bluderston	NB	10001	8070				263	234	-11%	1.869	210	181	-39%	2.101	42	42	0%	0.001	11	11	-1%	0.023
	61	Calibration	Road	NB	10025	20026				116	116	0%	0.031	73	73	-59%	0.015	39	39	1%	0.037	4	4	-10%	0.213
			TOTAL			bration	Yes	Yes	Yes	963	926	-4%	1.192	746	716	-4%	1.111	173	167	3%	0.456	44	43	1%	0.096
enline - SB	56 58	Calibration Calibration	B1385 Corton Road A12 Yarmouth Road	SB SB	9480 6250	9460 10257				99 542	99 502	0% -7%	0.038 1.750	80 370	80 331	-23% -57%	0.012 2.077	17 144	17 143	2% -1%	0.086 0.079	2 28	2 28	7% -1%	0.090 0.030
-	60 62	Calibration Calibration	B1375 Parkhill B1074 Bluderston	SB SB	8070	10001				193 101	186 107	-4% 6%	0.532	140 11	133 18	-43% -727%	0.604 1.711	46 82	46 82	0% 0%	0.008	7 8	7	-3% -8%	0.079
	02	Cambration	Road	35	20026	10025					<b></b>	<b>+</b>	0.570			<del> </del>	<b></b>				0.016		ļ	<b> </b>	0.224
	49	Calibration	TOTAL B1375 Gorleston Road	NB	8030	bration 8040	Yes	Yes	Yes	935	894 415	-4% -7%	1.360	601 336	562 306	-7% -41%	1.637	289 92	288 92	0%	0.046	45 18	44 17	2% -3%	0.128
enline - NB	51	Calibration	A1117 Millennium Way	NB	7070	7080				438	472	8%	1.575	348	378	-17%	1.564	75	81	8%	0.656	15	13	-13%	0.528
-			TOTAL	1	Cali	bration	Yes	Yes	Yes	884	887	0%	0.114	684	684	0%	0.010	167	173	-3%	0.436	33	30	8%	0.459
enline	50	Calibration	B1375 Gorleston Road	SB	8040	8030				473	462	-2%	0.489	367	357	-31%	0.523	89	89	0%	0.029	16	16	-2%	0.090
- SB	52	Calibration	A1117 Millennium Way	SB	7080	7070				392	445	14%	2.597	326	356	-11%	1.615	51	74	46%	2.942	15	15	0%	0.017
			TOTAL		Cali	bration	Yes	Yes	Yes	864	907	5%	1.430	693	713	3%	0.750	140	163	-16%	1.865	31	31	1%	0.053
enline	41	Calibration	Peto Way A1117 Normanston	NB	10190					445	449	1%	0.178	303	306	-46%	0.182	133	133	0%	0.031	10	10	2%	0.074
- NB	43	Calibration	Drive	NEB	7050	7060				641	678	6%	1.458	323	358	-88%	1.908	297	299	1%	0.089	20	21	3%	0.154
	42	Calibration	TOTAL Peto Way	SB	7060	bration 10190	Yes	Yes	Yes	1086 550	1127 553	4% 1%	1.238 0.146	626 300	664 305	6% -81%	1.511 0.274	430 237	432 236	0%	0.091	30 12	31 12	-3% -3%	0.169
enline - - SB	44	Calibration	A1117 Normanston	SWB	7060	7050				650	645	-1%	0.140	356	363	-81%	0.274	270	258	-4%	0.724	24	24	1%	0.039
-			Drive TOTAL		Cali	bration	Yes	Yes	Yes	1200	1198	0%	0.047	657	668	2%	0.441	507	494	3%	0.570	36	36	1%	0.035
enline	29	Calibration	Katwijk Way	NB	6040	10136	100	100	100	323	297	-8%	1.465	193	181	-74%	0.849	106	101	-5%	0.525	24	15	-37%	2.005
- NB	31	Calibration	A12 Battery Green Road	NB	6160	6150				465	467	0%	0.092	202	204	-129%	0.118	238	238	0%	0.019	25	25	0%	0.002
			TOTAL		Cali	bration	Yes	Yes	Yes	788	764	-3%	0.854	395	385	-3%	0.503	344	339	1%	0.273	49	40	18%	1.324
enline	30	Calibration	Katwijk Way A12 Battery Green	SB	10136					204	198	-3%	0.454	138	147	-42%	0.732	49	49	0%	0.012	17	2	-88%	4.920
- SB	32	Calibration	Road	SB	6150	6160				610	583	-4%	1.098	355	318	-82%	2.024	229	239	5%	0.682	26	26	0%	0.019
	00	0.5	TOTAL	055		bration	Yes	Yes	Yes	814	781	-4%	1.177	493	465	-6%	1.297	277	288	-4%	0.625	43	28	35%	2.573
enline - EB	22 23	Calibration	Kirkley Run A146 Waveney Drive	SEB EB	5270 10088	10103 4010				109 258	106 262	-3% 2%	0.329 0.264	75 151	73 156	-49% -67%	0.211 0.367	31 97	30 97	-3% 0%	0.186 0.001	4 9	3 9	-16% -3%	0.320 0.095
			TOTAL			bration	Yes	Yes	Yes	367	368	0%	0.044	226	229	1%	0.182	128	127	1%	0.092	13	12	7%	0.246
enline WB	21 24	Calibration Calibration	Kirkley Run A146 Waveney Drive	NWB WB	10103 4010	5270 10088				132 266	136 264	3% -1%	0.315 0.111	90 134	93 135	-44% -98%	0.281 0.124	38 122	39 119	1% -3%	0.087 0.296	4 10	4 10	12% 0%	0.216 0.000
			TOTAL		Cali	bration	Yes	Yes	Yes	398	400	0%	0.092	224	228	2%	0.275	161	158	2%	0.215	14	14	-3%	0.113
	37	Calibration	Denmark Road A1144 Normanston	EB	7200	10139				237	244	3%	0.456	153	158	-52%	0.420	78	79	2%	0.165	7	7	6%	0.142
enline - EB	45 47	Calibration	Drive Oulton Road	EB EB	9240 9270	9130 10010				281 325	298 266	6% -18%	0.975 3.421	160 182	176 171	-66% -85%	1.260 0.812	110 134	110 86	0% -36%	0.005 4.563	12	12 9	2% -2%	0.064
ļ	54	Calibration	A12 Yarmouth Road	SEB	10248			<b></b>		510	481	-6%	1.309	299	270	-80%	1.717	185	185	0%	0.035	26	26	1%	0.062
			TOTAL			bration	Yes	Yes	Yes	1353	1289	-5%	1.768	793	775	-2%	0.650	507	460	9%	2.129	53	54	-1%	0.102
enline	38 46	Calibration Calibration	Denmark Road A1144 Normanston	WB WB	10139 9130	7200 9240				338 275	345 275	2% 0%	0.367	228 180	232 177	-47% -54%	0.253 0.252	99 83	102 87	3% 4%	0.278 0.390	11 11	11 11	1% -3%	0.047 0.087
· WB	48	Calibration	Drive Oulton Road	WB	10010	9270				270	253	-6%	1.058	164	161	-67%	0.232	99	84	-15%	1.557	8	8	6%	0.164
	53	Calibration	A12 Yarmouth Road	NWB	10242	10248				508	508	0%	0.002	318	318	-60%	0.017	168	168	0%	0.004	22	22	-1%	0.039
enline	5	Calibration	TOTAL Gisleham Road	NB	9600		Yes	Yes	Yes	1391	1381	-1% -49%	0.278 2.521	890	888	0% -186%	0.064	450 11	441 3	2% -74%	0.406 3.118	52	52	0% 2%	0.019
- EB	7	Calibration	A146 Beccles Road	EB	4514	4513		<b></b>		589	617	5%	1.147	227	254	-148%	1.752	316	316	0%	0.028	47	47	1%	0.073
		0.5	TOTAL		Cali		Yes	Yes	Yes	609	627	3%	0.742	234	260	11%	1.640	327	319	2%	0.437	47	48	-1%	0.075
enline · WB	6 8	Calibration Calibration	Gisleham Road A146 Beccles Road	SB WB	5010 4513	9600 4514				22 588	24 588	7% 0%	0.318 0.014	10 161	10 162	-127% -264%	0.063 0.066	12 378	12 378	3% 0%	0.109 0.009	1 48	2 48	92% -1%	0.777 0.048
			TOTAL		Cali	bration	Yes	Yes	Yes	610	612	0%	0.075	171	172	1%	0.079	390	390	0%	0.011	49	50	-1%	0.089
enline	13 15	Calibration Calibration	London Road South A12 Tom Crisp Way	NEB NEB	9606 3000	1040 10015				385 490	367 535	-5% 9%	0.937 2.010	207 353	198 391	-90% -28%	0.662 1.957	158 114	151 121	-5% 6%	0.589 0.609	19 22	18 23	-7% 5%	0.330 0.241
NB	17	Calibration	A1117 Elm Tree Road		3030	3040				382	389	2%	0.338	211	218	-78%	0.490	153	153	0%	0.038	18	18	0%	0.016

Inde:

ID	Name	Link ID	Ctatus	Sita Location	Direction	A Nodo	D Node	AM	Interp	PM
	Nama	1182		TOTAL	IIII		oration	Yes	Yes	Yes
	Screenline	14	Calibration	London Road South	SWB	1040	9606			
16	8 - SB	16	Calibration	A12 Tom Crisp Way	SWB	10015	3000			
	0-05	18	Calibration	A1117 Elm Tree Road	SB	3040	3030			
				TOTAL	Calit		Yes	Yes	Yes	
19	Screenline	81	Validation	Saltwater Way	NB	2050	2060			
19	9 - NB	79	Validation	A12 Pier Terrace	NB	1260	10023			
				TOTAL	Vali	dation	Yes	Yes	Yes	
20	Screenline	82	Validation	Saltwater Way	SB	2060	2050			
20	9 - SB	80	Validation	A12 Pier Terrace	SB	10023	1260			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	9	Validation	A1145 Castleton	EB	5110	5060			
21	10 - NB	11	Validation	A12 London Road	NB	5390	1000			
	10 - 140	19	Validation	A146 Beccles Road	NEB	10111	10109			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	10	Validation	A1145 Castleton	WB	5060	5110			
22	10 - SB	12 Validation A12 London Road		SB	1000	5390				
	10-36	20	Validation	SWB	10109	10111		L		
				TOTAL		Vali	dation	Yes	Yes	Yes

		Flow < 5%		Calibration			
Screen	lines	All	16	100%	1		
ration	16	Car	12		1		
		LGV	14	88%	2		
		HGV	49		0		

GEH < 4	Calib	ration	Validation				
All	16	100%	3	75%			
Car	16	100%	3				
LGV	16	100%	4	100%			
HGV	16	100%	4	100%			

	Interpeak														
		All			C	ar		LGV				HGV			
Observed	Modelled	Difference	O.F.H	Observed	Modelled	Difference	OEH	Observed	Modelled	Difforence	CEU	Observed	Modelled	Difference	OEU.
1257	1291	3%	0.951	772	807	5%	1.263	426	425	0%	0.057	59	59	1%	0.046
408 492 405	411 499 395	1% 2% -2%	0.147 0.332 0.481	203 326 235	205 325 235	-100% -51% -72%	0.167 0.076 0.028	184 141 153	185 150 143	0% 6% -6%	0.050 0.706 0.792	21 24 17	21 24 17	0% 1% 3%	0.017 0.045 0.108
1304	1305	0%	0.021	764	765	0%	0.021	478	478	0%	0.020	61	62	-1%	0.075
983 1041	957 955	-3% -8%	0.845 2.722	718 453	526 570	-64% -104%	7.686 5.177	228 532	391 346	72% -35%	9.284 8.883	38 56	40 39	5% -30%	0.329 2.459
2024	1912	-6%	2.532	1171	1096	-6%	2.216	760	737	3%	0.835	94	79	16%	1.601
931 1051	974 1090	5% 4%	1.410 1.182	575 612	577 687	-61% -60%	0.079 2.932	329 394	357 352	9% -11%	1.525 2.178	27 45	40 51	50% 13%	2.318 0.867
1982	2064	4%	1.827	1187	1264	6%	2.188	723	709	2%	0.517	72	91	-27%	2.150
306 642 417	369 615 301	20% -4% -28%	3.412 1.096 6.104	161 313 224	189 355 131	-73% -92% -127%	2.131 2.322 6.982	123 292 172	152 237 153	24% -19% -11%	2.514 3.355 1.519	23 38 20	28 23 17	22% -40% -16%	0.999 2.775 0.745
1365	1285	-6%	2.209	697	675	-3%	0.856	586	542	8%	1.872	82	68	17%	1.566
322 664 399	297 615 316	-8% -7% -21%	1.430 1.926 4.391	158 375 258	102 363 116	-139% -80% -110%	4.941 0.610 10.393	137 249 124	168 235 179	22% -6% 44%	2.469 0.922 4.425	26 40 16	27 17 21	3% -57% 28%	0.138 4.252 1.065
1385	1228	-11%	4.340	791	581	-27%	8.026	511	582	-14%	3.023	82	65	21%	2.017

Index

ID	Name	Link ID	Status	Site Location	Direction	A-Node	B-Node	AM Peak	Interp eak	PM Peak
1	Screenline	55	Calibration	B1385 Corton Road	NB	9460	9480			
1	1 - NB	57 59	Calibration Calibration	A12 Yarmouth Road B1375 Parkhill	NB NB	10257 10001	6250 8070			
		61	Calibration	B1074 Bluderston	NB	10025	20026			
				Road						
				TOTAL			bration	Yes	Yes	Yes
2	Screenline	56 58	Calibration Calibration	B1385 Corton Road A12 Yarmouth Road	SB SB	9480 6250	9460 10257			
-	1 - SB	60	Calibration	B1375 Parkhill	SB	8070	10001			
		62	Calibration	B1074 Bluderston Road	SB	20026	10025			
				TOTAL		Cali	bration	Yes	Yes	Yes
		49	Calibration	B1375 Gorleston Road	NB	8030	8040	163	163	163
3	Screenline 2 - NB	51	Calibration	A1117 Millennium Way	NB	7070	7080			
	2-ND	31	Cambration	· ·	IND				ļ	
				TOTAL				Yes	Yes	Yes
4	Screenline	50	Calibration	B1375 Gorleston Road	SB	8040	8030			
4	2 - SB	52	Calibration	A1117 Millennium Way	SB	7080	7070			
				TOTAL	Cali	bration	Yes	Yes	Yes	
	Screenline	41	Calibration	Peto Way	NB	10190	7060			
5	3 - NB	43	Calibration	A1117 Normanston	NEB	7050	7060			
				Drive TOTAL		Cett	bration	Yes	Yes	Yes
		42	Calibration	Peto Way	SB	7060	10190	res	res	res
6	Screenline 3 - SB	44	Calibration	A1117 Normanston	SWB	7060	7050			
	3-35	44	Calibration	Drive	SWB	7060	7050		ļ	
				TOTAL		Calil		Yes	Yes	Yes
_	Screenline	29	Calibration	Katwijk Way	NB	6040	10136			
7	4 - NB	31	Calibration	A12 Battery Green Road	NB	6160	6150			
				TOTAL		Cali	bration	Yes	Yes	Yes
	Screenline	30	Calibration	Katwijk Way	SB	10136	6040			
8	4 - SB	32	Calibration	A12 Battery Green Road	SB	6150	6160			
				TOTAL		Cali	bration	Yes	Yes	Yes
	Screenline	22	Calibration	Kirkley Run	SEB	5270	10103	100	100	100
9	5 - EB	23	Calibration	A146 Waveney Drive	EB	10088	4010			
				TOTAL		Cali		Yes	Yes	Yes
10	Screenline	21	Calibration	Kirkley Run	NWB	10103	5270			
10	5 - WB	24	Calibration	A146 Waveney Drive	WB	4010	10088		ļ	
	<u></u>			TOTAL			bration	Yes	Yes	Yes
		37	Calibration	Denmark Road	EB	7200	10139			
11	Screenline 6 - FR	45	Calibration	A1144 Normanston Drive	EB	9240	9130			
	P-FR	47	Calibration	Oulton Road	EB	9270	10010			
		54	Calibration	A12 Yarmouth Road	SEB	10248	10242	Yes	Yes	Yes
		20	Coffication		WD		bration	Yes	res	res
	Carac	38	Calibration	Denmark Road A1144 Normanston	WB	10139	7200			
12	Screenline 6 - WB	46	Calibration	Drive	WB	9130	9240			
		48 53	Calibration Calibration	Oulton Road A12 Yarmouth Road	WB NWB	10010 10242	9270 10248			
				TOTAL			bration	Yes	Yes	Yes
	Screenline	5	Calibration	Gisleham Road	NB	9600	5010			
	7 - EB	7	Calibration	A146 Beccles Road	EB	4514	4513		ļ	
				TOTAL		Cali		Yes	Yes	Yes
	Screenline	6	Calibration	Gisleham Road	SB	5010	9600			
	7 - WB	8	Calibration	A146 Beccles Road	WB	4513	4514		ļ	
				TOTAL		Cali	bration	Yes	Yes	Yes
15	Screenline 8 - NB	13 15	Calibration Calibration	London Road South A12 Tom Crisp Way	NEB NEB	9606 3000	1040 10015			

	Flow < 5%	Calit	oration	Validation		
es	All	14	88%		50%	
	Car		94%		25%	
	LGV		44%		75%	
	HGV		44%		0%	

GEH < 4	Calib	ration	Validation				
All		100%		50%			
Car		100%		50%			
LGV		94%		100%			
HGV		100%		100%			

							PM	Peak			10070		10070		
	А	JI			С	ar			LC	SV			H	GV	
Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH	Observed	Modelled	Difference	GEH
104 656	104 687	0% 5%	0.025 1.180	88 561	89 574	-17% -15%	0.066 0.564	14 76	14 100	-1% 32%	0.033 2.558	1 20	1 13	-20% -35%	0.236 1.692
315	304	-3%	0.597	257	247	-15%	0.564	51	51	0%	0.035	7	6	-35%	0.200
219	229	5%	0.677	144	154	-45%	0.809	70	70	0%	0.015	5	5	8%	0.171
1294	1324	2%	0.842	1050	1064	1%	0.436	212	235	-11%	1.573	32	25	22%	1.352
93	93	0%	0.013	77	77	-21%	0.014	16	16	2%	0.094	0	0	-100%	0.866
730 485	672 430	-8% -11%	2.180 2.571	530 375	479 375	-47% -29%	2.271 0.013	182 101	176 46	-4% -54%	0.480 6.415	17 9	17 9	-2% 3%	0.069 0.084
143	173	21%	2.428	21	51	-446%	5.101	115	115	0%	0.035	7	7	6%	0.144
1450	1368	-6%	2.187	1003	982	-2%	0.655	414	353	15%	3.136	33	33	0%	0.006
543	523	-4%	0.860	429	410	-31%	0.941	105	105	0%	0.042	8	8	-2%	0.050
545	569	4%	1.012	443	468	-17%	1.154	89	89	0%	0.000	13	12	-6%	0.213
1088	1092	0%	0.122	873	878	1%	0.180	194	194	0%	0.031	21	20	4%	0.197
702	655	-7%	1.804	570	561	-25%	0.384	119	81	-32%	3.800	13	13	1%	0.040
510	601	18%	3.850	448	473	-8%	1.189	55	120	117%	6.901	7	8	8%	0.225
1212	1256	4%	1.245	1018	1034	2%	0.511	174	201	-15%	1.943	20	21	-4%	0.169
423	401	-5%	1.078	295	294	-44%	0.044	120	100	-17%	1.896	8	7	-15%	0.453
608	598	-2%	0.399	297	297	-105%	0.023	298	289	-3%	0.537	12	12	-2%	0.057
1031	999 588	-3% -3%	0.994	592 335	591 320	0% -86%	0.047	418 264	389	7% -2%	1.447 0.394	20	19 10	7% 1%	0.326
609 648	641	-3%	0.848 0.291	335	320	-86% -78%	0.802 0.502	264	258 272	-2% 2%	0.394	10 12	8	1% -32%	0.040 1.208
1257	1229	-2%	0.798	705	681	-3%	0.915	530	530	0%	0.016	22	18	17%	0.825
307	282	-2%	1.476	186	180	-3%	0.915	101	93	-7%	0.016	21	9	-58%	3.167
457	467	2%	0.479	241	246	-88%	0.348	206	211	2%	0.762	10	10	1%	0.045
764	749	-2%	0.547	426	426	0%	0.003	307	304	1%	0.159	31	19	39%	2.433
225	221	-2%	0.268	165	212	-8%	3.410	46	8	-83%	7.292	14	1	-93%	4.747
911	881	-3%	1.006	581	550	-62%	1.293	309	308	0%	0.036	22	23	6%	0.264
1136	1102	-3%	1.020	746	762	2%	0.586	354	316	11%	2.100	36	24	33%	2.150
183 221	178 221	-3% 0%	0.372 0.000	132 140	131 142	-39% -56%	0.065 0.159	49 75	45 79	-9% 5%	0.619 0.430	2 6	2	0% -100%	0.000 3.367
404	399	-1%	0.250	272	273	0%	0.069	124	124	0%	0.042	8	2	74%	2.578
219 431	190	-13%	2.028 0.112	155	153 235	-43% -84%	0.141 0.160	62 189	35	-44% 0%	3.877 0.032	2 10	2 9	-11%	0.171
650	433 623	1% -4%	1.057	233	388	0%	0.035	251	189 224	11%	1.724	12	11	-6% 7%	0.182
261	252	-3%	0.554	182	180	-45%	0.112	77	69	-10%	0.879	3	3	4%	0.073
238	222	-7%	1.055	142	161	-54%	1.565	90	56	-38%	3.979	6	5	-20%	0.527
371	286	-23%	4.664	205	184	-91%	1.532	160	96	-40%	5.618	6	6	7%	0.156
601 1470	572 1332	-5% -9%	1.197 3.697	380 908	358 883	-64% -3%	1.132 0.848	206 532	199 420	-4% 21%	0.518 5.150	15 30	15 29	1% 2%	0.032 0.115
406	406	0%	0.012	290	304	-35%	0.805	107	95	-12%	1.230	8	7	-15%	0.453
323	292	-9%	1.740	211	200	-58%	0.785	102	86	-16%	1.675	9	6	-33%	1.095
353	355	1%	0.100	220	221	-60%	0.076	126	127	1%	0.089	7	7	-3%	0.094
702 1783	702 1755	-2%	0.009	472 1193	471 1196	-49% 0%	0.029	215 551	215 523	0% 5%	0.026 1.208	15 39	16 36	8% 8%	0.319
42	1755	-2%	2.594	1193	1196	-192%	1.019	26	15	-42%	2.417	39	0	-100%	1.033
896	924	3%	0.928	383	405	-128%	1.134	489	494	1%	0.248	25	25	0%	0.000
938	951	1%	0.414	398	417	5%	0.926	514	509	1%	0.240	26	25	2%	0.106
26 664	20 653	-24% -2%	1.342 0.429	12 193	12 182	-117% -250%	0.115 0.803	13 448	7 448	-47% 0%	1.933 0.024	1 24	1 23	7% -2%	0.068 0.104
690	673	-3%	0.669	205	194	-6%	0.807	461	455	1%	0.263	24	24	2%	0.088
520 502	504 559	-3% 11%	0.718 2.475	287 383	275 431	-86% -19%	0.686 2.371	218 111	213 120	-2% 9%	0.315 0.885	16 8	16 8	-1% -4%	0.031 0.117
421	417	-1%	0.177	254	246	-69%	0.490	159	164	3%	0.364	8	7	-7%	0.117

Inde:

ID	Name	Link ID	Ctatus	Sita Location	Direction	A Nodo	D Node	AM	Interp	PM
	Nama	1182		TOTAL	IIII		oration	Yes	Yes	Yes
	Screenline	14	Calibration	London Road South	SWB	1040	9606			
16	8 - SB	16	Calibration	A12 Tom Crisp Way	SWB	10015	3000			
	0-05	18	Calibration	A1117 Elm Tree Road	SB	3040	3030			
				TOTAL	Calit		Yes	Yes	Yes	
19	Screenline	81	Validation	Saltwater Way	NB	2050	2060			
19	9 - NB	79	Validation	A12 Pier Terrace	NB	1260	10023			
				TOTAL	Vali	dation	Yes	Yes	Yes	
20	Screenline	82	Validation	Saltwater Way	SB	2060	2050			
20	9 - SB	80	Validation	A12 Pier Terrace	SB	10023	1260			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	9	Validation	A1145 Castleton	EB	5110	5060			
21	10 - NB	11	Validation	A12 London Road	NB	5390	1000			
	10 - 140	19	Validation	A146 Beccles Road	NEB	10111	10109			
				TOTAL		Vali	dation	Yes	Yes	Yes
	Screenline	10	Validation	A1145 Castleton	WB	5060	5110			
22	10 - SB	12 Validation A12 London Road		SB	1000	5390				
	10-36	20	Validation	SWB	10109	10111		L		
				TOTAL		Vali	dation	Yes	Yes	Yes



Flow < 5%	Calib	oration	Vali	dation
All	14	88%		50%
Car		94%		25%
LGV		44%		75%
HGV		44%		0%

GEH < 4	Calib	ration	Validation				
All		100%		50%			
Car		100%		50%			
LGV		94%		100%			
HGV		100%		100%			

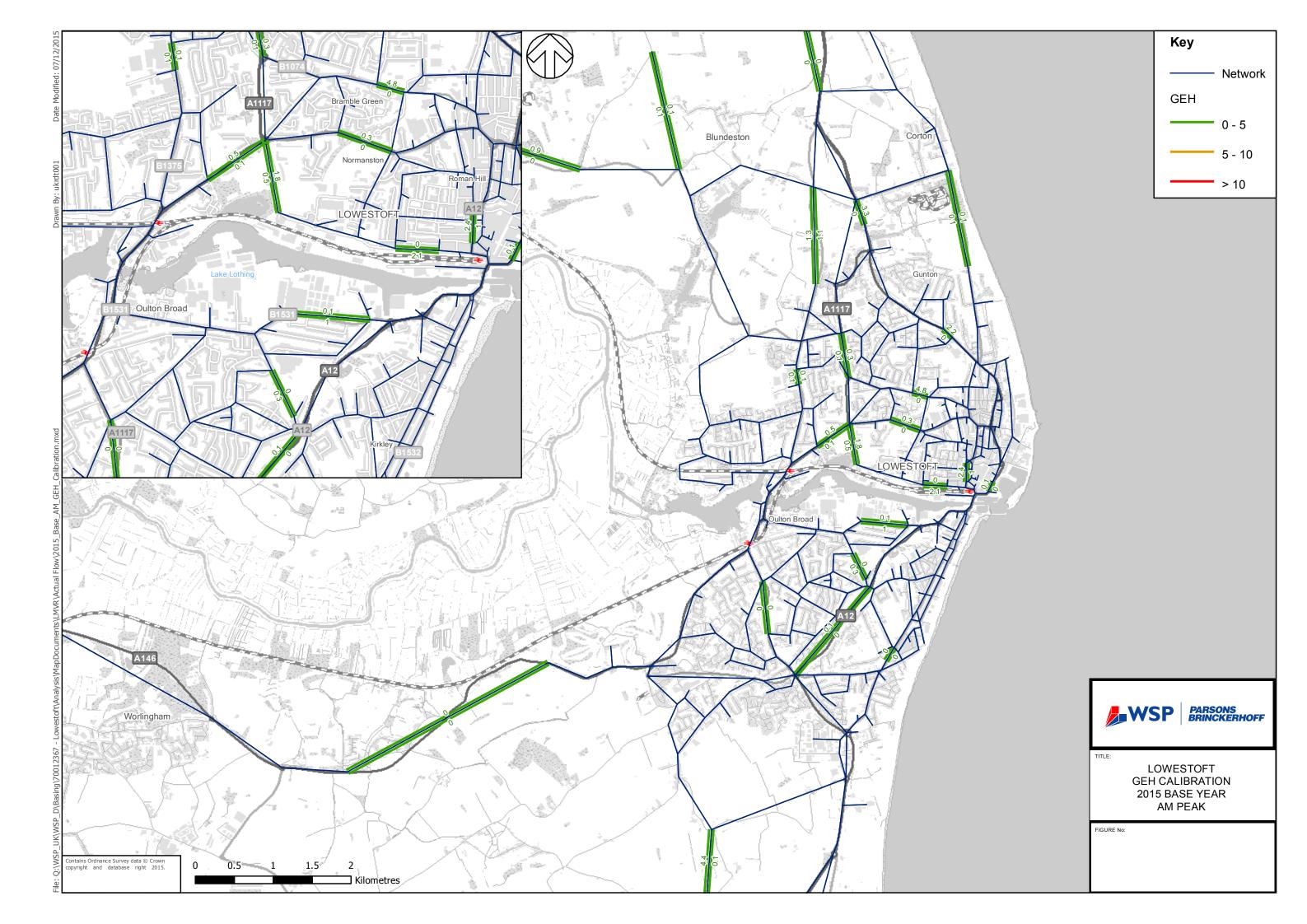
	PM Peak														
	A	JI .			С	ar			L	3V			Н	ΒV	
Observed	Modellad	Difference	CEU	Observed	Modellad	Difference	OEH	Observed	Modelled	Difference	CEU	Observed	Modellad	Difference	CEN
1443	1480	3%	0.971	923	952	3%	0.933	488	497	-2%	0.428	32	31	3%	0.171
499 708 417	483 768 448	-3% 9% 7%	0.728 2.227 1.485	270 520 256	258 540 278	-89% -32% -54%	0.708 0.891 1.323	221 174 152	216 211 161	-2% 21% 6%	0.347 2.667 0.750	9 14 9	9 17 9	6% 21% -1%	0.169 0.762 0.042
1624	1699	5%	1.846	1045	1076	3%	0.940	547	588	-8%	1.732	32	35	-11%	0.585
1114 1104	1209 976	9% -12%	2.787 3.969	852 582	747 653	-43% -78%	3.705 2.877	228 499	440 308	93% -38%	11.588 9.493	34 24	22 15	-35% -37%	2.274 2.003
2218	2185	-1%	0.703	1433	1400	-2%	0.885	727	748	-3%	0.779	58	37	36%	3.030
1133 1591	1017 1583	-10% -1%	3.538 0.201	749 1014	666 991	-62% -59%	3.135 0.730	370 539	331 557	-11% 3%	2.095 0.772	13 38	20 35	50% -8%	1.626 0.493
2724	2600	-5%	2.403	1764	1657	-6%	2.576	909	888	2%	0.705	51	55	-7%	0.502
460 759 535	519 617 434	13% -19% -19%	2.690 5.403 4.599	275 375 312	279 351 193	-66% -109% -110%	0.240 1.282 7.489	172 357 213	229 256 228	33% -28% 7%	3.997 5.784 1.044	12 26 11	11 10 13	-9% -62% 21%	0.331 3.771 0.653
1753	1570	-10%	4.501	962	823	-14%	4.667	742	713	4%	1.081	49	34	30%	2.311
448 775 491	497 794 186	11% 2% -62%	2.278 0.683 16.562	255 460 332	196 512 67	-99% -57% -128%	3.921 2.365 18.774	180 294 148	283 272 112	57% -8% -24%	6.751 1.316 3.168	12 21 10	18 10 7	45% -52% -32%	1.443 2.764 1.107
1713	1477	-14%	5.909	1047	775	-26%	9.011	623	667	-7%	1.752	43	35	20%	1.354

# Appendix E

INDIVIDUAL LINK COUNT PERFORMANCE

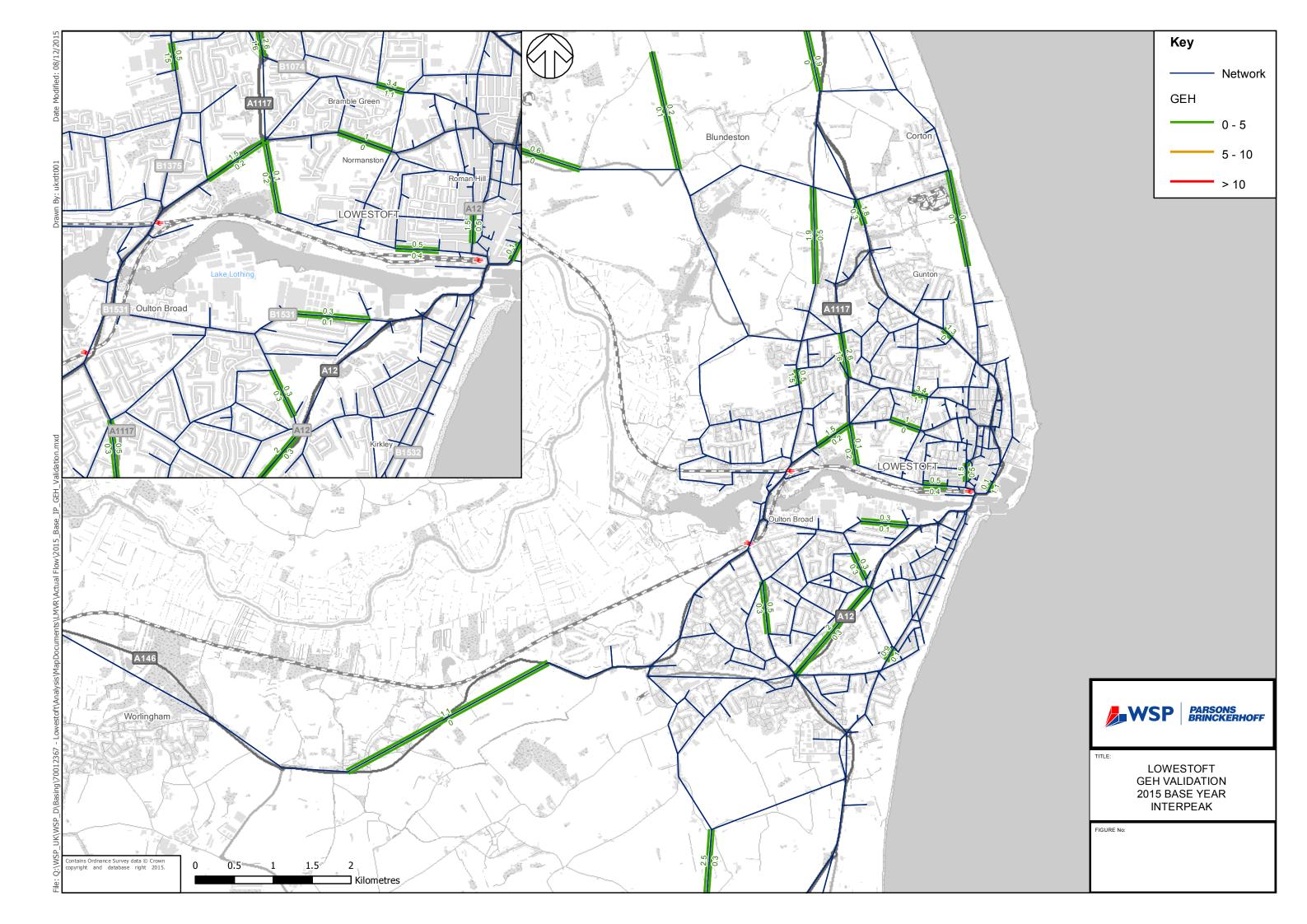
ID	Calibration / Validation	Area	ID	Site Location	Dir	Date	Data Type	Duplicate?	Ref	A-Node	B-Node	Factor	AM Peak	Interp eak	PM Peak	Check
5	Calibration		3	Gisleham Road	NB	Jul-15	ATC	No	600-501	9600	5010		Yes	Yes	Yes	OK
6	Calibration		3	Gisleham Road	SB	Jul-15	ATC	No	010-960	5010	9600		Yes	Yes	Yes	OK
7 8	Calibration Calibration		4	A146 Beccles Road A146 Beccles Road	EB WB	Jul-15 Jul-15	ATC ATC	No No	1514-451 1513-451	4514 4513	4513 4514		Yes	Yes Yes	Yes	OK OK
9	Validation		5	A1145 Castleton Avenue	EB	Jul-15	ATC	No	5110-506	5110	5060		Yes	Yes	Yes	OK
10	Validation		5	A1145 Castleton Avenue	WB	Jul-15	ATC	No	060-511	5060	5110		Yes	Yes	Yes	OK
11	Validation		6	A12 London Road	NB	Jul-15	ATC	No	390-100	5390	1000		Yes	Yes	Yes	OK
12 13	Validation Calibration		6 7	A12 London Road London Road South	SB NEB	Jul-15 Jul-15	ATC ATC	No No	1000-539 9606-104	1000	5390 1040		Yes	Yes	Yes	OK OK
14	Calibration		7	London Road South	SWB	Jul-15	ATC	No	1040-960	1040	9606		Yes	Yes	Yes	OK
15	Calibration		8	A12 Tom Crisp Way	NEB	Jul-15	ATC	No	000-1001	3000	10015		Yes	Yes	Yes	OK
16	Calibration		8	A12 Tom Crisp Way	SWB	Jul-15	ATC	No	0015-300	10015	3000		Yes	Yes	Yes	OK
17 18	Calibration Calibration		9	A1117 Elm Tree Road A1117 Elm Tree Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	8030-304 8040-303	3030	3040 3030		Yes	Yes Yes	Yes	OK OK
19	Validation		10	A146 Beccles Road	NEB	Jul-15	ATC	No	0111-101	10111	10109		Yes	Yes	Yes	OK
20	Validation		10	A146 Beccles Road	SWB	Jul-15	ATC	No	0109-101	10109	10111		Yes	Yes	Yes	OK
21	Calibration		11	Kirkley Run	NWB	Jul-15	ATC	No	0103-527	10103	5270		Yes	Yes	Yes	OK
22	Calibration Calibration		11	Kirkley Run A146 Waveney Drive	SEB EB	Jul-15 Jul-15	ATC ATC	No No	270-1010 0088-401	5270 10088	10103 4010		Yes Yes	Yes Yes	Yes Yes	OK OK
24	Calibration		12	A146 Waveney Drive	WB	Jul-15	ATC	No	010-1008	4010	10088		Yes	Yes	Yes	OK
29	Calibration		15	Katwijk Way	NB	Jul-15	ATC	No	040-1013	6040	10136		Yes	Yes	Yes	OK
30	Calibration		15	Katwijk Way	SB	Jul-15	ATC	No	0136-604	10136	6040		Yes	Yes	Yes	OK
31 32	Calibration Calibration		16 16	A12 Battery Green Road A12 Battery Green Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	6160-615 6150-616	6160	6150 6160		Yes	Yes	Yes	OK OK
33	Validation		17	A12 Old Nelson Street	NB	Jul-15	ATC	No	140-613	6140	6130		Yes	Yes	Yes	OK
34	Validation		17	A12 Old Nelson Street	SB	Jul-15	ATC	No	130-614	6130	6140		Yes	Yes	Yes	OK
35	Validation		18	St Peter's Street	EB	Jul-15	ATC	No	070-607	6070	6075		Yes	Yes	Yes	OK
36 37	Validation Calibration		18 19	St Peter's Street  Denmark Road	WB EB	Jul-15 Jul-15	ATC ATC	No No	6075-607 200-1013	6075	6070 10139		Yes	Yes Yes	Yes	OK OK
38	Calibration		19	Denmark Road  Denmark Road	WB	Jul-15 Jul-15	ATC	No	0139-720	10139	7200		Yes	Yes	Yes	OK
39	Validation		20	Rotterdam Road	NEB	Jul-15	ATC	No	7210-913	7210	9130		Yes	Yes	Yes	OK
40	Validation		20	Rotterdam Road	SWB	Jul-15	ATC	No	9130-721	9130	7210		Yes	Yes	Yes	OK
41	Calibration Calibration		21	Peto Way Peto Way	NB	Jul-15 Jul-15	ATC	No	0190-706	10190	7060		Yes	Yes	Yes	OK OK
42 43	Calibration		22	A1117 Normanston Drive	SB NEB	Jul-15 Jul-15	ATC ATC	No No	060-1019 7050-706	7060 7050	10190 7060		Yes	Yes Yes	Yes	OK
44	Calibration		22	A1117 Normanston Drive	SWB	Jul-15	ATC	No	7060-705	7060	7050		Yes	Yes	Yes	OK
45	Calibration		23	A1144 Normanston Drive	EB	Jul-15	ATC	No	240-913	9240	9130		Yes	Yes	Yes	OK
46	Calibration		23	A1144 Normanston Drive Oulton Road	WB	Jul-15	ATC	No	9130-924	9130	9240		Yes	Yes	Yes	OK
47 48	Calibration Calibration		24	Oulton Road Oulton Road	EB WB	Jul-15 Jul-15	ATC ATC	No No	270-1001 0010-927	9270	10010 9270	1	Yes	Yes	Yes	OK OK
49	Calibration		25	B1375 Gorleston Road	NB	Jul-15	ATC	No	8030-804	8030	8040		Yes	Yes	Yes	OK
50	Calibration		25	B1375 Gorleston Road	SB	Jul-15	ATC	No	8040-803	8040	8030		Yes	Yes	Yes	OK
51	Calibration		26	A1117 Millennium Way	NB	Jul-15	ATC		7070-708	7070	7080		Yes	Yes	Yes	OK
52 53	Calibration Calibration		26 27	A1117 Millennium Way A12 Yarmouth Road	SB NWB	Jul-15 Jul-15	ATC ATC	No No	7080-707 0242-102	7080 10242	7070 10248		Yes	Yes Yes	Yes	OK OK
54	Calibration		27	A12 Yarmouth Road	SEB	Jul-15	ATC		0248-102	10248	10242		Yes	Yes	Yes	OK
55	Calibration		28	B1385 Corton Road	NB	Jul-15	ATC	No	9460-948	9460	9480		Yes	Yes	Yes	OK
56	Calibration		28	B1385 Corton Road	SB	Jul-15	ATC	No	9480-946	9480	9460		Yes	Yes	Yes	OK
57 58	Calibration Calibration		29 29	A12 Yarmouth Road A12 Yarmouth Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	0257-625 250-1025	10257 6250	6250 10257		Yes	Yes Yes	Yes	OK OK
59	Calibration		30	B1375 Parkhill	NB	Jul-15	ATC	No	0001-807	10001	8070		Yes	Yes	Yes	OK
60	Calibration		30	B1375 Parkhill	SB	Jul-15	ATC	No	070-1000	8070	10001		Yes	Yes	Yes	OK
61	Calibration		31	B1074 Bluderston Road	NB	Jul-15	ATC	No	0025-200	10025	20026		Yes	Yes	Yes	OK
62 63	Calibration Calibration		31	B1074 Bluderston Road Fixton Road	SB NB	Jul-15 Jul-15	ATC ATC	No No	0026-100 440-1002	20026	10025 10024		Yes	Yes	Yes	OK OK
64	Calibration		32	Fixton Road	SB	Jul-15	ATC	No	0024-944	10024	9440		Yes	Yes	Yes	OK
65	Validation		33	Coast Road	NB	Jul-15	ATC	No	510-1002	9510	10027		Yes	Yes	Yes	OK
66	Validation		33	Coast Road	SB	Jul-15	ATC	No	0027-951	10027	9510		Yes	Yes	Yes	OK
67 75	Validation Calibration	0	6/605 3	Katwijk Way A12YarmouthRd	NB NB	Jul-13 Jul-15	TRADS ANPR	No No	7280-606 3280-452	7280 6280	6060 4520		Yes	Yes Yes	Yes	OK OK
76	Calibration		3	A12YarmouthRd	SB	Jul-15	ANPR	No	1520-628	4520	6280		Yes	Yes	Yes	OK
79	Validation		5	A12 Pier Terrace	NB	Jul-15	ANPR	No	260-1002	1260	10023		Yes	Yes	Yes	OK
80	Validation		5	A12 Pier Terrace	SB	Jul-15	ANPR	No No	0023-126	10023	1260		Yes	Yes	Yes	OK
81 82	Validation Validation		6	Saltwater Way Saltwater Way	NB SB	Jul-15 Jul-15	ANPR ANPR	No No	2050-206 2060-205	2050	2060 2050		Yes Yes	Yes Yes	Yes	OK OK
99	Validation		15	North Quay Retail Park	Entry	Jul-15	ANPR	No	9220-923	9220	9230		Yes	Yes	Yes	OK
100	Validation		15	North Quay Retail Park	Exit	Jul-15	ANPR	No	9230-922	9230	9220		Yes	Yes	Yes	OK
101	Validation		16	Links Road Car Park	EB	Jul-15	ANPR		9602-960	9602	9603		Yes	Yes	Yes	OK
102	Validation Validation		16 17	Links Road Car Park Swimming Pool Road Car Park	WB EB	Jul-15 Jul-15	ANPR ANPR	No No	9603-960 090-1025	9603	9602 10251		Yes	Yes	Yes	OK OK
104	Validation		17	Swimming Pool Road Car Park	WB	Jul-15	ANPR	No	0251-909	10251	9090		Yes	Yes	Yes	OK
106	Validation		18	Battery Green Road Car Park	Exit	Jul-15	ANPR	No	0127-101	10127	10126		Yes	Yes	Yes	OK
107	Validation		19	Gordon Road Car Park Entry	Entry	Jul-15	ANPR	No No	140-905	6140	9050		Yes	Yes	Yes	OK
109 112	Validation Validation		20	Surrey Street Car Park Entry Clapham Road Car Park Exit	Entry	Jul-15 Jul-15	ANPR ANPR	No No	0130-101 0132-101	10130	10131 10133		Yes Yes	Yes	Yes Yes	OK OK
113	Validation		22	Clapham Road South	Entry	Jul-15	ANPR	No	0137-101	10137	10138		Yes	Yes	Yes	OK
114	Validation		22	Clapham Road South	Exit	Jul-15	ANPR	No	0138-101	10138	10137		Yes	Yes	Yes	OK
115	Validation Validation		23	St Johns Road Car Park	Entry	Jul-15	ANPR		0083-100	10083	10084		Yes	Yes	Yes	OK
116 117	Validation Validation		23 24a	St Johns Road Car Park Kirkley Rise Car Park	Exit	Jul-15 Jul-15	ANPR ANPR		0084-100 000-1025	10084	10083 10256		Yes	Yes	Yes	OK OK
118	Validation		24a	Kirkley Rise Car Park	Exit	Jul-15 Jul-15	ANPR	No	0256-400	10256	4000		Yes	Yes	Yes	OK
119	Validation		24b	Kirkley Rise Car Park	Entry	Jul-15	ANPR	No	300-1007	5300	10078		Yes	Yes	Yes	OK
120	Validation		24b	Kirkley Rise Car Park	Exit	Jul-15	ANPR	No	0078-530	10078	5300		Yes	Yes	Yes	OK
121 122	Validation Validation		25 25	Kirkley Cliff Road Car Park Kirkley Cliff Road Car Park	Entry Exit	Jul-15 Jul-15	ANPR ANPR	No No	120-1007 0075-112	1120	10075 1120	-	Yes	Yes Yes	Yes	OK OK
125	Validation		27	Marine Parade	Entry	Jul-15 Jul-15	ANPR		0075-112	10075	10082		Yes	Yes	Yes	OK
126	Validation		27	Marine Parade	Exit	Jul-15	ANPR	No	0082-100	10082	10081		Yes	Yes	Yes	OK
127	Validation		28	Asda Car Park	Entry	Jul-15	ANPR	No	000-1008	4000	10085		Yes	Yes	Yes	OK
128	Validation		28	Asda Car Park	Exit	Jul-15	ANPR	No	0085-400	10085	4000		Yes	Yes	Yes	OK

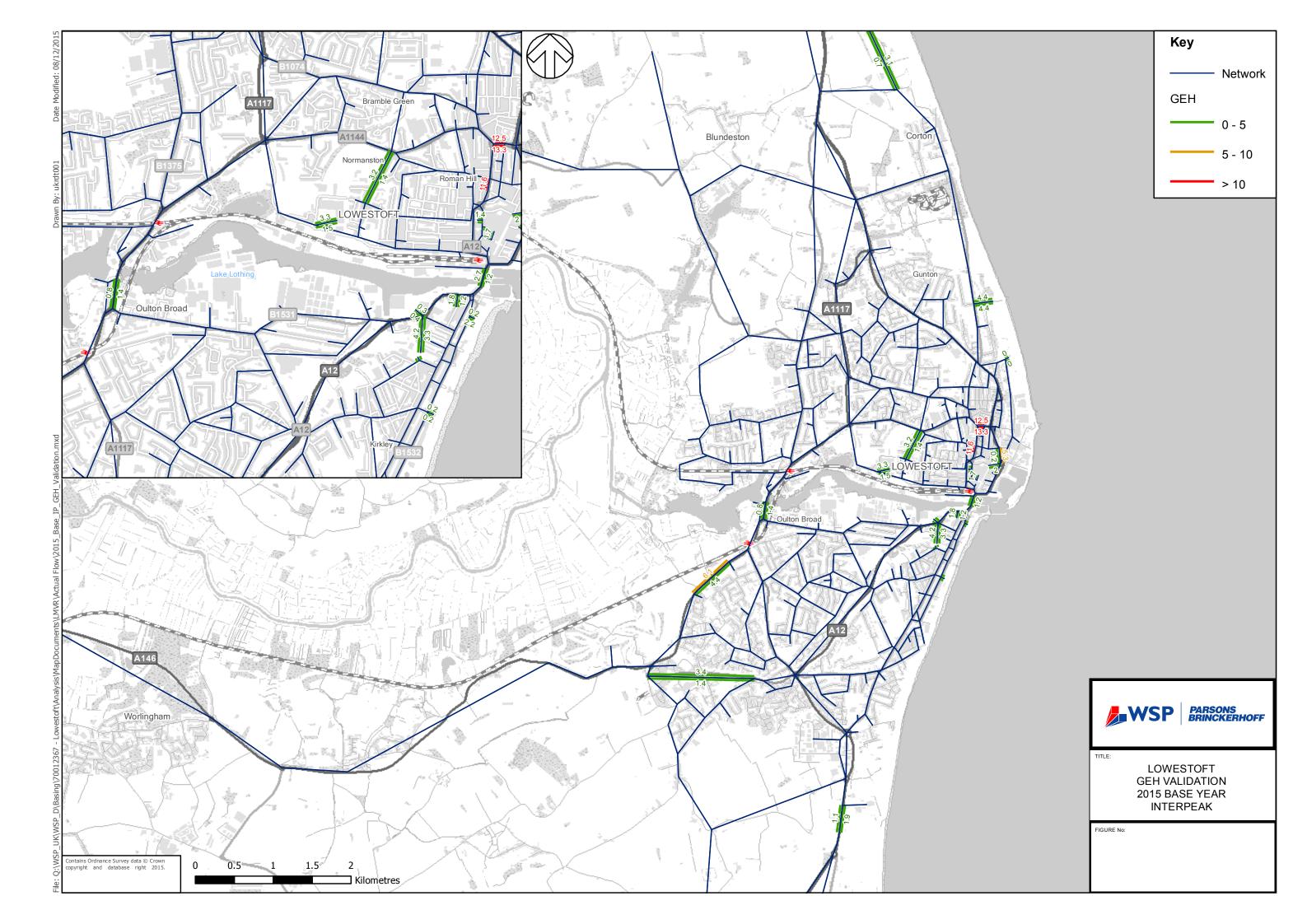
Column     Column     Column     Column   Colu									Peak							
1			ALL VEHICLE	ES	•			CAR				LGV			HGV	
1	Observed	Madellad	CELL	OFH Person	Flow Boss 2	Observed	Madellad	CELL	OFH Bases	Flow Bosso	Observed	Madellad	OFIL	Observed	Madellad	CELL
17	Observed	Modelled	GEH	GER Pass?	Flow Pass?	Observed	Modelled	GER	GER Pass?	Flow Pass?	Observed	wodelled	GER	Observed	wodelied	GEH
17	21	5	4.360	Yes	Yes	6	3	1.308	Yes	Yes	14	1	4.663	1	1	0.250
Fig.												9			3	
441 3869 2766 V66 V66 V67 2772 280 282 3.800 V66 V66 V66 1260 128 2.201 382 3.50 1.277 1.2	639		0.000					0.000			312	312	0.000	60		0.000
1950   1967   1968   1969																
Prop.   Prop																
## Part																
GEO   CAST   C																
1969   1969																
SEC   199   0.454   Yes   Yes   1620   199   0.447   Yes   Yes   172   172   0.000   29   29   0.000   180																
361   361   361   362   363																
200   203											111					
1975   1975	310	309	0.043	Yes	Yes			0.039	Yes	Yes				18	18	0.088
SS   192   1920   190																
129																
General Color   Print   Prin																
344																
15																
411   364   2388   Yes   Yes   261   231   1500   Yes   Yes   122   197   1377   288   280   0.448																
GFT																
STI   STO   CO.031   Vest   Vest   SST   SST   SST   SST   SST   Vest   Vest   SST   SST   SST   SST   SST   SST   Vest	134	123	0.970	Yes	Yes	87	87		Yes	Yes	34	34	0.029	13	2	4.093
144   943   2,915   No																
Add																
Sept																
196																
215   214   0.038																
304   342   2.133   Ves.   Ves.   Ves.   262   227   1.715   Ves.   Ves.   590   103   1.300   12   12   12   0.130   136   117   1.706   Ves.   Ves.   76   30   1.586   Ves.   Ves.   73   23   5.044   3   4   0.036   28   28   28   28   28   28   28   2																
136																
3986   388	136	117	1.708	Yes	Yes	76	90	1.588	Yes	Yes	57	23	5.404		4	0.288
317   226																
687   689   0.471   Ves																
408																
190																
476 377 4780 Yes Yes Yes 149 149 1000 Yes Yes 201 103 7010 12 11 10.000																
246         246         268         Yes         Yes         149         449         0.009         Yes         Yes         90         90         0.023         8         7         0.206           584         582         0.058         Yes         Yes         455         453         0.112         Yes         Yes         Yes         160         0.003         18         2         0.003         18         2         0.003         18         0.003         16         0.003         16         0.003         16         0.003         16         0.003         18         0.003         16         0.003         18         0.003         18         0.003         18         0.003         18         18         0.003         18         18         0.003         18         18         0.003         18         18         0.003         18         18         0.003         18         18         18         0.003         18         18         0.003         18         18         18         0.003         18         18         0.003         18         18         0.003         18         18         0.003         18         18         0.003         18         18 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>																
484         482         0.078         Yes         Yes         291         91         91         91         0.030         16         16         0.108           376         378         0.124         Yes         Yes         298         298         298         0.003         Yes         Yes         60         60         0.052         22         20         0.009           480         485         0.054         Yes         Yes         488         229         1.00	246							0.009								
378																
450         455         0.254         Yes         Yes         375         379         0.206         Yes         Yes         598         60         0.156         16         16         0.050           460         460         760         Yes         Yes         401         401         0.017         Yes         Yes         139         1.000         23         2.27         0.000           661         595         2.248         Yes         401         401         0.017         Yes         14         14         0.03         1         1         0.000           102         101         0.062         Yes         16         81         82         0.017         Yes         Yes         20         20         20         0.003         1         1         0.000           102         101         0.062         Yes         461         82         0.065         Yes         Yes         20         20         20         20         0.003         1         1         0.000           461         434         1.284         Yes         364         378         0.007         Yes         461         43         2.271         1         1 <td></td>																
460																
661 5965																
96 97 0.089 Yes Yes 81 82 0.111 Yes Yes 14 14 0.033 1 1 0.090 102 101 0.062 Yes Yes 81 80 0.056 Yes Yes 20 20 0.066 1 1 0.344 567 656 0.047 Yes Yes 456 456 0.012 Yes Yes 88 84 0.022 27 26 0.122 567 647 3.262 Yes Yes 456 456 0.012 Yes Yes 132 133 0.120 24 24 0.076 461 434 1.284 Yes Yes 384 378 0.307 Yes Yes 64 33 2.271 133 13 0.046 461 434 1.284 Yes Yes 178 198 1.304 Yes Yes 86 65 0.041 8 8 0.117 113 102 0.854 Yes Yes 104 108 108 1.304 Yes Yes 65 65 0.041 8 8 0.117 113 122 0.854 Yes Yes 104 108 108 1.304 Yes Yes 94 0.000 5 5 5 0.110 51 52 0.033 Yes Yes Yes 8 9 0.012 Yes Yes 38 99 0.027 4 4 0.084 84 85 0.109 Yes Yes 8 9 0.024 Yes Yes 38 99 0.027 4 4 0.084 85 0.109 Yes Yes 8 9 0.024 Yes Yes 38 99 0.027 4 4 0.084 86 85 0.109 Yes Yes 8 9 10 0.024 Yes Yes 38 99 0.027 4 4 0.084 87 88 1 88 1 0.09 Yes Yes 8 11 28 3.333 Yes Yes Yes 39 18 0.033 3 3 0.095 414 99 19 0.668 No No 381 85 19.592 No No 18 12 1.549 15 2 0 0.004 1633 1353 1353 0.000 Yes Yes Yes 118 26 3.333 Yes Yes Yes 135 0.000 44 44 0.0004 1633 1353 1353 0.000 Yes Yes Yes 118 0.037 Yes Yes 135 0.000 44 44 0.0004 1633 1359 0.000 Yes Yes Yes 9 11 28 0.333 Yes Yes Yes 135 0.000 44 44 0.0004 1633 1359 0.000 Yes Yes Yes 9 11 28 0.037 Yes Yes 135 0.000 44 44 0.0004 1633 1359 0.000 Yes Yes Yes 9 11 28 0.037 Yes Yes 135 0.000 44 44 0.0004 1633 1359 0.000 Yes Yes Yes 9 18 0.037 Yes Yes 135 0.000 44 44 0.0000 1633 1359 0.000 Yes Yes Yes 9 18 0.037 Yes Yes 135 0.000 44 44 0.0000 164 0.000 Yes Yes Yes 9 18 0.000 Yes Yes Yes 135 0.0000 0.000 0.000 0.0000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000																
101																
Seff																
461	567	566				456	456	0.012			85	84		27	26	0.122
251   269																
179																
113																
51         52         0.093         Yes         Yes         9         9         0.112         Yes         Yes         39         39         0.027         4         4         0.084           84         85         0.109         Yes         Yes         8         8         77         10.584         No         Yes         51         6         8.433         2         0         1.871           50         38         1.309         Yes         Yes         11         26         3.383         Yes         Yes         37         12         4.975         2         0         2.062         414         99         19.668         No         No         381         85         19.392         No         No         18         12         1.549         15         2         0         2.062         4.459         932         9333         0.033         Yes         Yes         76         747         0.037         Yes         Yes         135         135         0.000         44         44         0.000         1353         1353         0.000         Yes         Yes         135         135         0.000         44         44         0.000         1353																
84         85         0.109         Yes         Yes         8         9         0.224         Yes         Yes         T3         73         0.039         3         3         0.085           61         83         2.699         Yes         Yes         11         26         3.333         Yes         Yes         37         12         4.975         2         0         2.062           414         99         19.668         No         No         381         185         19.392         No         No         18         12         4.975         2         0         2.062         9.33         0.033         Yes         Yes         747         0.037         Yes         Yes         142         1.900         44         44         0.000           1353         3.000         Yes         Yes         178         178         178         178         0.000         441         44         0.000         441         44         0.000         441         44         0.000         441         442         0.000         441         441         442         0.000         441         448         142         142         0.000         441         441 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>																
61																
50													8.443			
414   99	50	38	1.809		Yes	11	26			Yes	37	12	4.975	2	0	2.062
1353         1353         0.000         Yes         Yes         1178         0.000         Yes         Yes         135         135         0.00         40         40         0.000           1531         1395         3.556         Yes         Yes         566         6.839         6.688         No         No         810         500         12.103         65         56         1.173         894         768         4.504         Yes         Yes         530         473         2.555         Yes         Yes         322         256         3.869         46         39         1.077           944         973         0.937         Yes         Yes         666         545         4.520         Yes         No         242         383         7.974         46         45         0.178           904         902         0.067         Yes         Yes         566         545         4.520         Yes         Yes         367         344         1.230         31         40         1.539           158         170         0.937         Yes         Yes         143         105         3.413         Yes         Yes         15         65							85					12				
1531   1395   3.556   Yes   Yes   656   839   6.688   No   No   810   500   12.103   65   56   1.173     944   973   0.937   Yes   Yes   530   473   2.555   Yes   Yes   322   256   3.889   46   39   1.077     944   973   0.937   Yes   Yes   506   518   0.532   Yes   No   242   383   7.974   46   45   0.178     904   902   0.067   Yes   Yes   506   518   0.532   Yes   Yes   367   344   1.230   31   40   1.539     158   170   0.937   Yes   Yes   143   105   3.413   Yes   Yes   15   65   7.906   0   0   0.000     86   154   6.208   No   Yes   Yes   3 0   0.2449   Yes   Yes   14   41   5.149   1   1   0.000     4   0   2.828   Yes   Yes   4   0   2.828   Yes   Yes   0   0   0.000   0   0   0.000     4   0   2.828   Yes   Yes   4   0   2.828   Yes   Yes   0   0   0.000   0   0   0.000     0   0   0.000   Yes   Yes   0   0   0.000   Yes   Yes   0   0   0.000   0   0   0.000     0   0   0.000   Yes   Yes   0   0   0.000   0   0   0.000     0   0   0.000   Yes   Yes   0   0   0.000   0   0   0.000     2   0   2.000   Yes   Yes   2 0   0   0.000   Yes   Yes   0   0   0.000   0   0   0.000     32   17   3.030   Yes   Yes   32   17   3.030   Yes   Yes   0   0   0.000   0   0   0.000     22   33   2.098   Yes   Yes   32   3   17   3.030   Yes   Yes   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   32   3   17   3.030   Yes   Yes   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   3   0   2.449   Yes   Yes   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   9   10   3.244   Yes   Yes   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   27   18   1.897   Yes   Yes   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   9   10   3.244   Yes   Yes   9   0   0   0.000   0   0   0.000     27   46   3.145   Yes   Yes   9   10   3.244   Yes   Yes   0   0   0.000   0   0   0.000     38   2.132   Yes   Yes   9   10   3.244   Yes   Yes   0   0   0.000   0   0   0.000     39   30   3.444   Yes   Yes   5   5   7   0.816   Yes   Yes   5   0   0.000   0   0   0.000																
898         768         4.50.4         Yes         Yes         650         473         2.55.5         Yes         No         242         322         256         3.869         46         39         1.077           904         902         0.067         Yes         Yes         506         518         0.532         Yes         Yes         367         344         1.230         31         40         1.539           158         170         0.937         Yes         Yes         143         105         3.413         Yes         Yes         15         65         7.906         0         0         0.000           36         154         6.208         No         Yes         71         112         4.286         Yes         Yes         14         41         5.7906         0         0         0.000           3         0         2.449         Yes         Yes         49         Yes         Yes         0         0         0.000         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>																
944         973         0.937         Yes         Yes         656         545         4.520         Yes         No         242         383         7.974         46         45         0.178           904         902         0.067         Yes         Yes         506         518         0.532         Yes         Yes         367         344         1.230         31         40         1.539           158         170         0.937         Yes         Yes         143         105         3.413         Yes         Yes         15         65         7.906         0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>																
904         902         0.067         Yes         Yes         506         518         0.532         Yes         Yes         387         344         1.230         31         40         1.539           158         170         0.937         Yes         Yes         143         105         3.413         Yes         Yes         15         65         7.906         0         0         0.000           3         0         2.449         Yes         Yes         3         0         2.449         Yes         Yes         0         0         0.000         0         0         0.000           4         0         2.2828         Yes         Yes         0         0         0.000         0         0         0.000           0         0         0.000         Yes         Yes         0         0         0.000         0         0.000         0         0         0.000         0         0         0.000         0         0         0.000         0         0         0.000         0         0         0.000         0         0         0.000         0         0         0.000         0         0.000         0         0.000																
158																
86         154         6.208         No         Yes         71         112         4.286         Yes         Yes         14         41         5.149         1         1         0.000           3         0         2.449         Yes         Yes         0         0         0.000         0         0         0.000         0         <	158	170				143	105		Yes		15	65				
4         0         2.828         Yes         Yes         0         0         0.000         0	86		6.208	No		71		4.286		Yes	14	41	5.149	1	1	0.000
0         0         0.000         Yes         Yes         0         0         0.000         Yes         0         0         0.000         0																
0         0         0.000         Yes         Yes         0         0.000         Yes         Yes         0         0.000																
2         0         2,000         Yes         Yes         2         0         2,000         Yes         Yes         0         0         0,000         0         0,000           32         17         3,030         Yes         Yes         0         0         0,000         0         0,000           22         33         2,098         Yes         Yes         0         0         0,000         0         0,000           3         0         2,449         Yes         Yes         3         0         2,449         Yes         0         0         0,000         0         0,000           27         46         3,145         Yes         Yes         9         10         0,324         Yes         Yes         0         23         6,782         0         5         3,162           10         15         1,414         Yes         Yes         9         10         0,324         Yes         Yes         1         4         1,887         0         5         3,162           10         15         1,414         Yes         Yes         9         10         0,324         Yes         Yes         1         4 <td></td>																
32																
22         33         2.098         Yes         Yes         22         33         2.098         Yes         Yes         0         0         0.000         0         0.000           3         0         2.249         Yes         Yes         Yes         0         0         0.000         0         0.000           27         46         3.145         Yes         Yes         9         10         0.324         Yes         Yes         0         23         6.782         0         5         3.162           10         15         1.414         Yes         Yes         9         10         0.324         Yes         Yes         1         4         1.897         0         1         1.414           5         3         1.000         Yes         Yes         2         2         0.2000         1         0         1.414           5         3         1.000         Yes         Yes         2         2         0.000         Yes         Yes         2         1         0.816         1         0         1.414           5         3         1.000         Yes         Yes         2         1         0.816																
3         0         2.449         Yes         Yes         3         0         2.449         Yes         Yes         0         0         0.000         0         0.000           27         46         3.145         Yes         Yes         27         18         1.897         Yes         Yes         0         5         3.000         5         3.000         5         3.000         1         1.414         Yes         Yes         9         10         0.324         Yes         Yes         1         4         1.897         0         1         1.414           3         8         2.132         Yes         Yes         0         8         4.000         Yes         Yes         2         0         2.000         1         0         1.414           27         23         0.800         Yes         Yes         2         2         0         2.000         0         0         0.000           11         10         0.309         Yes         Yes         9         10         0.324         Yes         Yes         2         0         2.000         0         0         0.000           11         10         0.316 <td></td>																
27         46         3.145         Yes         Yes         27         18         1.897         Yes         Yes         0         23         6.782         0         5         3.162           10         15         1.414         Yes         Yes         9         10         0.324         Yes         Yes         1         4         1.1897         0         1         1.414           3         8         2.132         Yes         Yes         0         8         4.000         Yes         Yes         2         0         2.000         1         0         1.414           5         3         1.000         Yes         Yes         2         2         0.000         Yes         Yes         2         1         0.816         1         0         1.414           5         3         1.000         Yes         Yes         2         2         0.000         Yes         2         1         0.816         1         0         1.414           5         3         1.000         Yes         Yes         2         1         0.806         1         0         1.414           11         1.0         0.309																
3         8         2.132         Yes         Yes         0         8         4.000         Yes         Yes         2         0         2.000         1         0         1.414           5         3         1.000         Yes         Yes         2         2         0.000         Yes         Yes         2         1         0.816         1         0         1.414           27         23         0.800         Yes         Yes         25         23         0.408         Yes         Yes         2         0         2.000         0         0         0.000           11         10         0.309         Yes         Yes         9         10         0.324         Yes         Yes         2         0         2.000         0         0         0.000           5         7         0.816         Yes         Yes         Yes         Yes         2         0         2.000         0         0         0.000           3         2         0.632         Yes         Yes         9         0         0         0.000         0         0.000           1         0         1.414         Yes         Yes	27	46	3.145		Yes	27		1.897			0		6.782	0		
5         3         1.000         Yes         Yes         2         2         0.000         Yes         Yes         2         1         0.816         1         0         1.414           27         23         0.800         Yes         Yes         25         23         0.408         Yes         Yes         2         0         2.000         0         0         0.000           11         10         0.309         Yes         Yes         9         10         0.324         Yes         Yes         2         0         2.000         0         0.000           5         7         0.816         Yes         Yes         Yes         0         0         0.000         0         0.000           3         2         0.632         Yes         Yes         3         2         0.632         Yes         O         0         0.000         0         0.000           1         0         1.414         Yes         Yes         Yes         0         0         0.000         0         0.000           0         2         2.000         Yes         Yes         0         1         1.414         Yes         Yes																
27         23         0.800         Yes         Yes         25         23         0.408         Yes         Yes         2         0         2.000         0         0.000           11         10         0.309         Yes         Yes         9         10         0.324         Yes         Yes         2         0         2.000         0         0         0.000           5         7         0.816         Yes         Yes         Yes         0         0         0.000         0         0.000           3         2         0.632         Yes         Yes         Yes         0         0         0.000         0         0.000           1         0         1.414         Yes         Yes         0         0         0.000         0         0.000           0         2         2.000         Yes         Yes         0         1         1.414         O         0         0.000           0         2         2.000         Yes         Yes         0         1         1.414         O         0         0.000           6         0         3.464         Yes         Yes         5         0																
11         10         0.309         Yes         Yes         9         10         0.324         Yes         Yes         2         0         2.000         0         0         0.000           5         7         0.816         Yes         Yes         0         0         0.000         0         0         0.000           3         2         0.632         Yes         Yes         0         0         0.000         0         0.000           1         0         1.414         Yes         Yes         0         0         0.000         0         0.000           0         2         2.000         Yes         Yes         Yes         0         0         0.000         0         0.000           6         0         3.464         Yes         Yes         5         0         3.162         Yes         Yes         1         0         1.414         Yes         Yes         1         0         0.000           3         0         2.449         Yes         Yes         1         0         1.414         Yes         Yes         1         0         0.000         0         0.000           3         <																
5         7         0.816         Yes         Yes         5         7         0.816         Yes         Yes         0         0         0.000         0         0.000           3         2         0.632         Yes         Yes         0         0         0.000         0         0.000           1         0         1.414         Yes         Yes         0         0         0.000         0         0.000           0         2         2.000         Yes         Yes         0         1         1.414         Yes         Yes         0         1         1.414         0         0         0.000           6         0         3.464         Yes         Yes         5         0         3.162         Yes         Yes         1         0         1.414         0         0         0.000           3         0         2.449         Yes         Yes         3         0         2.449         Yes         Yes         0         0         0.000         0         0         0.000           229         266         2.352         Yes         Yes         215         216         0.068         Yes         Yes																
3         2         0.632         Yes         Yes         3         2         0.632         Yes         Yes         0         0         0.000         0         0.000           1         0         1.414         Yes         Yes         0         0         0.000         0         0.000           0         2         2.000         Yes         Yes         0         1         1.414         0         0         0.000           6         0         3.464         Yes         Yes         5         0         3.162         Yes         Yes         1         0         1.414         0         0         0.000           3         0         2.449         Yes         Yes         Yes         Yes         0         0         0.000         0         0.000           229         266         2.352         Yes         Yes         215         216         0.068         Yes         Yes         14         50         6.364         0         0         0.000																
1     0     1.414     Yes     Yes     1     0     1.414     Yes     Yes     0     0     0.000     0     0.000       0     2     2.000     Yes     Yes     0     1     1.414     Yes     Yes     0     1     1.414     0     0     0.000       6     0     3.464     Yes     Yes     5     0     3.162     Yes     Yes     1     0     1.414     0     0     0.000       3     0     2.449     Yes     Yes     3     0     2.449     Yes     Yes     0     0     0.000     0     0     0.000       229     266     2.352     Yes     Yes     215     216     0.068     Yes     Yes     14     50     6.364     0     0     0.000																
0     2     2.000     Yes     Yes     0     1     1.414     Yes     Yes     0     1     1.414     0     0     0.000       6     0     3.464     Yes     Yes     5     0     3.162     Yes     Yes     1     0     1.414     0     0     0.000       3     0     2.449     Yes     Yes     3     0     0     0     0.000     0     0     0.000       229     266     2.352     Yes     Yes     215     216     0.068     Yes     Yes     Yes     14     50     6.364     0     0     0.000																
6         0         3.464         Yes         Yes         5         0         3.162         Yes         Yes         1         0         1.414         0         0         0.000           3         0         2.449         Yes         Yes         1         0         0.000         0         0         0.000           229         266         2.352         Yes         Yes         215         216         0.068         Yes         Yes         14         50         6.364         0         0         0.000																
3 0 2.449 Yes Yes 3 0 2.449 Yes Yes 0 0 0.000 0 0.000 229 266 2.352 Yes Yes 215 216 0.068 Yes Yes 14 50 6.364 0 0 0.000			3.464			5	0	3.162			1	0	1.414			0.000
	3	0	2.449	Yes	Yes	3	0	2.449	Yes	Yes		0	0.000		0	0.000
168   169   0.077   Yes   Yes   155   142   1.067   Yes   Yes   13   27   3.130   0   0   0.000																
	168	169	0.077	Yes	Yes	155	142	1.067	Yes	Yes	13	27	3.130	0	0	0.000



ID	Calibration / Validation	Area	ID	Site Location	Dir	Date	Data Type	Duplicate?	Ref	A-Node	B-Node	Factor Pea	Interp k eak	PM Peak	Check
5	Calibration		3	Gisleham Road	NB	Jul-15	ATC	No	9600-5010	9600	5010	Ye		Yes	OK
6 7	Calibration Calibration		3	Gisleham Road A146 Beccles Road	SB EB	Jul-15 Jul-15	ATC ATC	No No	5010-9600 1514-4513	5010 4514	9600 4513	Ye.	Yes Yes	Yes	OK OK
8	Calibration		4	A146 Beccles Road	WB	Jul-15	ATC	No	1513-4514	4513	4514	Ye		Yes	OK
9	Validation		5	A1145 Castleton Avenue	EB	Jul-15	ATC	No	110-5060	5110	5060	Ye		Yes	OK
10 11	Validation Validation		5	A1145 Castleton Avenue A12 London Road	WB NB	Jul-15 Jul-15	ATC ATC	No No	5060-5110 5390-1000	5060 5390	5110 1000	Ye: Ye:		Yes	OK OK
12	Validation		6	A12 London Road	SB	Jul-15	ATC	No	1000-5390	1000	5390	Ye		Yes	OK
13	Calibration		7	London Road South	NEB	Jul-15	ATC	No	9606-1040	9606	1040	Ye		Yes	OK
14 15	Calibration Calibration		7	London Road South A12 Tom Crisp Way	SWB NEB	Jul-15 Jul-15	ATC ATC	No No	040-9606 000-1001	1040 3000	9606 10015	Ye: Ye:		Yes	OK OK
16	Calibration		8	A12 Tom Crisp Way	SWB	Jul-15	ATC	No	0015-300	10015	3000	Ye		Yes	OK
17	Calibration		9	A1117 Elm Tree Road	NB	Jul-15	ATC	No	3030-3040	3030	3040	Ye		Yes	OK
18 19	Calibration Validation		9	A1117 Elm Tree Road A146 Beccles Road	SB NEB	Jul-15 Jul-15	ATC ATC	No No	3040-3030 0111-1010	3040 10111	3030 10109	Ye: Ye:		Yes	OK OK
20	Validation		10	A146 Beccles Road	SWB	Jul-15	ATC	No	0109-101	10109	10111	Ye		Yes	OK
21	Calibration		11	Kirkley Run	NWB	Jul-15	ATC	No	0103-527	10103	5270	Ye		Yes	OK
22	Calibration Calibration		11	Kirkley Run A146 Waveney Drive	SEB EB	Jul-15 Jul-15	ATC ATC	No No	270-1010 0088-401	5270 10088	10103 4010	Ye: Ye:		Yes	OK OK
24	Calibration		12	A146 Waveney Drive	WB	Jul-15	ATC	No	010-1008	4010	10088	Ye		Yes	OK
29	Calibration		15	Katwijk Way	NB	Jul-15	ATC	No	040-1013	6040	10136	Ye		Yes	OK
30 31	Calibration		15 16	Katwijk Way A12 Battery Green Road	SB NB	Jul-15 Jul-15	ATC ATC	No No	0136-604 3160-6150	10136 6160	6040 6150	Ye: Ye:		Yes	OK OK
32	Calibration Calibration		16	A12 Battery Green Road	SB	Jul-15 Jul-15	ATC	No	3150-6160	6150	6160	Ye		Yes	
33	Validation		17	A12 Old Nelson Street	NB	Jul-15	ATC	No	3140-6130	6140	6130	Ye	Yes	Yes	OK
34 35	Validation Validation		17 18	A12 Old Nelson Street St Peter's Street	SB EB	Jul-15 Jul-15	ATC ATC	No No	3130-6140 3070-6075	6130 6070	6140 6075	Ye. Ye.		Yes	OK OK
36	Validation Validation		18	St Peter's Street St Peter's Street	WB	Jul-15 Jul-15	ATC	No No	075-607	6075	6070	Ye	Yes Yes	Yes	OK
37	Calibration		19	Denmark Road	EB	Jul-15	ATC	No	200-1013	7200	10139	Ye	Yes	Yes	OK
38	Calibration Validation		19	Denmark Road	WB	Jul-15	ATC	No	0139-720	10139	7200	Ye		Yes	OK
39 40	Validation Validation		20	Rotterdam Road Rotterdam Road	NEB SWB	Jul-15 Jul-15	ATC ATC	No No	7210-9130 9130-7210	7210 9130	9130 7210	Ye: Ye:		Yes	OK OK
41	Calibration		21	Peto Way	NB	Jul-15	ATC	No	0190-706	10190	7060	Ye		Yes	OK
42	Calibration		21	Peto Way	SB	Jul-15	ATC	No	060-1019	7060	10190	Ye		Yes	
43 44	Calibration Calibration		22	A1117 Normanston Drive A1117 Normanston Drive	NEB SWB	Jul-15 Jul-15	ATC ATC	No No	7050-7060 7060-7050	7050 7060	7060 7050	Ye: Ye:		Yes	OK OK
45	Calibration		23	A1144 Normanston Drive	EB	Jul-15	ATC	No	240-9130	9240	9130	Ye		Yes	OK
46	Calibration		23	A1144 Normanston Drive	WB	Jul-15	ATC	No	130-9240	9130	9240	Ye		Yes	OK
47 48	Calibration Calibration		24	Oulton Road Oulton Road	EB WB	Jul-15 Jul-15	ATC ATC	No No	270-1001 0010-927	9270 10010	10010 9270	Ye: Ye:		Yes	OK OK
49	Calibration		25	B1375 Gorleston Road	NB	Jul-15	ATC	No	3030-8040	8030	8040	Ye		Yes	OK
50	Calibration		25	B1375 Gorleston Road	SB	Jul-15	ATC	No	3040-8030	8040	8030	Ye	Yes	Yes	OK
51 52	Calibration Calibration		26 26	A1117 Millennium Way A1117 Millennium Way	NB SB	Jul-15 Jul-15	ATC ATC	No No	7070-7080 7080-7070	7070 7080	7080 7070	Ye: Ye:		Yes	OK OK
53	Calibration		27	A12 Yarmouth Road	NWB	Jul-15	ATC	No	030-7070	10242	10248	Ye		Yes	OK
54	Calibration		27	A12 Yarmouth Road	SEB	Jul-15	ATC	No	)248-1024	10248	10242	Ye	Yes	Yes	OK
55 56	Calibration		28	B1385 Corton Road B1385 Corton Road	NB SB	Jul-15	ATC ATC	No No	9460-9480 9480-9460	9460 9480	9480 9460	Ye		Yes	OK
57	Calibration Calibration		29	A12 Yarmouth Road	NB	Jul-15 Jul-15	ATC	No	0257-625	10257	6250	Ye: Ye:		Yes	
58	Calibration		29	A12 Yarmouth Road	SB	Jul-15	ATC	No	250-1025	6250	10257	Ye	Yes	Yes	OK
59 60	Calibration Calibration		30	B1375 Parkhill B1375 Parkhill	NB SB	Jul-15 Jul-15	ATC ATC	No No	0001-807 070-1000	10001 8070	8070 10001	Ye: Ye:		Yes	OK OK
61	Calibration		31	B1074 Bluderston Road	NB	Jul-15 Jul-15	ATC	No	070-1000	10025	20026	Ye		Yes	OK
62	Calibration		31	B1074 Bluderston Road	SB	Jul-15	ATC	No	0026-1002	20026	10025	Ye	Yes	Yes	OK
63	Calibration Calibration		32	Fixton Road	NB SB	Jul-15	ATC ATC	No	440-1002 0024-944	9440 10024	10024 9440	Ye		Yes	OK OK
64 65	Validation		33	Fixton Road Coast Road	NB	Jul-15 Jul-15	ATC	No No	510-1002	9510	10027	Ye: Ye:		Yes	OK
66	Validation		33	Coast Road	SB	Jul-15	ATC	No	0027-951	10027	9510	Ye	Yes	Yes	OK
67	Validation		6/605	Katwijk Way	NB NB	Jul-13	TRADS ANPR	No No	7280-6060	7280	6060	Ye		Yes	OK
75 76	Calibration Calibration		3	A12YarmouthRd A12YarmouthRd	SB	Jul-15 Jul-15	ANPR	No No	3280-4520 1520-6280	6280 4520	4520 6280	Ye: Ye:		Yes	OK OK
79	Validation		5	A12 Pier Terrace	NB	Jul-15	ANPR	No	260-1002	1260	10023	Ye	Yes	Yes	OK
80 81	Validation Validation		5	A12 Pier Terrace Saltwater Way	SB NB	Jul-15 Jul-15	ANPR ANPR	No No	0023-126 2050-2060	10023 2050	1260 2060	Ye: Ye:		Yes	OK OK
82	Validation		6	Saltwater Way Saltwater Way	SB	Jul-15 Jul-15	ANPR	No	2060-2060	2060	2050	Ye		Yes	OK
99	Validation		15	North Quay Retail Park	Entry	Jul-15	ANPR	No	220-9230	9220	9230	Ye	Yes	Yes	OK
100	Validation Validation		15 16	North Quay Retail Park Links Road Car Park	Exit EB	Jul-15 Jul-15	ANPR ANPR	No No	9230-9220	9230	9220	Ye: Ye:		Yes	OK OK
101	Validation		16	Links Road Car Park Links Road Car Park	WB	Jul-15 Jul-15	ANPR	No	9602-9603 9603-9602	9602 9603	9603 9602	Ye	Yes	Yes	OK
103	Validation		17	Swimming Pool Road Car Park	EB	Jul-15	ANPR	No	090-1025	9090	10251	Ye	Yes	Yes	OK
104	Validation		17	Swimming Pool Road Car Park Battery Green Road Car Park	WB Exit	Jul-15	ANPR	No No	0251-909	10251	9090	Ye		Yes	OK
106 107	Validation Validation		18 19	Battery Green Road Car Park Gordon Road Car Park Entry	Entry	Jul-15 Jul-15	ANPR ANPR	No No	)127-1012 3140-9050	10127 6140	10126 9050	Ye: Ye:		Yes	OK OK
109	Validation		20	Surrey Street Car Park Entry	Entry	Jul-15	ANPR	No	)130-1013	10130	10131	Ye	Yes	Yes	OK
112	Validation		21	Clapham Road Car Park Exit	Exit	Jul-15	ANPR	No	0132-1013	10132	10133	Ye		Yes	
113 114	Validation Validation		22	Clapham Road South Clapham Road South	Entry Exit	Jul-15 Jul-15	ANPR ANPR	No No	)137-1013 )138-1013	10137 10138	10138 10137	Ye: Ye:		Yes	OK OK
115	Validation		23	St Johns Road Car Park	Entry	Jul-15	ANPR	No	0083-1008	10083	10084	Ye		Yes	OK
116	Validation		23	St Johns Road Car Park	Exit	Jul-15	ANPR	No	000 1025	10084	10083	Ye		Yes	
117 118	Validation Validation		24a 24a	Kirkley Rise Car Park Kirkley Rise Car Park	Entry	Jul-15 Jul-15	ANPR ANPR	No No	000-1025 0256-400	4000 10256	10256 4000	Ye: Ye:		Yes	OK OK
119	Validation		24b	Kirkley Rise Car Park	Entry	Jul-15	ANPR	No	300-1007	5300	10078	Ye		Yes	OK
120	Validation		24b	Kirkley Rise Car Park	Exit	Jul-15	ANPR	No	0078-530	10078	5300	Ye	Yes	Yes	OK
121 122	Validation Validation		25 25	Kirkley Cliff Road Car Park Kirkley Cliff Road Car Park	Entry Exit	Jul-15 Jul-15	ANPR ANPR	No No	120-1007 0075-112	1120 10075	10075 1120	Ye: Ye:		Yes	
125	Validation Validation		25	Marine Parade	Entry	Jul-15 Jul-15	ANPR	No	0075-112	10075	10082	Ye		Yes	
126	Validation		27	Marine Parade	Exit	Jul-15	ANPR	No	0082-1008	10082	10081	Ye	Yes	Yes	OK
127	Validation Validation		28 28	Asda Car Park Asda Car Park	Entry	Jul-15	ANPR	No No	000-1008 0085-400	4000	10085	Ye		Yes	OK
128			40	ASUA CAI PAIK	Exit	Jul-15	ANPR	No	vvov-400	10085	4000	Ye	Yes	Yes	OK

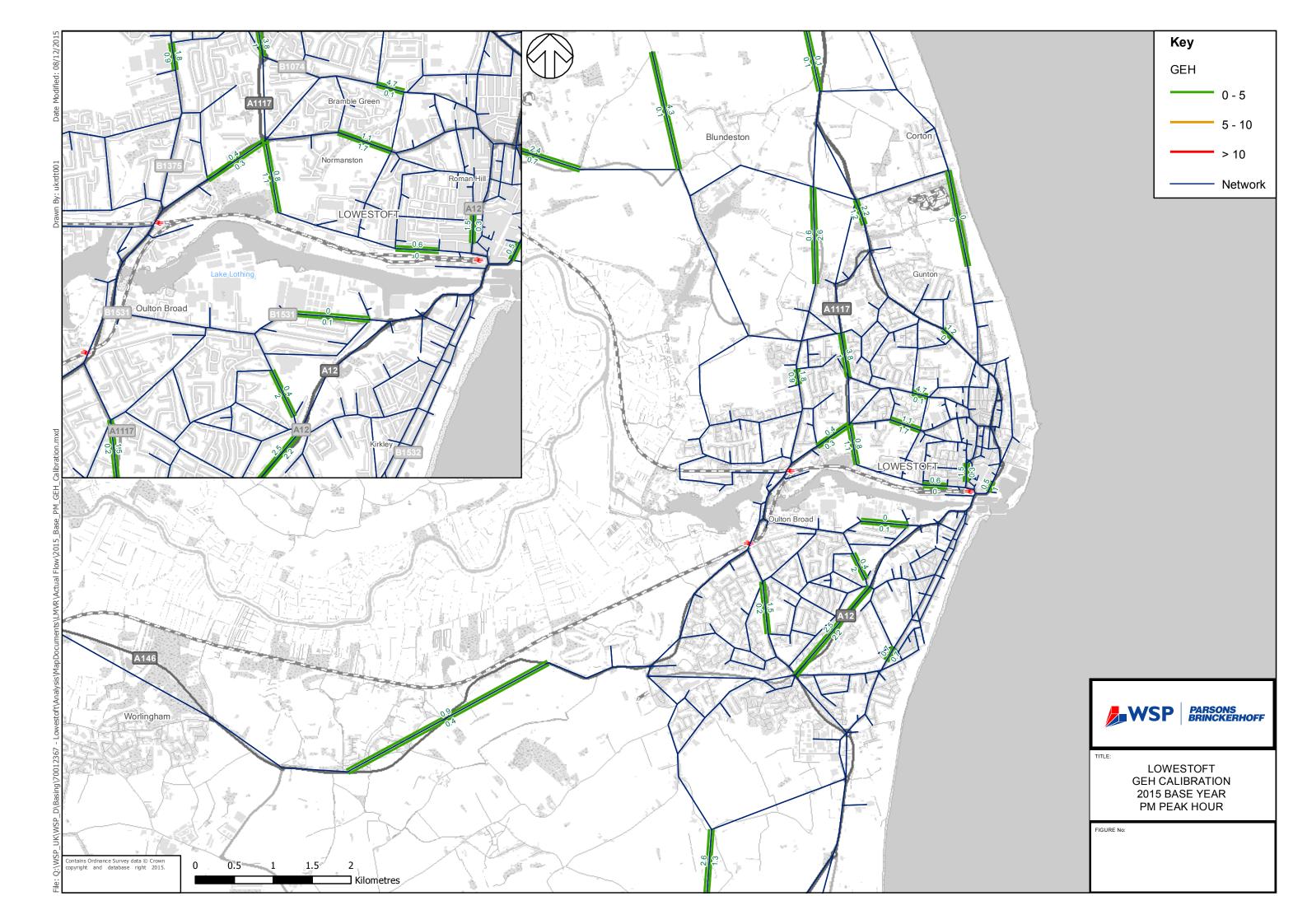
	Interpeak ALL VEHICLES CAR LGV HGV												HGV					
Observed	Modelled	GEH		Flow Pass?	Observed	Modelled	GEH	GEH Pass?	Flow Pass?	Observed	Modelled	GEH	Observed	Modelled	GEH			
20	10	2.521	Yes	Yes	7	6	0.536	Yes	Yes	11	3	3.118	1	1	0.021			
22	24	0.318	Yes	Yes	10	10	0.063	Yes	Yes	12	12	0.109	1	2	0.021			
589	617	1.147	Yes	Yes	227	254	1.752	Yes	Yes	316	316	0.028	47	47	0.073			
588	588 369	0.014 3.412	Yes	Yes	161 161	162 189	0.066 2.131	Yes	Yes	378 123	378 152	0.009 2.514	48 23	48 28	0.048			
306 322	297	1.430	Yes Yes	Yes Yes	158	102	4.941	Yes Yes	Yes Yes	137	168	2.469	26	27	0.999			
642	615	1.096	Yes	Yes	313	355	2.322	Yes	Yes	292	237	3.355	38	23	2.775			
664	615	1.926	Yes	Yes	375	363	0.610	Yes	Yes	249	235	0.922	40	17	4.252			
385 408	367 411	0.937 0.147	Yes Yes	Yes Yes	207 203	198 205	0.662 0.167	Yes Yes	Yes Yes	158 184	151 185	0.589 0.050	19 21	18 21	0.330			
490	535	2.010	Yes	Yes	353	391	1.957	Yes	Yes	114	121	0.609	22	23	0.241			
492	499	0.332	Yes	Yes	326	325	0.076	Yes	Yes	141	150	0.706	24	24	0.045			
382 405	389 395	0.338 0.481	Yes Yes	Yes Yes	211 235	218 235	0.490 0.028	Yes Yes	Yes Yes	153 153	153 143	0.038 0.792	18 17	18 17	0.016			
417	301	6.104	No	No	224	131	6.982	No	Yes	172	153	1.519	20	17	0.745			
399	316	4.391	Yes	Yes	258	116	10.393	No	No	124	179	4.425	16	21	1.065			
132	136	0.315	Yes	Yes	90	93	0.281	Yes	Yes	38	39	0.087	4	4	0.216			
109 258	106 262	0.329 0.264	Yes Yes	Yes Yes	75 151	73 156	0.211 0.367	Yes Yes	Yes Yes	31 97	30 97	0.186 0.001	9	3 9	0.320			
266	264	0.111	Yes	Yes	134	135	0.124	Yes	Yes	122	119	0.296	10	10	0.000			
323	297	1.465	Yes	Yes	193	181	0.849	Yes	Yes	106	101	0.525	24	15	2.005			
204	198	0.454 0.092	Yes	Yes	138	147	0.732	Yes	Yes	49	49	0.012	17	2	4.920			
465 610	467 583	1.098	Yes Yes	Yes Yes	202 355	204 318	0.118 2.024	Yes Yes	Yes Yes	238 229	238 239	0.019 0.682	25 26	25 26	0.002			
440	436	0.185	Yes	Yes	325	215	6.668	No	No	88	201	9.396	27	20	1.506			
474	597	5.335	No	No	336	354	0.969	Yes	Yes	115	223	8.336	23	20	0.624			
646 446	364 206	12.533 13.274	No No	No No	274 299	269 154	0.311 9.645	Yes No	Yes No	344 121	90 46	17.243 8.242	27 25	5 6	5.571 4.828			
237	244	0.456	Yes	Yes	153	158	0.420	Yes	Yes	78	79	0.165	7	7	0.142			
338	345	0.367	Yes	Yes	228	232	0.253	Yes	Yes	99	102	0.278	11	11	0.047			
146	110	3.165	Yes	Yes	87	76	1.234	Yes	Yes	54	32	3.392	4	4	1.328			
140 445	124 449	1.398 0.178	Yes Yes	Yes Yes	88 303	84 306	0.405 0.182	Yes Yes	Yes Yes	50 133	36 133	2.069 0.031	3 10	10	0.661			
550	553	0.146	Yes	Yes	300	305	0.274	Yes	Yes	237	236	0.065	12	12	0.099			
641	678	1.458	Yes	Yes	323	358	1.908	Yes	Yes	297	299	0.089	20	21	0.154			
650	645	0.199	Yes	Yes	356	363	0.346	Yes	Yes	270	258	0.724	24	24 12	0.027			
281 275	298 275	0.975 0.004	Yes Yes	Yes Yes	160 180	176 177	1.260 0.252	Yes Yes	Yes Yes	110 83	110 87	0.005 0.390	12 11	11	0.064			
325	266	3.421	Yes	Yes	182	171	0.812	Yes	Yes	134	86	4.563	9	9	0.053			
270	253	1.058	Yes	Yes	164	161	0.210	Yes	Yes	99	84	1.557	8	8	0.164			
445 473	415 462	1.457 0.489	Yes Yes	Yes Yes	336 367	306 357	1.648 0.523	Yes Yes	Yes Yes	92 89	92 89	0.011 0.029	18 16	17 16	0.142			
438	472	1.575	Yes	Yes	348	378	1.564	Yes	Yes	75	81	0.656	15	13	0.528			
392	445	2.597	Yes	Yes	326	356	1.615	Yes	Yes	51	74	2.942	15	15	0.017			
508	508	0.002	Yes	Yes	318	318	0.017	Yes	Yes	168	168	0.004	22	22	0.039			
510 88	481 87	1.309 0.074	Yes Yes	Yes Yes	299 73	270 73	1.717 0.019	Yes Yes	Yes Yes	185 13	185 12	0.035 0.161	26 2	26 2	0.062			
99	99	0.038	Yes	Yes	80	80	0.012	Yes	Yes	17	17	0.086	2	2	0.090			
495	489	0.276	Yes	Yes	389	389	0.018	Yes	Yes	80	74	0.639	26	26	0.031			
542	502 234	1.750 1.869	Yes	Yes Yes	370 210	331 181	2.077 2.101	Yes Yes	Yes Yes	144 42	143 42	0.079 0.001	28 11	28 11	0.030			
263 193	186	0.532	Yes Yes	Yes	140	133	0.604	Yes	Yes	42	42	0.001	7	7	0.023			
116	116	0.031	Yes	Yes	73	73	0.015	Yes	Yes	39	39	0.037	4	4	0.213			
101	107	0.570	Yes	Yes	11	18	1.711	Yes	Yes	82	82	0.016	8	7	0.224			
49 71	50 73	0.131 0.209	Yes Yes	Yes Yes	7	7	0.105 0.060	Yes Yes	Yes Yes	40 63	40 63	0.063 0.023	3 4	3 6	0.150 0.819			
63	68	0.681	Yes	Yes	7	49	7.867	No	Yes	53	18	5.853	2	1	1.071			
60	86	3.059	Yes	Yes	14	60	7.464	No	Yes	43	25	3.081	2	1	1.109			
411	207	11.581	No	No	383	166	13.081	No	No	17	36	3.729	11	5	2.121			
860 864	861 838	0.045 0.891	Yes Yes	Yes Yes	704 711	704 685	0.013 0.984	Yes Yes	Yes Yes	119 118	120 118	0.076 0.031	37 35	37 35	0.027 0.056			
1041	955	2.722	Yes	Yes	453	570	5.177	No	No	532	346	8.883	56	39	2.459			
1051	1090	1.182	Yes	Yes	612	687	2.932	Yes	Yes	394	352	2.178	45	51	0.867			
983 931	957 974	0.845 1.410	Yes Yes	Yes Yes	718 575	526 577	7.686 0.079	No Yes	No Yes	228 329	391 357	9.284 1.525	38 27	40 40	0.329 2.318			
405	474	3.308	Yes	Yes	376	296	4.381	Yes	Yes	27	178	14.870	1	0	1.414			
402	372	1.542	Yes	Yes	373	283	4.987	Yes	Yes	28	88	7.851	1	1	0.174			
10	0	4.435 4.397	Yes	Yes	10	0	4.359 4.282	Yes	Yes	0	0	0.816	0	0	0.000			
10 0	0	0.000	Yes Yes	Yes Yes	9	0	0.000	Yes Yes	Yes Yes	0	0	1.000 0.000	0	0	0.000			
0	0	0.000	Yes	Yes	0	0	0.000	Yes	Yes	0	0	0.000	0	0	0.000			
37	30	1.182	Yes	Yes	36	29	1.283	Yes	Yes	1	1	0.577	0	0	0.000			
46 62	33 49	2.044 1.682	Yes Yes	Yes Yes	45 60	31 49	2.247 1.533	Yes Yes	Yes Yes	1	0	0.816 1.528	0	0	0.000			
66	55	1.435	Yes	Yes	65	52	1.700	Yes	Yes	1	3	1.270	0	0	0.000			
105	126	1.970	Yes	Yes	102	106	0.359	Yes	Yes	3	17	4.644	0	3	2.449			
109	124	1.406	Yes	Yes	106	113	0.637	Yes	Yes	3	9	2.711	0	2	2.000			
6	9	1.163 1.807	Yes Yes	Yes Yes	4	9	2.119 0.990	Yes Yes	Yes Yes	1	0	1.732 1.633	1	0	1.155 1.000			
10	2	3.311	Yes	Yes	9	2	3.081	Yes	Yes	1	0	1.155	0	0	0.577			
11	1	4.161	Yes	Yes	11	1	3.962	Yes	Yes	1	0	1.155	0	0	0.577			
4	7	1.279 2.517	Yes	Yes	3	7	1.443 2.380	Yes	Yes	0	0	0.816 0.816	0	0	0.000			
3 2	2	0.246	Yes Yes	Yes Yes	2	1	0.447	Yes Yes	Yes Yes	0	1	1.091	0	0	0.000			
2	2	0.246	Yes	Yes	2	1	0.447	Yes	Yes	0	1	1.091	0	0	0.000			
41	42	0.155	Yes	Yes	38	39	0.188	Yes	Yes	3	3	0.198	1	0	1.000			
39 354	26 362	2.201 0.441	Yes Yes	Yes Yes	36 336	26 347	1.713 0.577	Yes Yes	Yes Yes	3 16	0 14	2.236 0.558	1	1	1.000 0.160			
	302	0.441	Yes	Yes	340	318	1.195	Yes	Yes	15	32	3.426	1	1	0.160			

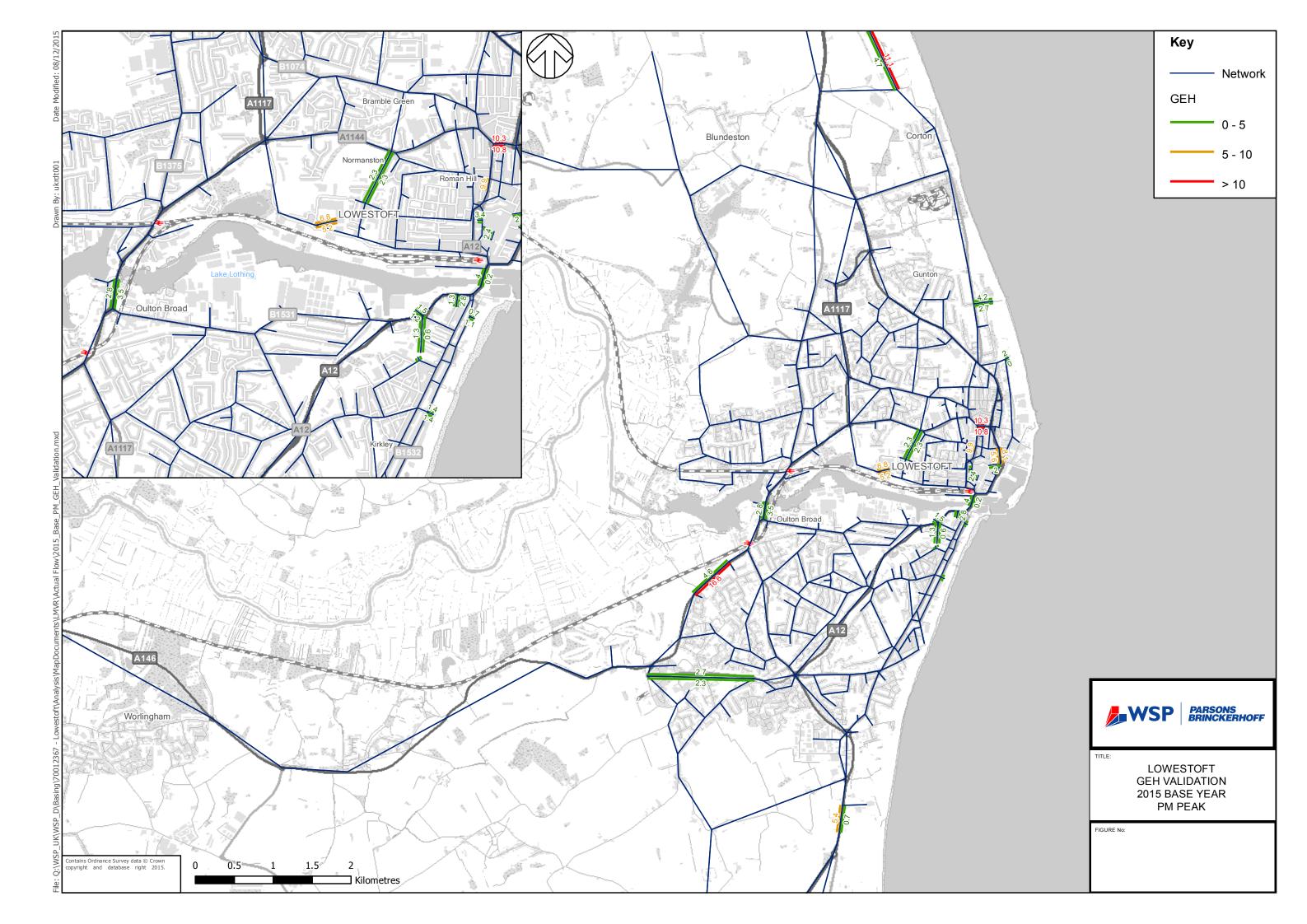




	Calibration / Validation	Area	ID	Site Location	Dir	Date	Data Type	Duplicate?	Ref	A-Node	B-Node	Factor	AM Poak	Interp eak	PM Peak	Check
5	Calibration		3	Gisleham Road	NB	Jul-15	ATC	No	9600-5010	9600	5010		Yes	Yes	Yes	OK
6	Calibration		3	Gisleham Road	SB	Jul-15	ATC	No	5010-9600	5010	9600		Yes	Yes	Yes	OK
7	Calibration		4	A146 Beccles Road A146 Beccles Road	EB WB	Jul-15 Jul-15	ATC ATC	No No	1514-4513 1513-4514	4514 4513	4513 4514		Yes	Yes	Yes	OK OK
9	Calibration Validation		5	A146 Beccles Road A1145 Castleton Avenue	EB	Jul-15 Jul-15	ATC	No	5110-5060	5110	5060		Yes	Yes Yes	Yes Yes	OK
10	Validation		5	A1145 Castleton Avenue	WB	Jul-15	ATC	No	5060-5110	5060	5110		Yes	Yes	Yes	OK
11 12	Validation Validation		6	A12 London Road A12 London Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	5390-1000 1000-5390	5390 1000	1000 5390		Yes	Yes	Yes Yes	OK OK
13	Calibration		7	London Road South	NEB	Jul-15 Jul-15	ATC	No	9606-1040	9606	1040		Yes	Yes	Yes	OK
14	Calibration		7	London Road South	SWB	Jul-15	ATC	No	1040-9606	1040	9606		Yes	Yes	Yes	OK
15	Calibration		8	A12 Tom Crisp Way A12 Tom Crisp Way	NEB	Jul-15	ATC ATC	No	000-1001	3000	10015		Yes	Yes	Yes	OK
16 17	Calibration Calibration		8	A12 Tom Crisp Way A1117 Elm Tree Road	SWB NB	Jul-15 Jul-15	ATC	No No	0015-300 3030-3040	10015 3030	3000 3040		Yes	Yes	Yes Yes	OK OK
18	Calibration		9	A1117 Elm Tree Road	SB	Jul-15	ATC	No	3040-3030	3040	3030		Yes	Yes	Yes	OK
19 20	Validation Validation		10	A146 Beccles Road	NEB SWB	Jul-15 Jul-15	ATC ATC	No No	0111-1010 0109-1011	10111	10109		Yes	Yes	Yes	OK OK
21	Calibration		11	A146 Beccles Road Kirkley Run	NWB	Jul-15	ATC	No	0103-101	10103	5270		Yes	Yes Yes	Yes	OK
22	Calibration		11	Kirkley Run	SEB	Jul-15	ATC	No	270-1010	5270	10103		Yes	Yes	Yes	OK
23	Calibration Calibration		12	A146 Waveney Drive A146 Waveney Drive	EB WB	Jul-15 Jul-15	ATC ATC	No No	0088-401 010-1008	10088 4010	4010 10088		Yes	Yes	Yes	OK OK
29	Calibration		15	Katwijk Way	NB	Jul-15	ATC	No	040-1008	6040	10136		Yes	Yes	Yes	OK
30	Calibration		15	Katwijk Way	SB	Jul-15	ATC	No	0136-604	10136	6040		Yes	Yes	Yes	OK
31	Calibration		16	A12 Battery Green Road	NB	Jul-15	ATC	No.	3160-6150	6160	6150		Yes	Yes	Yes	OK
32	Calibration Validation		16 17	A12 Battery Green Road A12 Old Nelson Street	SB NB	Jul-15 Jul-15	ATC ATC	No No	6150-6160 6140-6130	6150 6140	6160 6130		Yes	Yes Yes	Yes Yes	OK OK
34	Validation		17	A12 Old Nelson Street	SB	Jul-15	ATC	No	3130-6140	6130	6140		Yes	Yes	Yes	OK
35	Validation Validation		18 18	St Peter's Street St Peter's Street	EB WB	Jul-15 Jul-15	ATC ATC	No No	6070-6079 6075-6070	6070 6075	6075 6070		Yes	Yes	Yes	OK OK
36 37	Calibration		19	St Peter's Street  Denmark Road	EB	Jul-15 Jul-15	ATC	No	200-1013	7200	10139		Yes	Yes Yes	Yes Yes	OK
38	Calibration		19	Denmark Road	WB	Jul-15	ATC	No	0139-720	10139	7200		Yes	Yes	Yes	OK
39 40	Validation		20	Rotterdam Road Rotterdam Road	NEB SWB	Jul-15	ATC ATC	No	7210-9130 9130-7210	7210 9130	9130 7210		Yes	Yes	Yes	OK
41	Validation Calibration		21	Peto Way	NB	Jul-15 Jul-15	ATC	No No	0190-7210	10190	7060		Yes	Yes	Yes Yes	OK OK
42	Calibration		21	Peto Way	SB	Jul-15	ATC	No	060-1019	7060	10190		Yes	Yes	Yes	OK
43 44	Calibration Calibration		22	A1117 Normanston Drive	NEB	Jul-15	ATC	No No	7050-7060	7050	7060		Yes	Yes	Yes	OK
45	Calibration		23	A1117 Normanston Drive A1144 Normanston Drive	SWB	Jul-15 Jul-15	ATC ATC	No No	7060-7050 9240-9130	7060 9240	7050 9130		Yes	Yes Yes	Yes Yes	OK OK
46	Calibration		23	A1144 Normanston Drive	WB	Jul-15	ATC	No	9130-9240	9130	9240		Yes	Yes	Yes	OK
47 48	Calibration		24	Oulton Road Oulton Road	EB WB	Jul-15 Jul-15	ATC ATC	No No	270-1001 0010-927	9270	10010 9270		Yes	Yes	Yes	OK
49	Calibration Calibration		24 25	B1375 Gorleston Road	NB	Jul-15 Jul-15	ATC	No	3030-8040	10010 8030	8040		Yes	Yes Yes	Yes Yes	OK OK
50	Calibration		25	B1375 Gorleston Road	SB	Jul-15	ATC	No	3040-8030	8040	8030		Yes	Yes	Yes	OK
51	Calibration		26	A1117 Millennium Way	NB	Jul-15	ATC	No	7070-7080	7070	7080		Yes	Yes	Yes	OK
52 53	Calibration Calibration		26 27	A1117 Millennium Way A12 Yarmouth Road	SB NWB	Jul-15 Jul-15	ATC ATC	No No	7080-7070 0242-1024	7080 10242	7070 10248		Yes	Yes	Yes Yes	OK OK
54	Calibration		27	A12 Yarmouth Road	SEB	Jul-15	ATC	No	0248-1024	10248	10242		Yes	Yes	Yes	OK
55 56	Calibration Calibration		28 28	B1385 Corton Road B1385 Corton Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	9460-9480 9480-9460	9460 9480	9480 9460		Yes	Yes Yes	Yes	OK OK
57	Calibration		29	A12 Yarmouth Road	NB	Jul-15	ATC	No	0257-625	10257	6250		Yes	Yes	Yes	OK
58	Calibration		29	A12 Yarmouth Road	SB	Jul-15	ATC	No	250-1025	6250	10257		Yes	Yes	Yes	OK
59 60	Calibration		30	B1375 Parkhill B1375 Parkhill	NB SB	Jul-15 Jul-15	ATC ATC	No No	0001-807 070-1000	10001 8070	8070 10001		Yes	Yes Yes	Yes Yes	OK OK
61	Calibration Calibration		31	B1073 Faikhiii B1074 Bluderston Road	NB	Jul-15	ATC	No	070-1000	10025	20026		Yes	Yes	Yes	OK
62	Calibration		31	B1074 Bluderston Road	SB	Jul-15	ATC	No	0026-1002	20026	10025		Yes	Yes	Yes	OK
63 64	Calibration Calibration		32	Fixton Road Fixton Road	NB SB	Jul-15 Jul-15	ATC ATC	No No	440-1002 0024-944	9440 10024	10024 9440		Yes	Yes Yes	Yes Yes	OK OK
65	Validation		33	Coast Road	NB	Jul-15	ATC	No	510-1002	9510	10027		Yes	Yes	Yes	OK
66	Validation		33	Coast Road	SB	Jul-15	ATC	No	0027-951	10027	9510		Yes	Yes	Yes	OK
67 75	Validation Calibration	06	3	Katwijk Way A12YarmouthRd	NB NB	Jul-13 Jul-15	TRADS ANPR	No No	7280-6060 5280-4520	7280 6280	6060 4520		Yes	Yes Yes	Yes Yes	OK OK
76	Calibration		3	A12YarmouthRd	SB	Jul-15	ANPR	No	1520-6280	4520	6280		Yes	Yes	Yes	OK
79	Validation		5	A12 Pier Terrace	NB	Jul-15	ANPR	No	260-1002	1260	10023		Yes	Yes	Yes	OK
80 81	Validation Validation		5 6	A12 Pier Terrace Saltwater Way	SB NB	Jul-15 Jul-15	ANPR ANPR	No No	0023-126 2050-2060	10023 2050	1260 2060		Yes	Yes	Yes Yes	OK OK
82	Validation		6	Saltwater Way	SB	Jul-15	ANPR	No	2060-2050	2060	2050		Yes	Yes	Yes	OK
99	Validation		15	North Quay Retail Park	Entry	Jul-15	ANPR	No	9220-9230	9220	9230		Yes	Yes	Yes	OK
100	Validation Validation		15 16	North Quay Retail Park Links Road Car Park	Exit EB	Jul-15 Jul-15	ANPR ANPR	No No	9230-9220 9602-9603	9230 9602	9220 9603		Yes	Yes	Yes	OK OK
102	Validation		16	Links Road Car Park	WB	Jul-15	ANPR	No	9603-9602	9603	9602		Yes	Yes	Yes	OK
103	Validation		17	Swimming Pool Road Car Park	EB WB	Jul-15	ANPR	No	090-1025	9090	10251		Yes	Yes	Yes	OK
104 106	Validation Validation		17 18	Swimming Pool Road Car Park Battery Green Road Car Park	Exit	Jul-15 Jul-15	ANPR ANPR	No No	0251-909 0127-1012	10251 10127	9090 10126		Yes	Yes Yes	Yes Yes	OK OK
107	Validation		19	Gordon Road Car Park Entry	Entry	Jul-15	ANPR	No	3140-9050	6140	9050		Yes	Yes	Yes	OK
109	Validation Validation		20	Surrey Street Car Park Entry	Entry	Jul-15	ANPR ANPR	No No	0130-1013	10130	10131		Yes	Yes	Yes	OK
112 113	Validation		21	Clapham Road Car Park Exit Clapham Road South	Exit	Jul-15 Jul-15	ANPR	No No	0132-1011 0137-1011	10132 10137	10133		Yes	Yes	Yes	OK OK
114	Validation		22	Clapham Road South	Exit	Jul-15	ANPR	No	0138-1013	10138	10137		Yes	Yes	Yes	OK
115	Validation		23	St Johns Road Car Park	Entry	Jul-15	ANPR ANPR	No No	0083-1008	10083 10084	10084		Yes	Yes	Yes	OK
116 117	Validation Validation		23 24a	St Johns Road Car Park Kirkley Rise Car Park	Exit	Jul-15 Jul-15	ANPR	No No	0084-1008 000-1025	4000	10083 10256		Yes	Yes	Yes	OK OK
118	Validation		24a	Kirkley Rise Car Park	Exit	Jul-15	ANPR	No	0256-400	10256	4000		Yes	Yes	Yes	OK
119	Validation		24b	Kirkley Rise Car Park	Entry	Jul-15	ANPR	No	300-1007	5300	10078		Yes	Yes	Yes	OK
120 121	Validation Validation		24b 25	Kirkley Rise Car Park Kirkley Cliff Road Car Park	Exit Entry	Jul-15 Jul-15	ANPR ANPR	No No	0078-530 120-1007	10078 1120	5300 10075		Yes	Yes Yes	Yes Yes	OK OK
122	Validation		25	Kirkley Cliff Road Car Park	Exit	Jul-15	ANPR	No	0075-112	10075	1120		Yes	Yes	Yes	OK
405	Validation		27 27	Marine Parade Marine Parade	Entry	Jul-15	ANPR	No	0081-1008	10081	10082		Yes	Yes	Yes	OK
125					Exit	Jul-15	ANPR	No	0082-1008	10082	10081		Yes	Yes	Yes	OK
126 127	Validation Validation		28	Asda Car Park	Entry	Jul-15	ANPR	No	000-1008	4000	10085		Yes	Yes	Yes	OK

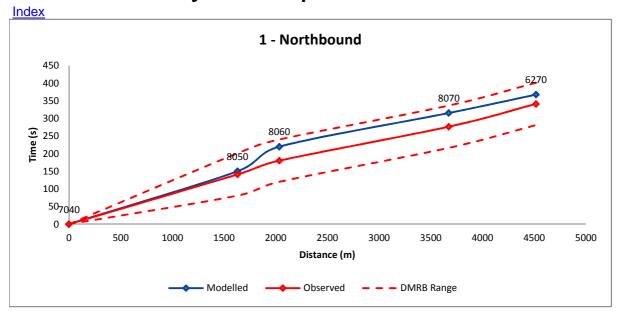
								Peak							
		ALL VEHICLES	S				CAR				LGV			HGV	
Observed	Modelled	GEH	GEH Pass?	Flow Pass?	Observed	Modelled	GEH	GEH Pass?	Flow Pass?	Observed	Modelled	GEH	Observed	Modelled	GEH
42	27	2.594	Yes	Yes	16	12	1.019	Yes	Yes	26	15	2.417	1	0	1.033
26	20	1.342	Yes	Yes	12	12	0.115	Yes	Yes	13	7	1.933	1 25	1	0.068
896 664	924 653	0.928 0.429	Yes Yes	Yes Yes	383 193	405 182	1.134 0.803	Yes Yes	Yes Yes	489 448	494 448	0.248	25 24	25 23	0.000
460	519	2.690	Yes	Yes	275	279	0.240	Yes	Yes	172	229	3.997	12	11	0.331
448	497	2.278	Yes	Yes	255	196	3.921	Yes	Yes	180	283	6.751	12	18	1.443
759 775	617 794	5.403 0.683	No Yes	No Yes	375 460	351 512	1.282 2.365	Yes Yes	Yes Yes	357 294	256 272	5.784 1.316	26 21	10 10	3.771 2.764
520	504	0.718	Yes	Yes	287	275	0.686	Yes	Yes	218	213	0.315	16	16	0.031
499	483	0.728	Yes	Yes	270	258	0.708	Yes	Yes	221	216	0.347	9	9	0.169
502 708	559 768	2.475 2.227	Yes Yes	Yes Yes	383 520	431 540	2.371 0.891	Yes Yes	Yes Yes	111 174	120 211	0.885 2.667	8 14	8 17	0.117 0.762
421	417	0.177	Yes	Yes	254	246	0.490	Yes	Yes	159	164	0.364	8	7	0.186
417	448	1.485	Yes	Yes	256	278	1.323	Yes	Yes	152	161	0.750	9	9	0.042
535 491	434 186	4.599 16.562	Yes No	No No	312 332	193 67	7.489 18.774	No No	No No	213 148	228 112	1.044 3.168	11 10	13 7	0.653 1.107
219	190	2.028	Yes	Yes	155	153	0.141	Yes	Yes	62	35	3.877	2	2	0.171
183	178	0.372	Yes	Yes	132	131	0.065	Yes	Yes	49	45	0.619	2	2	0.000
221 431	221 433	0.000 0.112	Yes Yes	Yes Yes	140 233	142 235	0.159 0.160	Yes Yes	Yes Yes	75 189	79 189	0.430	6 10	9	3.367 0.182
307	282	1.476	Yes	Yes	186	180	0.407	Yes	Yes	101	93	0.762	21	9	3.167
225	221	0.268	Yes	Yes	165	212	3.410	Yes	Yes	46	8	7.292	14	1	4.747
457	467	0.479	Yes	Yes	241	246	0.348	Yes	Yes	206	211	0.326	10	10	0.045
911 630	881 498	1.006 5.558	Yes No	Yes No	581 502	550 275	1.293 11.533	Yes No	Yes No	309 104	308 211	0.036 8.538	22 24	23 12	0.264 2.779
577	788	8.082	No	No	449	553	4.635	Yes	No	114	221	8.245	13	14	0.169
624	391	10.348	No No	No No	289	348	3.328	Yes	Yes	324	41	20.960	11	2	3.594
510 261	294 252	10.757 0.554	No Yes	No Yes	365 182	225 180	8.138 0.112	No Yes	No Yes	127 77	62 69	6.644 0.879	18 3	7	3.193 0.073
406	406	0.012	Yes	Yes	290	304	0.805	Yes	Yes	107	95	1.230	8	7	0.453
151	124	2.262	Yes	Yes	97	95	0.217	Yes	Yes	52	28	3.744	2	1	0.640
146 423	120 401	2.275 1.078	Yes Yes	Yes Yes	101 295	82 294	1.937 0.044	Yes Yes	Yes Yes	45 120	36 100	1.396 1.896	1 8	7	0.938 0.453
609	588	0.848	Yes	Yes	335	320	0.802	Yes	Yes	264	258	0.394	10	10	0.040
608	598	0.399	Yes	Yes	297	297	0.023	Yes	Yes	298	289	0.537	12	12	0.057
648 238	641 222	0.291 1.055	Yes Yes	Yes Yes	371 142	361 161	0.502 1.565	Yes Yes	Yes Yes	266 90	272 56	0.366 3.979	12 6	8 5	1.208 0.527
323	292	1.740	Yes	Yes	211	200	0.785	Yes	Yes	102	86	1.675	9	6	1.095
371	286	4.664	Yes	Yes	205	184	1.532	Yes	Yes	160	96	5.618	6	6	0.156
353	355	0.100	Yes	Yes	220	221 410	0.076 0.941	Yes	Yes	126	127	0.089	7 8	7	0.094 0.050
543 702	523 655	0.860 1.804	Yes Yes	Yes Yes	429 570	561	0.384	Yes Yes	Yes Yes	105 119	105 81	3.800	13	8 13	0.030
545	569	1.012	Yes	Yes	443	468	1.154	Yes	Yes	89	89	0.000	13	12	0.213
510	601	3.850	Yes	Yes	448	473 471	1.189	Yes	Yes	55 215	120	6.901	7 15	8	0.225
702 601	702 572	0.009 1.197	Yes Yes	Yes Yes	472 380	358	0.029 1.132	Yes Yes	Yes Yes	206	215 199	0.026 0.518	15	16 15	0.319 0.032
104	104	0.025	Yes	Yes	88	89	0.066	Yes	Yes	14	14	0.033	1	1	0.236
93	93	0.013	Yes	Yes	77	77	0.014	Yes	Yes	16	16	0.094	0	0	0.866
656 730	687 672	1.180 2.180	Yes Yes	Yes Yes	561 530	574 479	0.564 2.271	Yes Yes	Yes Yes	76 182	100 176	2.558 0.480	20 17	13 17	1.692 0.069
315	304	0.597	Yes	Yes	257	247	0.614	Yes	Yes	51	51	0.035	7	6	0.200
485	430	2.571	Yes	Yes	375	375	0.013	Yes	Yes	101	46	6.415	9	9	0.084
219 143	229 173	0.677 2.428	Yes Yes	Yes Yes	144 21	154 51	0.809 5.101	Yes No	Yes Yes	70 115	70 115	0.015 0.035	5 7	5 7	0.171 0.144
56	57	0.133	Yes	Yes	8	9	0.343	Yes	Yes	47	47	0.024	1	1	0.160
76	118	4.264	Yes	Yes	7	49	7.851	No	Yes	67	67	0.041	2	2	0.000
51 69	23 196	4.653 11.087	Yes No	Yes No	5 14	15 107	3.113 12.001	Yes No	Yes Yes	44 54	8 89	7.060 4.189	2	0	2.121 1.500
439	254	9.938	No	No	423	196	12.001	No	No	10	52	7.543	6	6	0.000
1579	1575	0.101	Yes	Yes	1388	1389	0.027	Yes	Yes	173	167	0.460	18	19	0.232
1019 1104	1023 976	0.125 3.969	Yes Yes	Yes Yes	909 582	887 653	0.734 2.877	Yes Yes	Yes Yes	91 499	110 308	1.895 9.493	19 24	26 15	1.476 2.003
1591	1583	0.201	Yes	Yes	1014	991	0.730	Yes	Yes	539	557	0.772	38	35	0.493
1114	1209	2.787	Yes	Yes	852	747	3.705	Yes	Yes	228	440	11.588	34	22	2.274
1133	1017	3.538	Yes	Yes	749 274	666 277	3.135	Yes	Yes	370 24	331 151	2.095	13 0	20 0	1.626
298 333	428 245	6.823 5.176	No No	No Yes	309	189	0.181 7.605	Yes No	Yes No	24	151 56	13.577 5.060	0	0	0.000
9	0	4.243	Yes	Yes	9	0	4.243	Yes	Yes	0	0	0.000	0	0	0.000
8	2	2.683	Yes	Yes	8	2	2.683	Yes	Yes	0	0	0.000	0	0	0.000
0	0	2.000 0.000	Yes Yes	Yes Yes	0	0	2.000 0.000	Yes Yes	Yes Yes	0	0	0.000	0	0	0.000
16	15	0.254	Yes	Yes	16	15	0.254	Yes	Yes	0	0	0.000	0	0	0.000
2	0	2.000	Yes	Yes	1	0	1.414	Yes	Yes	1	0	1.414	0	0	0.000
3 15	9	2.449 1.732	Yes Yes	Yes Yes	3 15	9	2.449 1.732	Yes Yes	Yes Yes	0	0	0.000	0	0	0.000
24	35	2.025	Yes	Yes	22	23	0.211	Yes	Yes	2	11	3.530	0	1	1.414
49	76	3.415	Yes	Yes	46	61	2.051	Yes	Yes	3	14	3.773	0	1	1.414
8 4	18 7	2.774	Yes	Yes	8	17	2.546	Yes	Yes	0	1	1.414	0	0	0.000
3	2	1.279 0.632	Yes Yes	Yes Yes	2	5 2	0.471	Yes Yes	Yes Yes	0 1	0	1.414	0	0	1.414 0.000
11	7	1.333	Yes	Yes	10	7	1.029	Yes	Yes	1	0	1.414	0	0	0.000
4	0	2.828	Yes	Yes	4	0	2.828	Yes	Yes	0	0	0.000	0	0	0.000
1	3	0.816 1.414	Yes Yes	Yes Yes	1	2	0.816 0.816	Yes Yes	Yes Yes	0	0	0.000 1.414	0	0	0.000
1	3	1.414	Yes	Yes	1	2	0.816	Yes	Yes	0	1	1.414	0	0	0.000
18	15	0.739	Yes	Yes	17	15	0.500	Yes	Yes	1	0	1.414	0	0	0.000
28 307	34 286	1.078 1.220	Yes Yes	Yes Yes	23 288	19 278	0.873 0.594	Yes Yes	Yes Yes	4 19	15 8	3.569 2.994	0	0	1.414 0.000
336	365	1.549	Yes	Yes	315	305	0.568	Yes	Yes	21	60	6.128	0	0	0.000

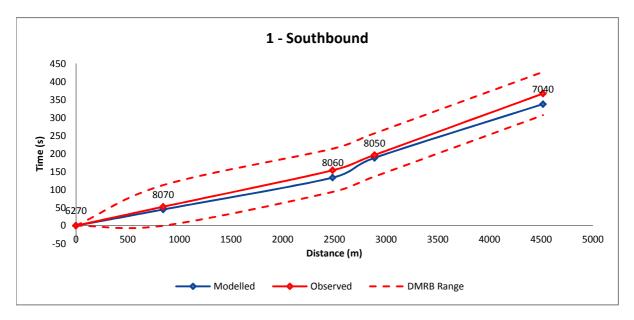


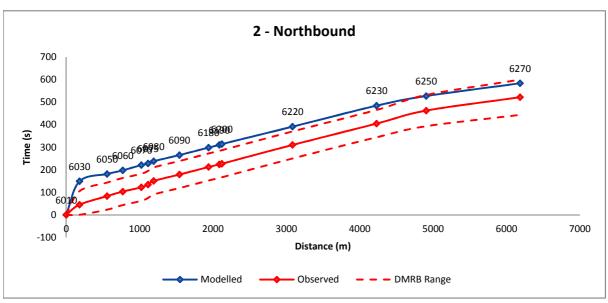


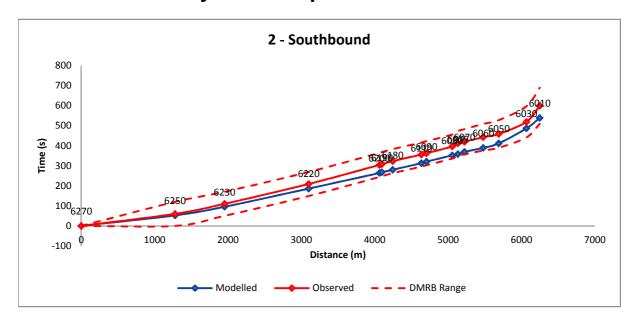
# Appendix F

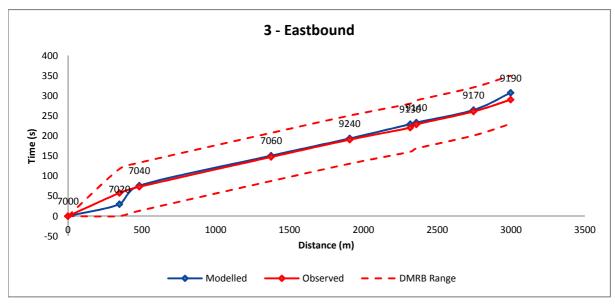
**JOURNEY TIME GRAPHS** 

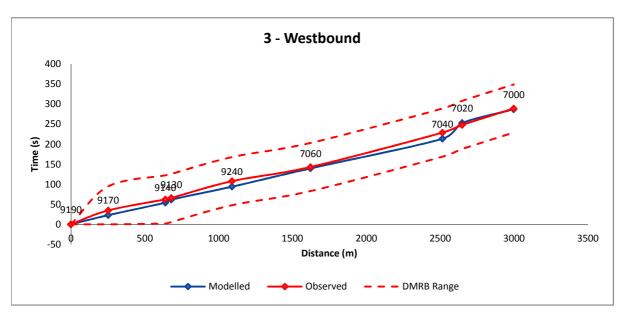


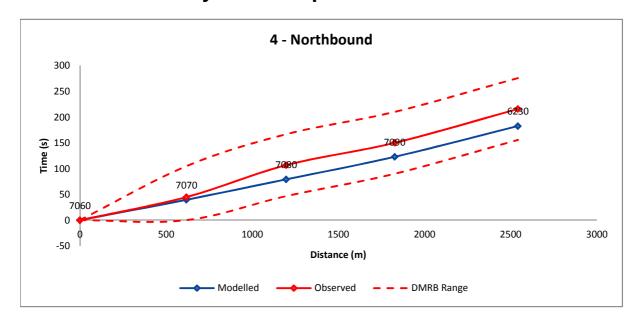


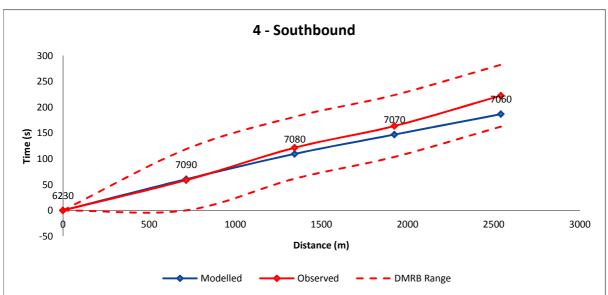


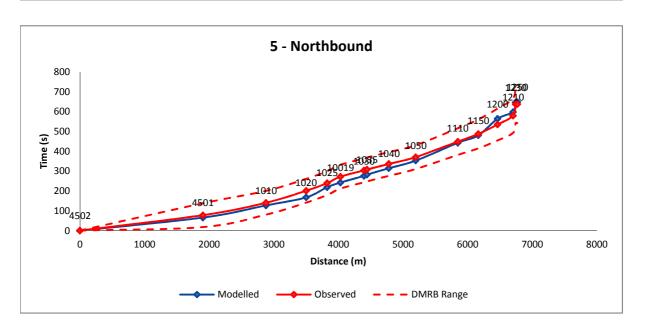


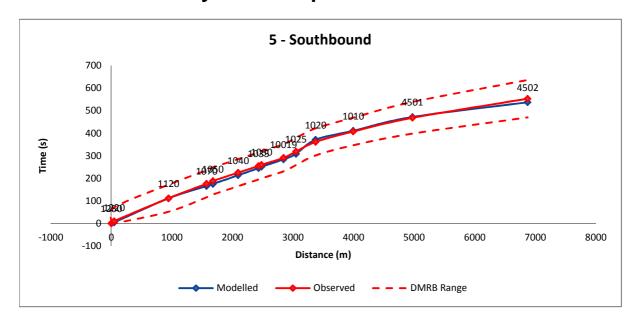


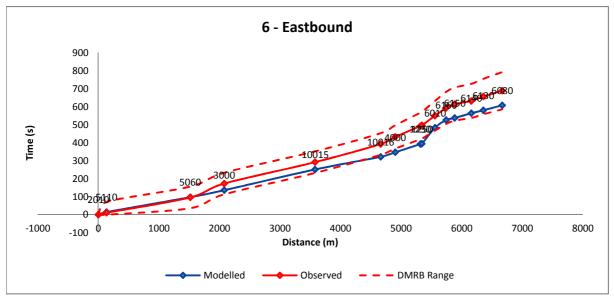


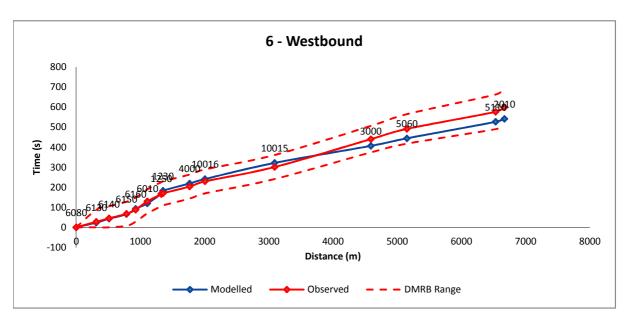


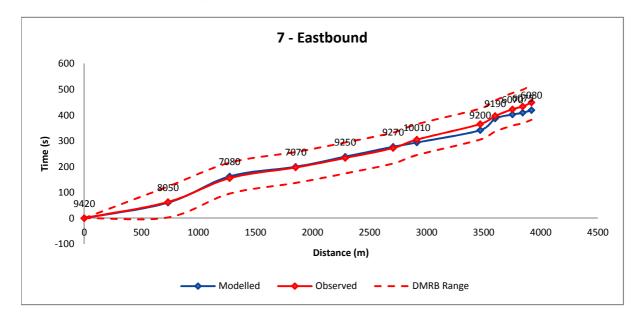


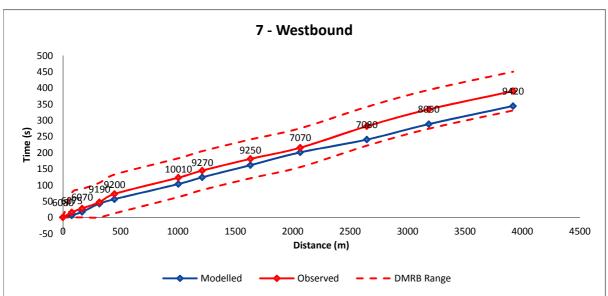


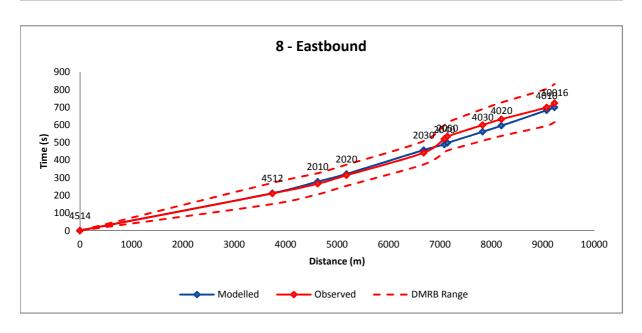


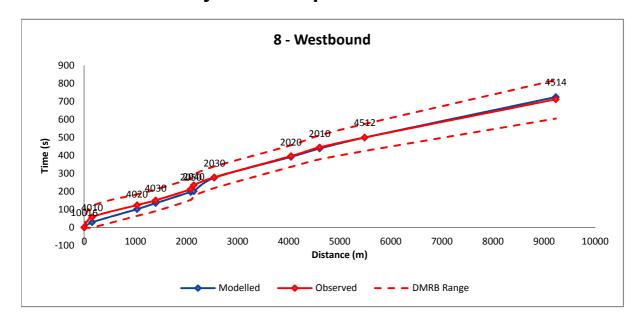


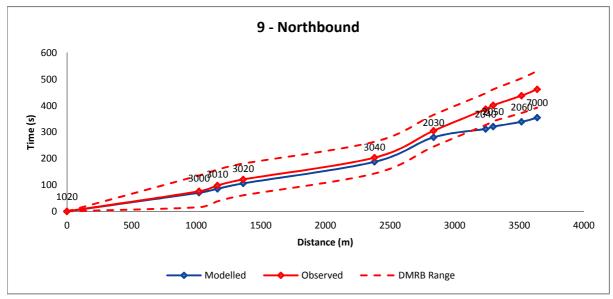


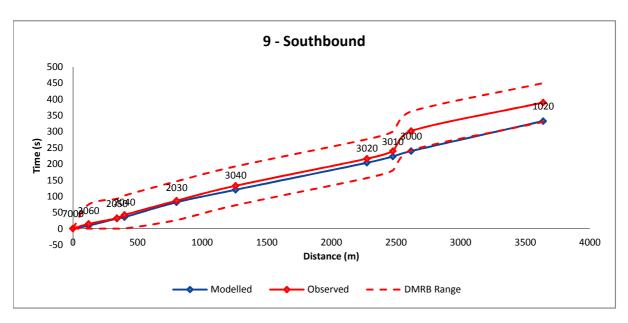


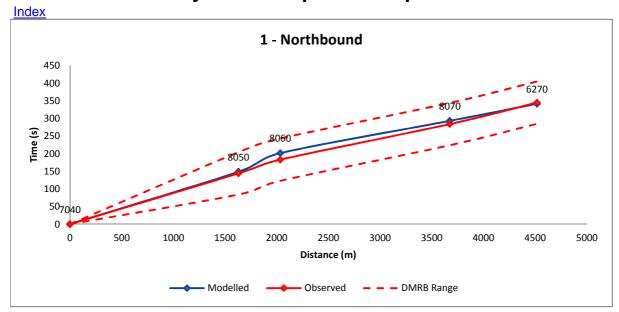


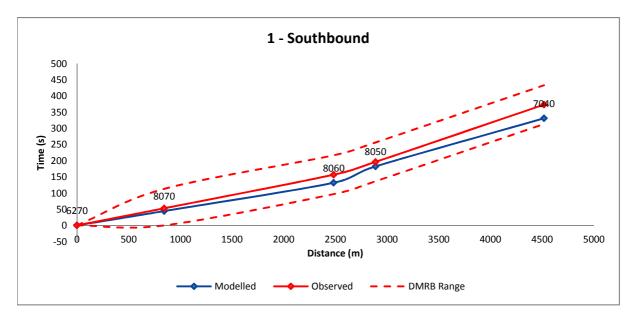


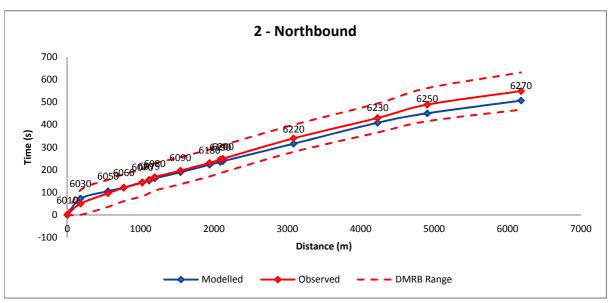


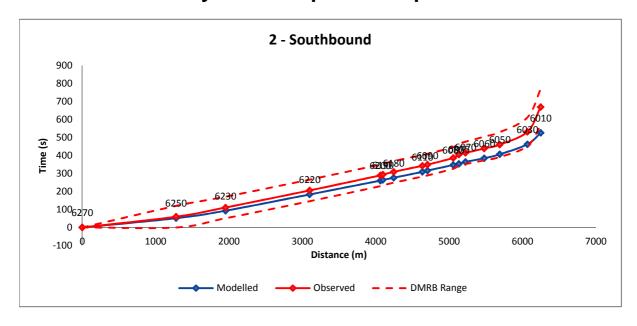


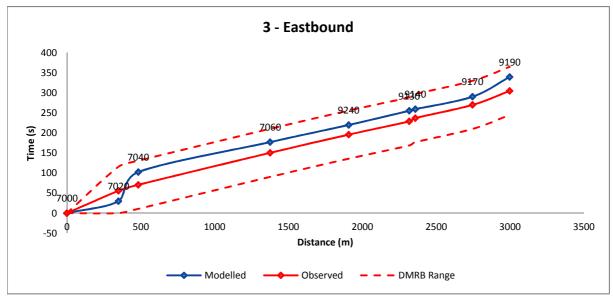


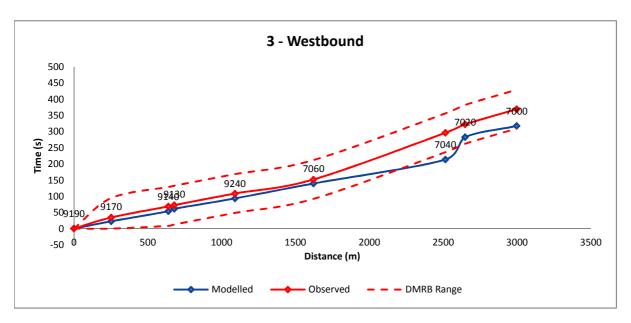


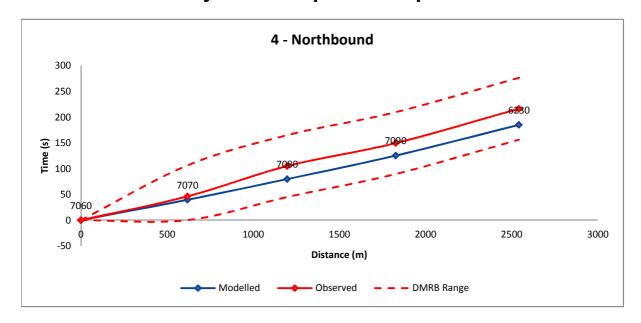


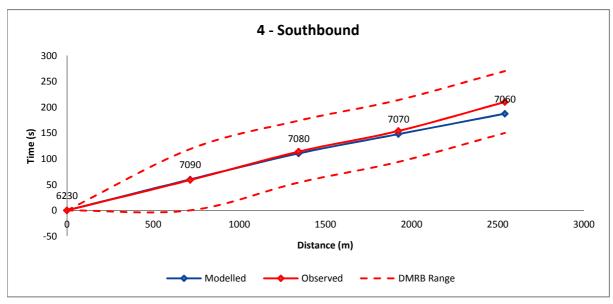


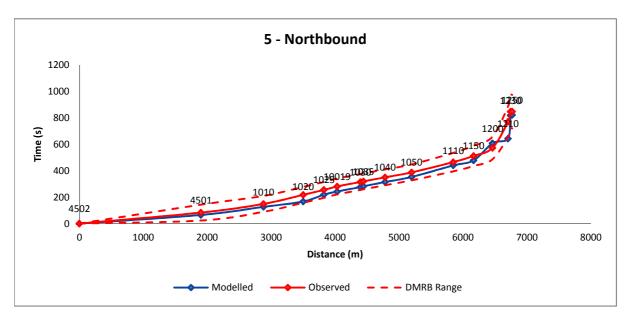


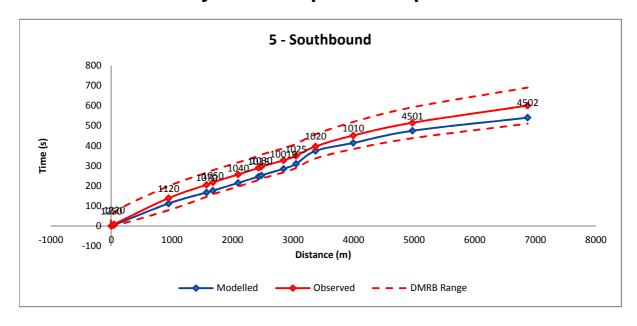


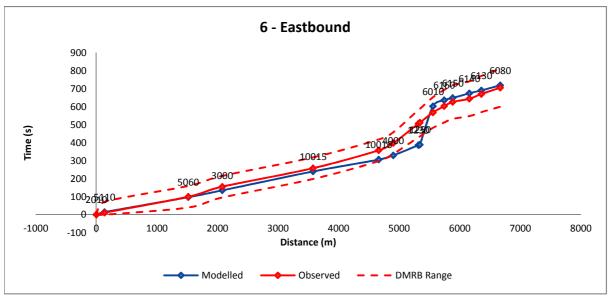


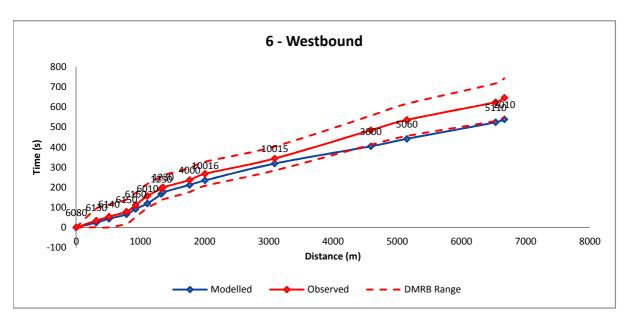


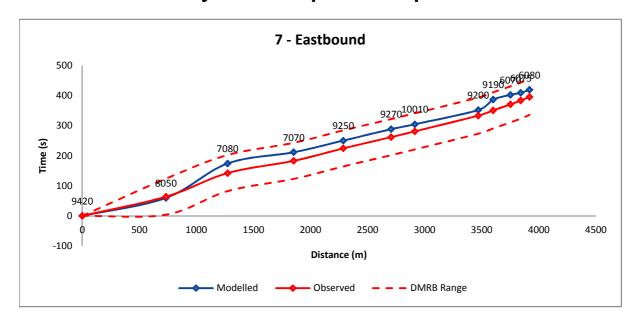


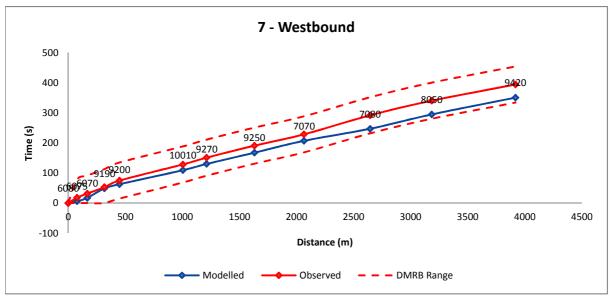


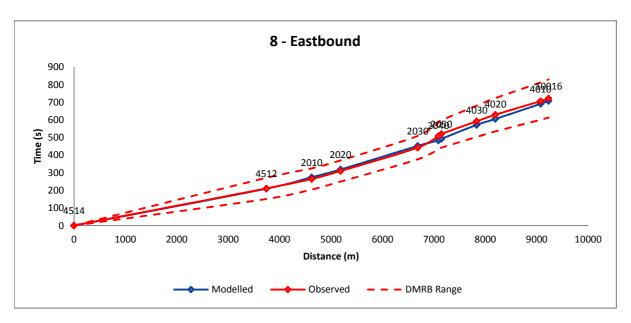


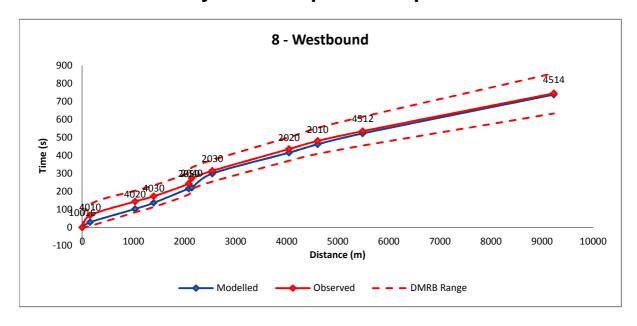


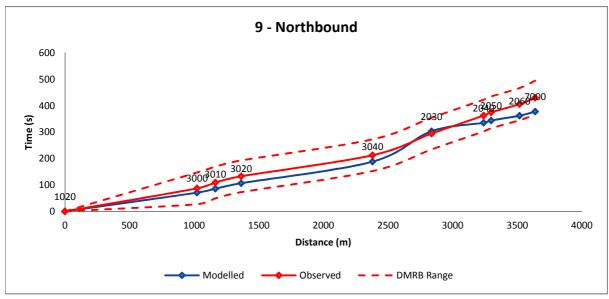


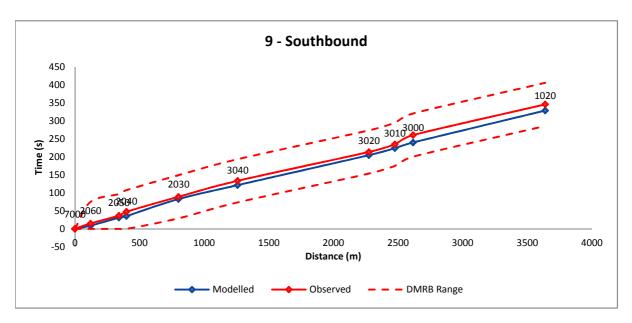


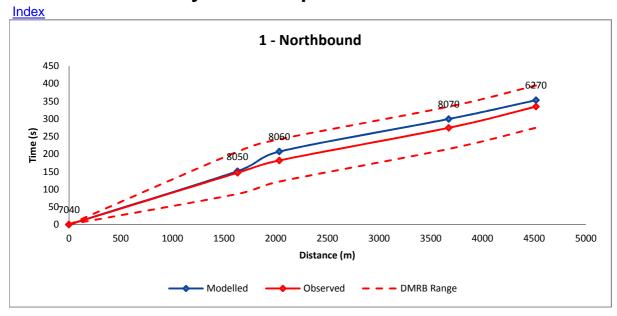


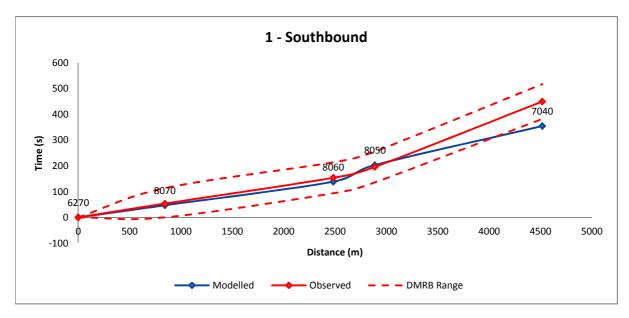


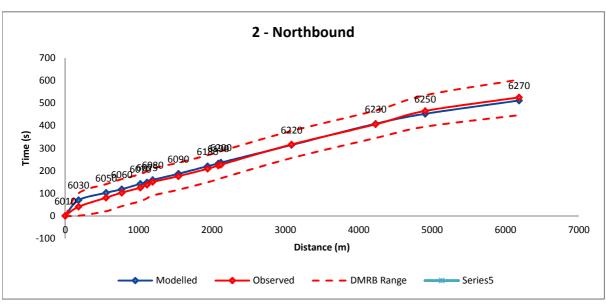


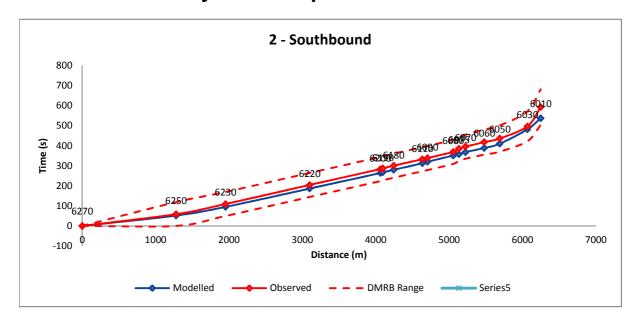


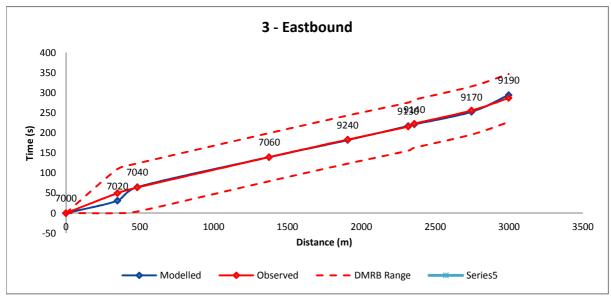


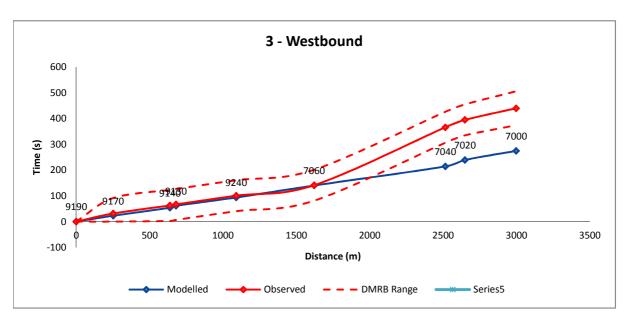


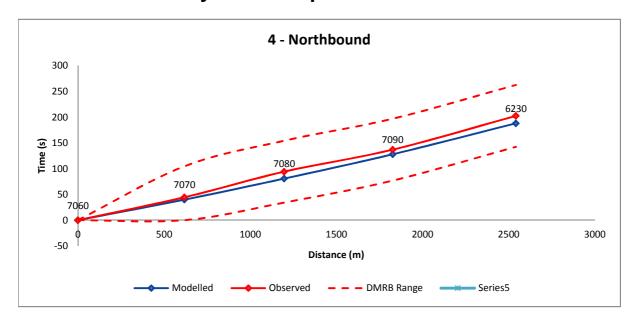


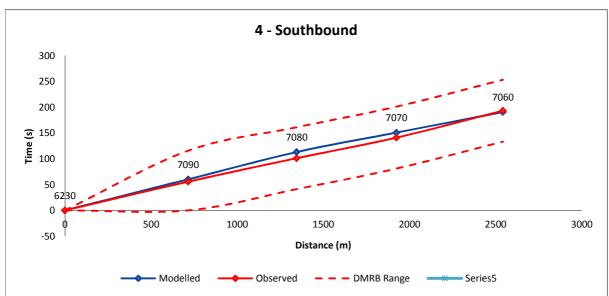


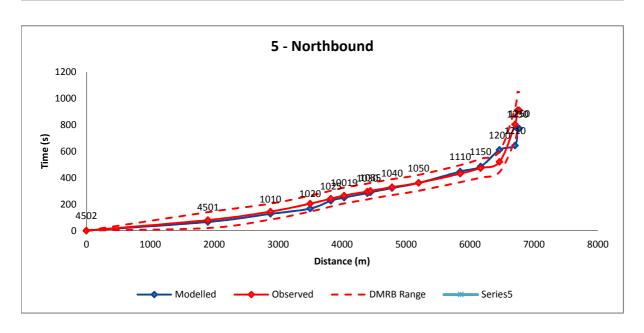


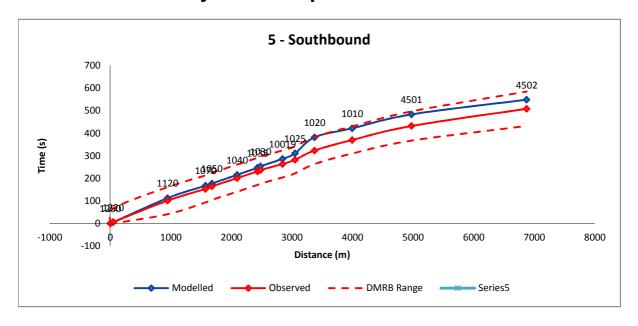


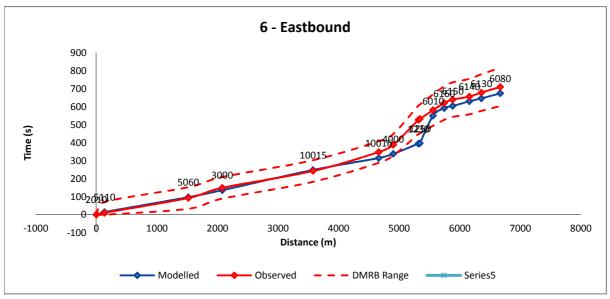


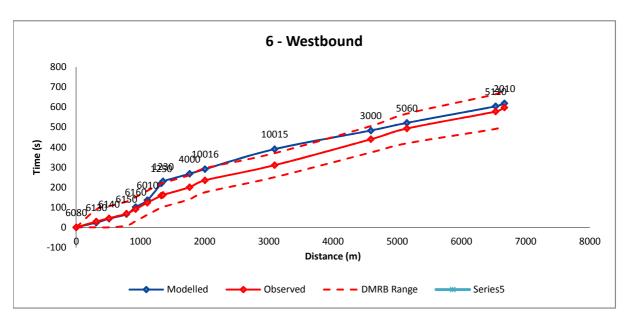


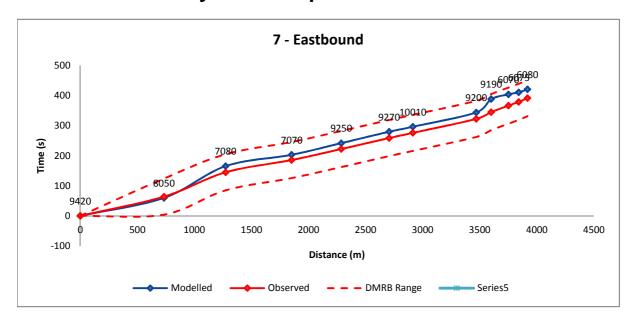


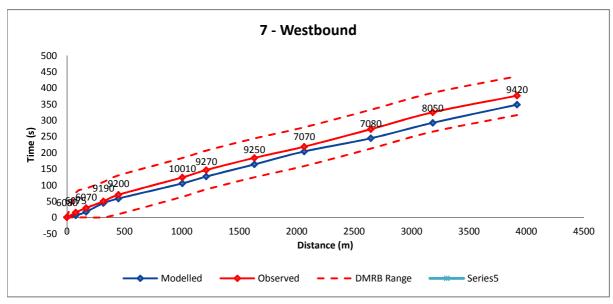


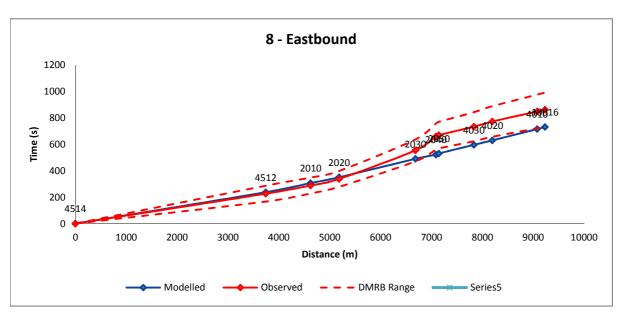


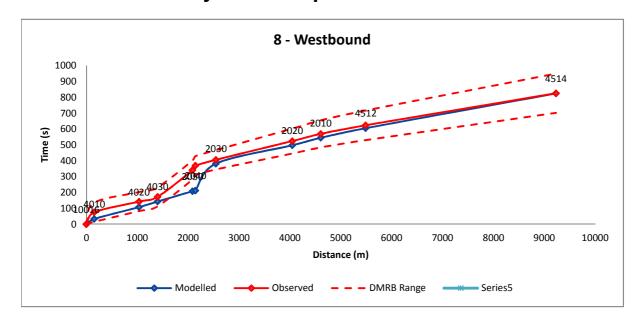


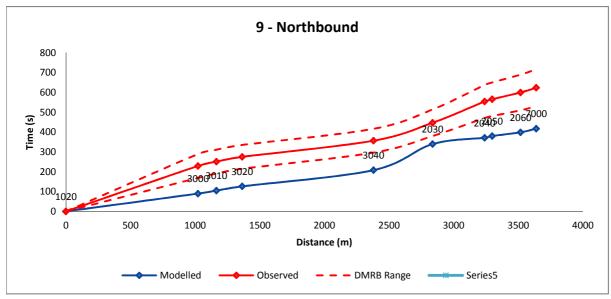


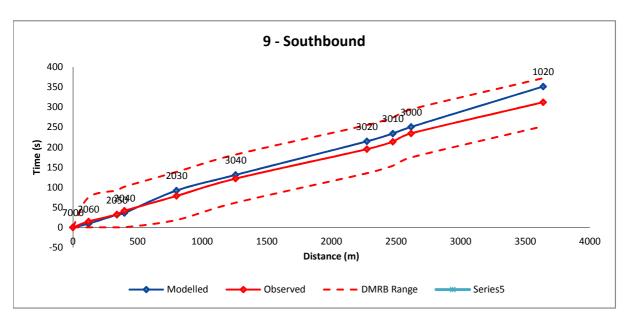












# Appendix G

FLOW AND V/C PLOTS

